



Karlsruher Institut für Technologie

(3A-LS-01.9)

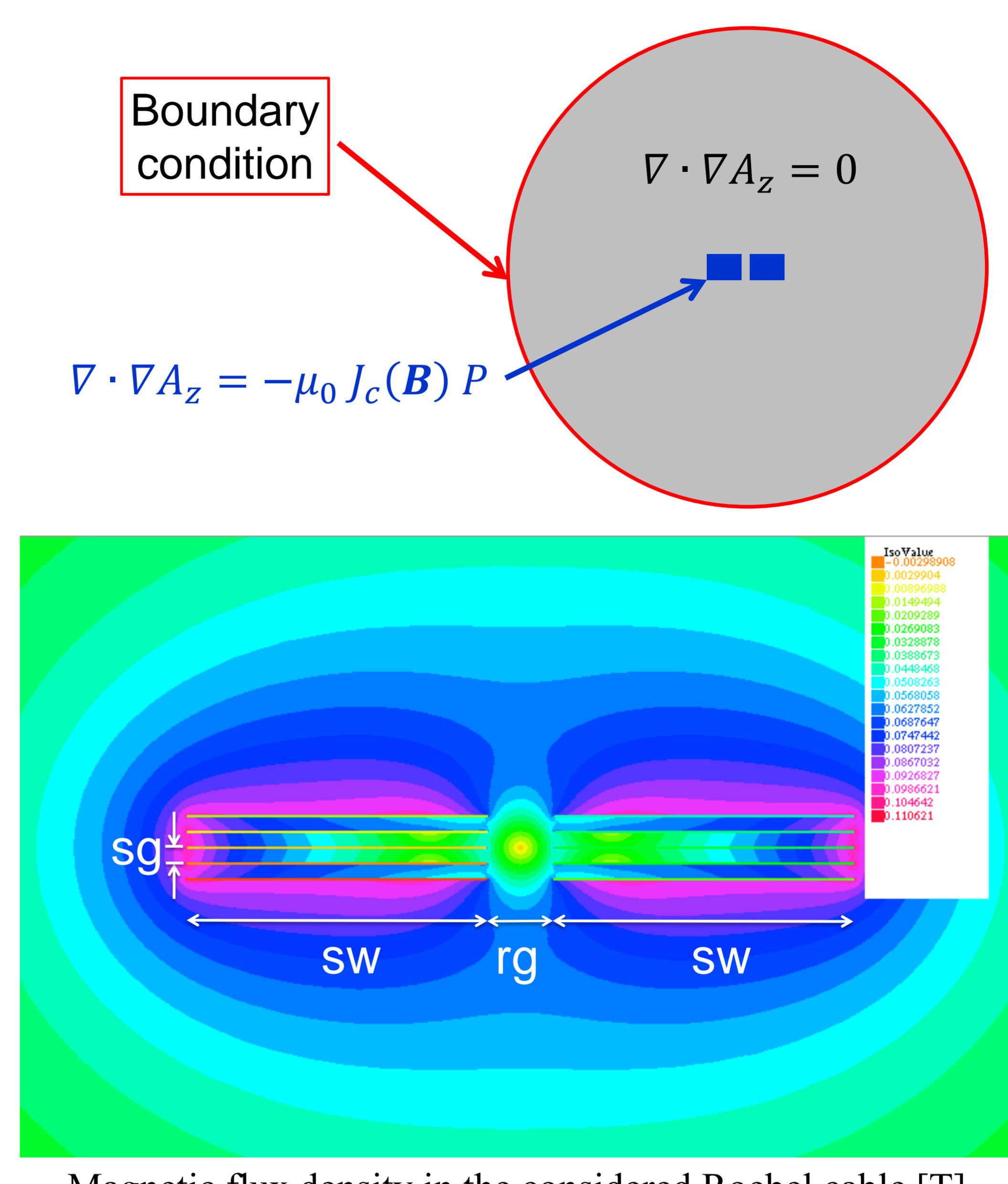
Open Source Codes for Computing the Critical Current of Superconducting Devices

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1 // A FreeFem++ code to calculate the Ic of superconducting cables //
2 // By Victor Zermeno and Salman Quaiyum doi:10.1109/TASC.2015.XXXXXXX //
3 //Declaration of parameters and variables for geometry, Physics and mesh //
4 bool s=0; string c="AVG"; if(s){c="MAX";} //Ic criteria: s=(1->MAX,0->AVG)
5 real Jc0=4.75e10, Bc=35e-3, b=0.6, k=.25; // Jc(B) parameters
6 int ns=10, ny=ns/2; // ns-number of strands in cable
7 real th=le-6, sw=1.8e-3, rg=4e-4, sg=le-4, n=21, tolAz=le-9, tolP=le-9;
8 real I0=Jc0*th*sw, x0=-sw-rg/2, y0=-((th+sg)*ny-sg)/2, E=0, Ec=le-4, err;
9 real[int] XC(ns), YC(ns), Ics(ns), p(ns^2), pn(p.n); p=0.9; pn=0.9;
10 int[int] cm(1), hm(ns), vm(ns); cm=50; hm=50; vm=1; // Mesh parameters
11 //////////////////// Creation of geometry and mesh ///////////////////
12 for(int i=0; i<ns; i++) {XC[i]=x0+(rg+sw)*(i/ny); YC[i]=y0+(sg+th)*(i/ny);}
13 border bb (t=0, 2*pi) {x=20*sw*cos(t); y=20*sw*sin(t); label= 1;}
14 border top (t=0, 1; i) {x=XC[i]+t*sw; y=YC[i]+th; label=i+2;}
