



# Overview on the research and development of HTS conductors and irradiation studies within the EU-DEMO project

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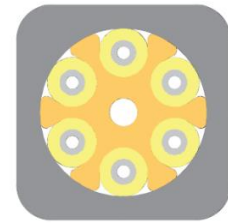
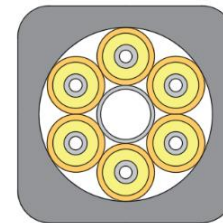
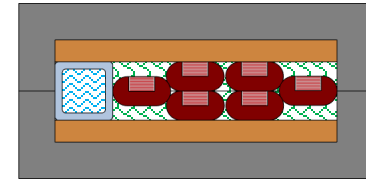
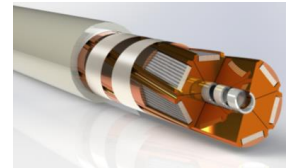
This work has been carried out within the framework of the EUROfusion Consortium, funded by the European Union via the Euratom Research and Training Programme (Grant Agreement No 101052200 — EUROfusion). Views and opinions expressed are however those of the author(s) only and do not necessarily reflect those of the European Union or the European Commission. Neither the European Union nor the European Commission can be held responsible for them.



## □ Introduction on EU DEMO tokamak

## □ HTS conductors for the hybrid Central Solenoid

- SECTOR ASsembled CICC (SECAS)
- Aligned Stacks Transposed in Roebel Arrangement (ASTRA)
- CORC-like conductors developed by ASIPP

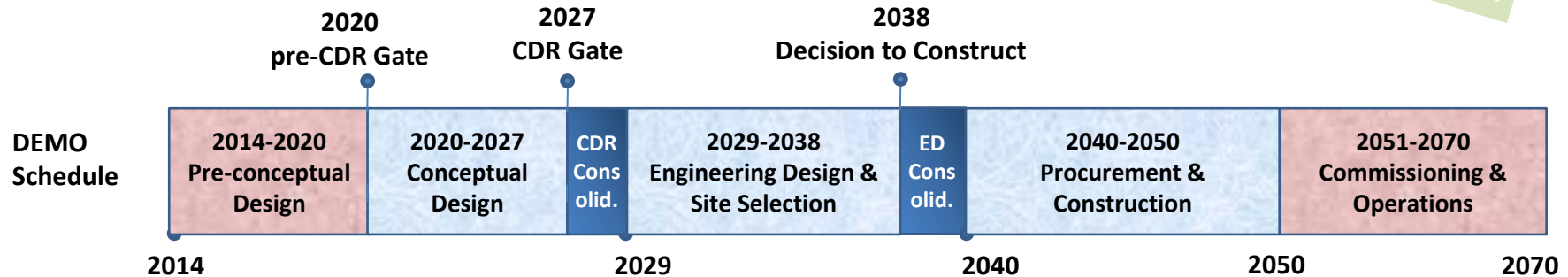


## □ Irradiation activities

# EU Fusion Energy Roadmap



- **EU-DEMO** reactor is designed for demonstrating net production of electricity and operation with a closed fuel cycle (TBR>1)
- The intermediate step between ITER and a commercial Fusion Power Plant (FPP)
- **DEMO: 500 MW net electric power**, and supply to the grid
- The DEMO staged-design approach relies on a progressive flow of validation input from ITER prior to start the DEMO construction (2040).
- Allow extrapolation to a Fusion Power Plant



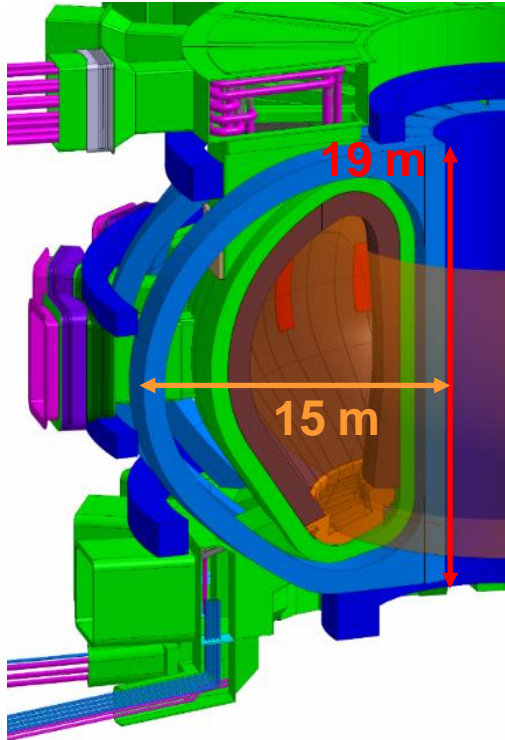
# Main parameters of the DEMO Baseline 2018