15 border right (t=0, 1; i) {x=XC[i]+sw; y=YC[i]+(1-t)*th; label=i+2;}
16 border bottom (t=0, 1; i) {x=XC[i]+(1-t)*sw; y=YC[i]; label=i+2;}
17 border left (t=0, 1; i) {x=XC[i]; y=YC[i]+t*th; label=i+2;}
18 mesh Th=buildmesh(bb(cm)+top(hm)+right(vm)+bottom(hm)+left(vm));
19 //////////////////// Build FEM Solution Space ///////////////////
20 fespace Vh(Th,P2); // Quadratic elements for Az
21 Vh Az, Az0, v;
22 fespace Wh(Th,P1dc); // Piecewise-linear discontinuous elements for J
23 Wh J=Jc0;
24 p[Th(0,0).region]=0; // p=0 in the Air region
25 ////////////////// JcB and J as functions of Az using the dummy variable u ///////////////////
26 macro JcB(u) Jc0/(1+sqrt((k*dy(u))^2+(-dx(u))^2)/Bc)^b //
27 macro J(u) JcB(u)*(p[region])//
28 //PDE(in weak form) Div(Grad(Az))+mu0*Jc(B)*p=0 and boundary condition Az=0
29 problem Pmodel(Az,v)=int2d(Th)(dx(Az)*dx(v)+dy(Az)*dy(v))
30 -int2d(Th)(4e-7*pi*J(Az0)*v)+on(1,Az=0);
31 //////////////////// Solution using an iterative solver ///////////////////
32 while(abs(p.max-1)*s+abs(pn(0:ns-1).sum/ns-1)*(1-s)>tolp){ // Ic criterion
33 err=1; // Reset err variable
34 while(err > tolAz){ // Self consistency loop
35 Az0=Az;
36 Pmodel; // Update old Az estimate
37 for(int j=0; j < ns; j++){ // Ic and p value of j-th strand
38 Ics(j)=int2d(Th,j)(JcB(Az));
39 p(j)=I0/Ics(j); // Difference between old and new Az estimates
40 Az0=Az-Az0; // Error defined using the L-infinity norm
41 err=Az0[].linfty; // Error defined using the L-infinity norm
42 for(int i=0; i<ns; i++) {pn(i)=p(i)*n;}
43 E= pn(0:ns-1).sum/ns*Ec; // Average electric field in cable
44 I0=2*I0/((1+p.max)*s+(1+(E/Ec)^(1/n))*(1-s)); //Net current in strand
45 //////////////////// Post Processing: Output data and plotting ///////////////////
46 cout << endl << "Ic= " << ns*I0 << " A " << "(<< c << criteria)" << endl;
47 Vh B=sqrt(dx(Az)^2+dy(Az)^2);
48 plot(B, wait=1, fill=1, value=1);

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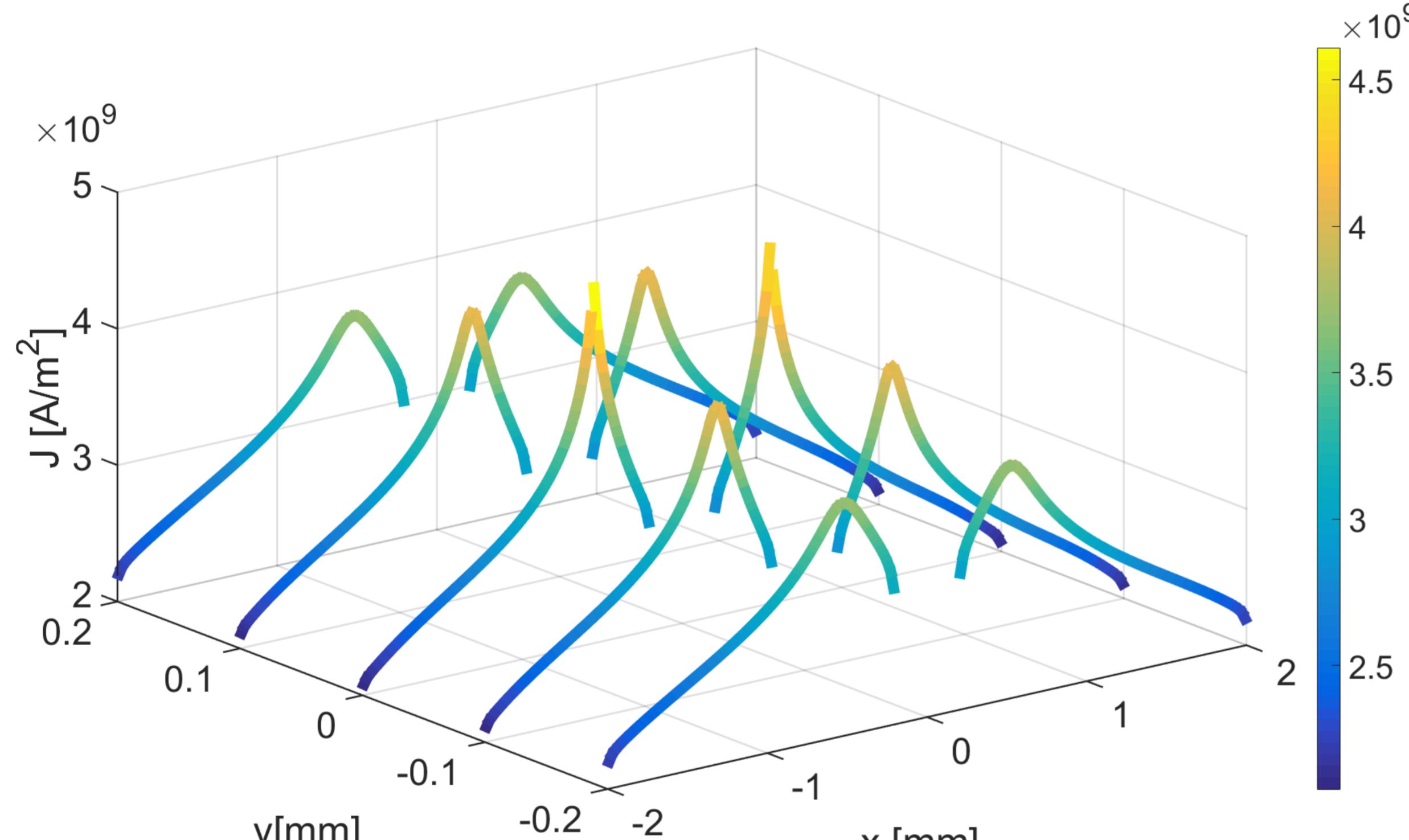
Magnetic flux density in the considered Roebel cable [T]

Comparison of results given by different implementations				
Software	I _c _{MAX} (A)	I _c _{AVG} (A)	c _t _{MAX} (s)	c _t _{AVG} (s)
Comsol	534.65	538.93	6.00	5.00
FreeFEM++	535.76	537.12	34.30	45.01
MATLAB	535.83	53		
Octave	535.83	539.25	0.13	0.13

I_c=critical current, c_t=computing time (excluding plotting).