**16 TF coils** ( $B_{\text{peak}} = 12\text{T}$ ,  $E_{\text{total}} = 150\text{GJ}$ )

**5 CS coils** ( $B_{\text{peak}} = 15.8\text{T}$ ,  $E_{\text{total}} = 15\text{GJ}$ )

**6 PF coils** ( $B_{\text{peak}} = 8\text{T}$ ,  $E_{\text{total}} = 21\text{GJ}$ )



Parameters	Symbol	EU-DEMO
Major radius	$R_0$ (m)	<b>9</b>
Minor radius	$a$ (m)	2.9
Aspect ratio	$A$	3.1
Plasma current	$I_p$ (MA)	18
Safety factor	$q$	3.6
Plasma elongation	$k_{95}$	1.6
Triangularity	$\delta_{95}$	0.33
Av. electron density	$\langle n_{e,\text{vol}} \rangle$ ( $10^{20}\text{m}^{-3}$ )	0.73
Eff. ionic charge	$Z_{\text{eff}}$	2.2
Confinement enhancement	$H$	1.1
Burn Time	$t_{\text{burn}}$ (hrs)	<b>2</b>
Bootstrap fraction	$f_{\text{bs}}$ (%)	37
Fusion Power	$P_{\text{fus}}$ (MW)	2000
Net electric power	$P_{e,\text{net}}$ (MW)	<b>500</b>
Divertor configuration		Single null

# DEMO CS WP: Hybrid variant

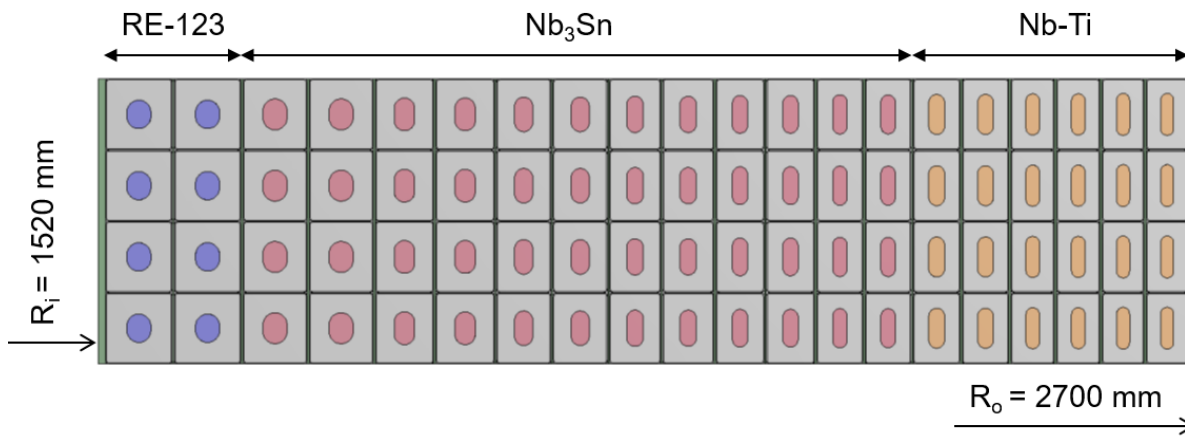


Design		Hybrid variant
Total current [MA]		72.2
Cond current [kA]		46.3
$R_i$ [mm]		1520
$R_o$ [mm]		2700
Max B [T]		15.8
Mag flux [Wb]	Only CS	218.5
	CS+PF	239
$\sigma_{hoop}$ [MPa]		295.4

5 modules CS (with a central double one)

The hybrid variant allows the **Increase of the magnetic flux** wrt the ITER-like design of 13%.