$$\mathbf{B}_i = \frac{\mu_0}{2 \pi} \sum_{j \neq i} P I_c(\mathbf{B}_j) \frac{\{-(y_i - y_j), x_i - x_j\}}{(x_i - x_j)^2 + (y_i - y_j)^2}$$

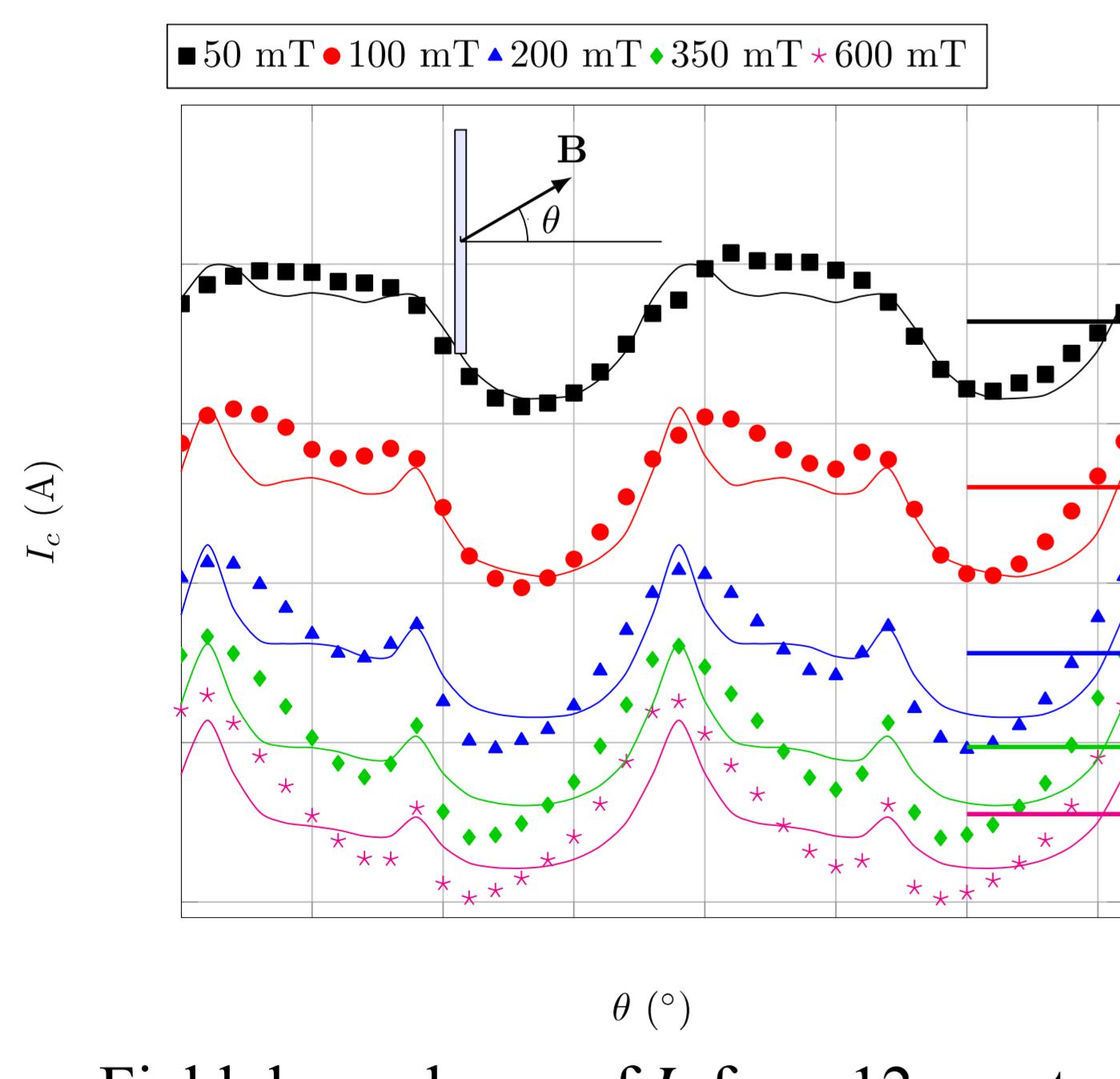
The diagram shows a multi-strand cable with several strands. A green arrow points downwards from the strands, indicating the direction of current flow. To the right, a mathematical equation for calculating the magnetic flux density \mathbf{B}_i is shown, involving the permeability of free space μ_0 , the number of strands j , the critical current I_c of each strand, and the coordinates of the strands.



```

1 % A MATLAB code to calculate the Ic of superconducting cables %
2 % By Victor Zermeno and Salman Quaiyum doi:10.1109/TASC.2015.XXXXXXX %
3 %% Initialization and declaration of parameters and variables %
4 clc; clear all; close all;
5 s=0; c='AVG'; if (s==1) c='MAX';end; %Ic criteria: s=(1->MAX,0->AVG)
6 Jc0=4.75e10; Bc=35e-3; k=0.25; b=0.6; % Jc(B)parameters
7 m=100; ns=10; th=le-6; sw=1.8e-3; rg=4e-4; sg=le-4; n=21; % parameters
8 mu0=4e-7*pi; Ec=le-9; tolIc=le-9; tolP=le-9; %mu0, Ec criterion, tolerances
9 I0=Jc0*sw*th; P=0.5*ones(1,m*ns); E=0; % Initial values for I0, P and E
10 [Bx,By,Ic]=deal(zeros(1,m*ns)); %Magnetic flux density and critical current
11 %% Geometry creation: lines of current are located at the points (Rx,Ry) %%
12 xRange=(1-m:2:m-1)*sw/2;m; % Span of values for x coordinate
13 Rx=[repmat(xRange-(rg+sw)/2,[1 ns/2]),repmat(xRange+(rg+sw)/2,[1 ns/2])];
14 yRange=((2-ns):4:(ns-2))*sg/4; % Span of values for y coordinate
15 Ry=[reshape(repmat(yRange,m,1),1,[]),reshape(repmat(yRange,m,1),1,[])];
16 %% Definition of auxiliary variables for field calculation %%
17 r2=bsxfun(@minus,Rx,Rx').^2+bsxfun(@minus,Ry,Ry').^2; r2=(x-x')^2+(y-y')^2
18 xn=bsxfun(@minus,Rx,Rx')./r2; xn(isnan(xn))=0; % if(r2>0,(x-x')/r2,0)
19 yn=bsxfun(@minus,Ry,Ry')./r2; yn(isnan(yn))=0; % if(r2>0,(y-y')/r2,0)
20 %% Iterative solution %%
21 while (abs(max(P)-1)*s+abs(E/Ec-1)*tolP) > tolIc % Ic criteria loop
22 err = 1; % Error reset
23 while (err > tolIc) % Self consistency loop
24 IcOld=Ic;
25 Ic=(sw*th)*(Jc0./(1+sqrt((k*Bx).^2+Bx.^2)./Bc)).^b; %local Ic(B)
26 P=reshape((I0./((reshape(Ic,m,ns)'*ones(m,m))),1,m*ns)); %P values
27 It=P.*Ic; % Local current in strand
28 Bx=-mu0/(2*pi)*It*yn; % Magnetic flux density
29 By=mu0/(2*pi)*It*xn;
30 err=norm(IcOld - Ic); % Error. It compares old and new Ic estimates
31 end
32 E=Ec*abs(sum(P(1:m:end).^n)/ns); % Average electric field in cable
33 I0=2*I0/(s*(1+max(P))+(1+(E/Ec)^(1/n))*(1-s)); %Net current in strand
34 %% Post Processing: Output data and plotting %%
35 fprintf('Ic(cable)= %0.2f A (%s criteria)\n',ns*I0,c);
36 fprintf('Avg(E)= %0.6f microV/cm\n',abs(sum(P(1:100:end).^n)/ns));
37 fprintf('max(P)= %0.6f\n',max(P));
38 x=reshape(Rx,ns,[])/le-3;
39 y=reshape(Ry,ns,[])/le-3;
40 Z=(ns/sw/th)*reshape(It,ns,[]);
41 xlabel('x [mm]'); ylabel('y [mm]'); zlabel('J [A/m^2]');
42 mesh(X,Y,Z,'MeshStyle','column','FaceColor','none','LineWidth',3); % J(x,y)
43 colorbar;

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Field dependence of I_c for a 12 mm tape.

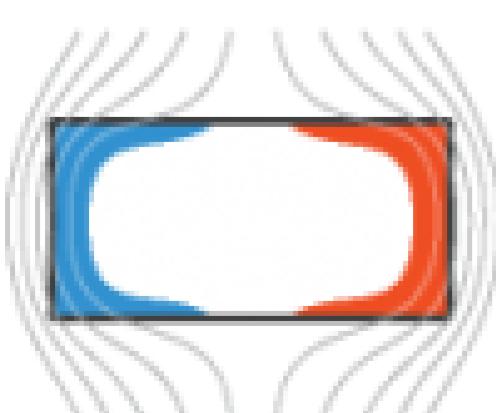
Application:

Effect of the angular dependence of $J_c(\mathbf{B})$ in calculating the I_c of a 10-strand Roebel cable.

I_c of a 12 mm-wide Roebel

	I _c _{MAX} (A)	I _c _{AVG} (A)
Precise $J_c(\mathbf{B})$	1005	1035
Simplified $J_c(\mathbf{B})$	1045	1067

This and more codes available at



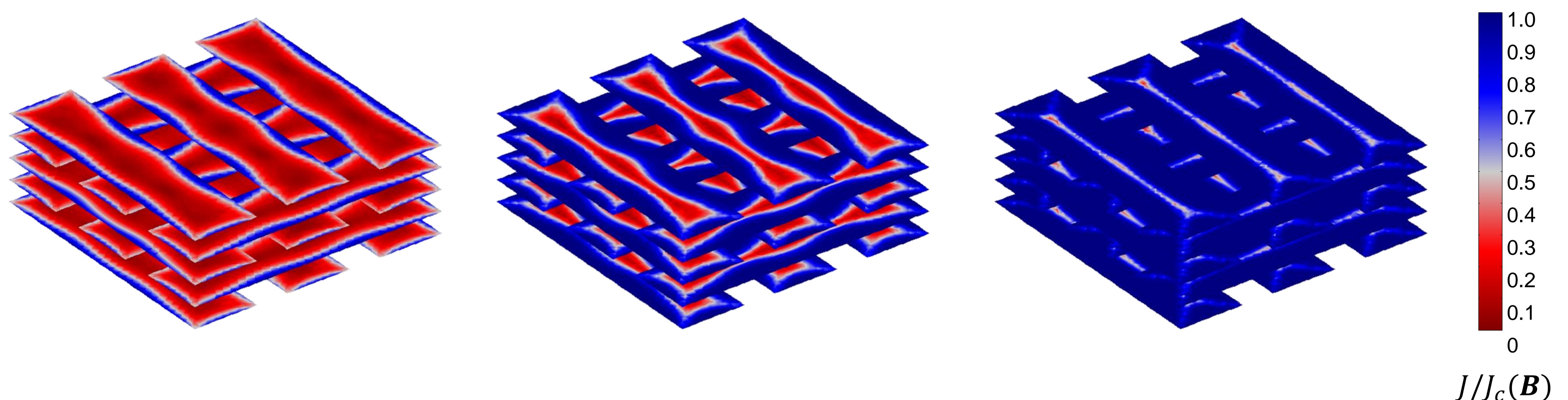
HTS MODELLING
WORKGROUP



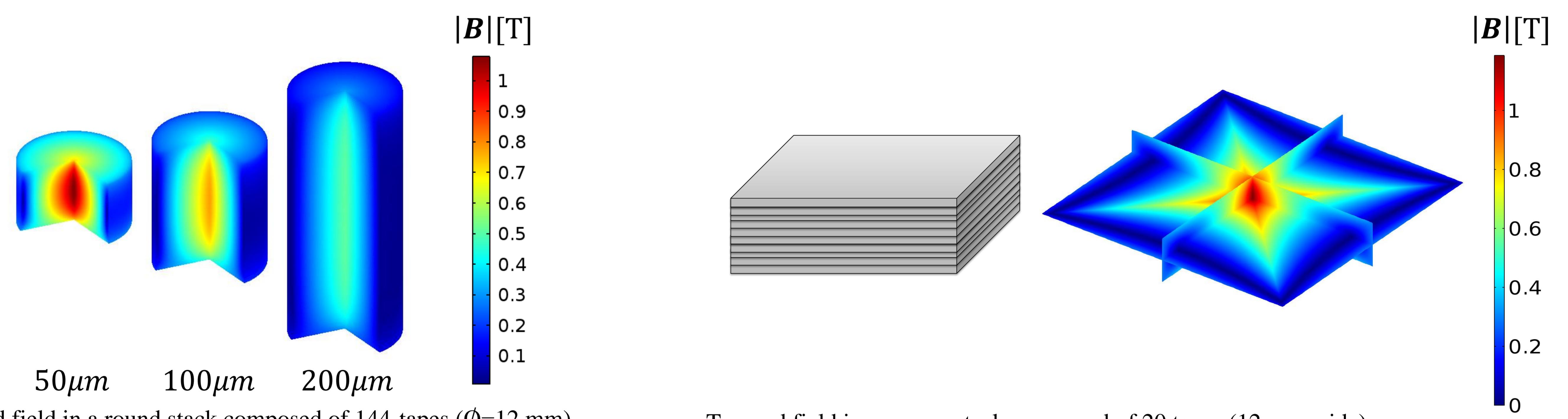
Current modeling activities (3A-LS-01.9)

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Magnetization of crossed HTS stacks



Maximum possible trapped field in HTS stacks



Trapped field in a round stack composed of 144-tapes ($\phi=12$ mm).
Three different separations between the HTS layer are considered:
50 μ m, 100 μ m and 200 μ m.

Trapped field in a square stack composed of 20 tapes (12 mm wide).
A distance of 100 μ m between HTS layers is assumed

Current distribution in multi-filamentary wires