**Layer winding with grading on superconductor and stainless-steel**



**Need to study HTS conductors suitable for the EU-DEMO central solenoid**

# Target for HTS CICC



European-Chinese collaboration with ASIPP for manufacturing, testing and modelling HTS cables and testing the BEST hybrid CS module.

**Presently all manufactured conductors use REBCO tapes**

Inlet Temperature = **4.5 K**

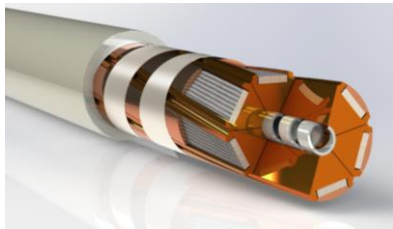
Peak field = **18 T**

Operating current = **60 kA**

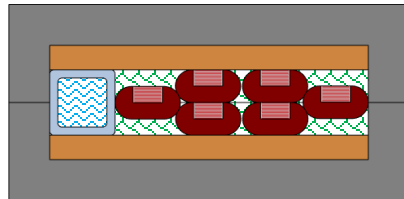
Minimum bending radius = **1.5 m**

DEMO  
CS target

SECAS



ASTRA



Inlet Temperature = **4.5 K**

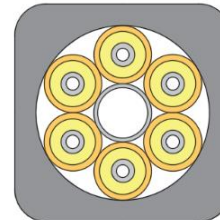
Peak field = **20 T**

Operating current = **46.5 kA**

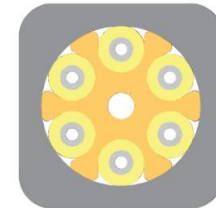
Minimum bending radius = **0.5 m**

BEST CS  
target

Option 1



Option 2



## BRAided STack & SECTOR ASsembled cable:

HTS stack sub-unit + new cable layout/concept

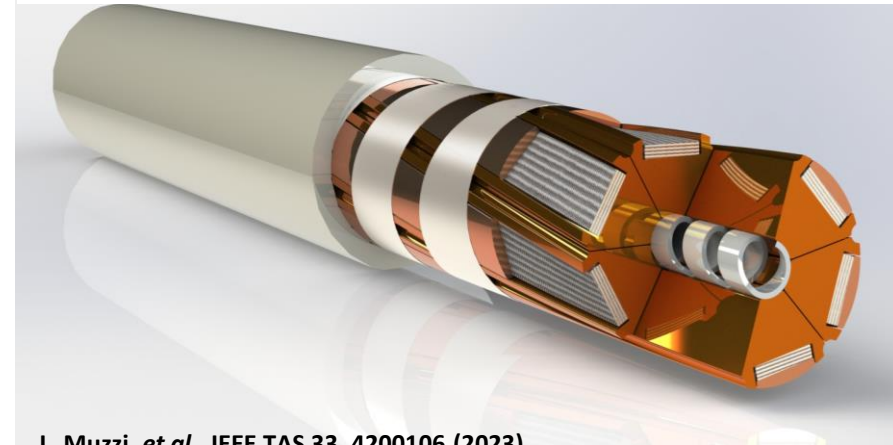
BRAided STacks (**BRAST**) of REBCO tapes



### BRAST Features

Flexible  
Compact  
Easy to handle

SECTOR ASsembled (**SECAS**) CICC concept



L. Muzzi, *et al.*, IEEE TAS 33, 4200106 (2023)

## Multi-stage cable processing approach

### SULTAN sample in preparation: test in 2024

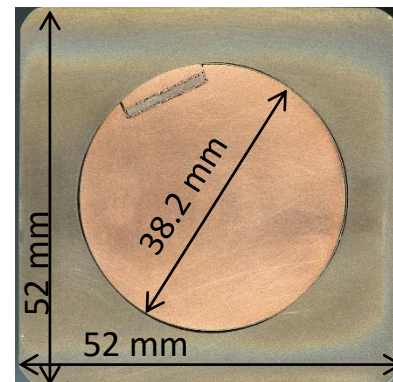
IEEE-CSC, ESAS and CSSJ SUPERCONDUCTIVITY NEWS FORUM (global edition), Issue No. 55, January, 2024. Invited presentation given at IREF 23, November 13, 2023, Arona, Italy



# BRAST mechanical assessment: twisting and compaction



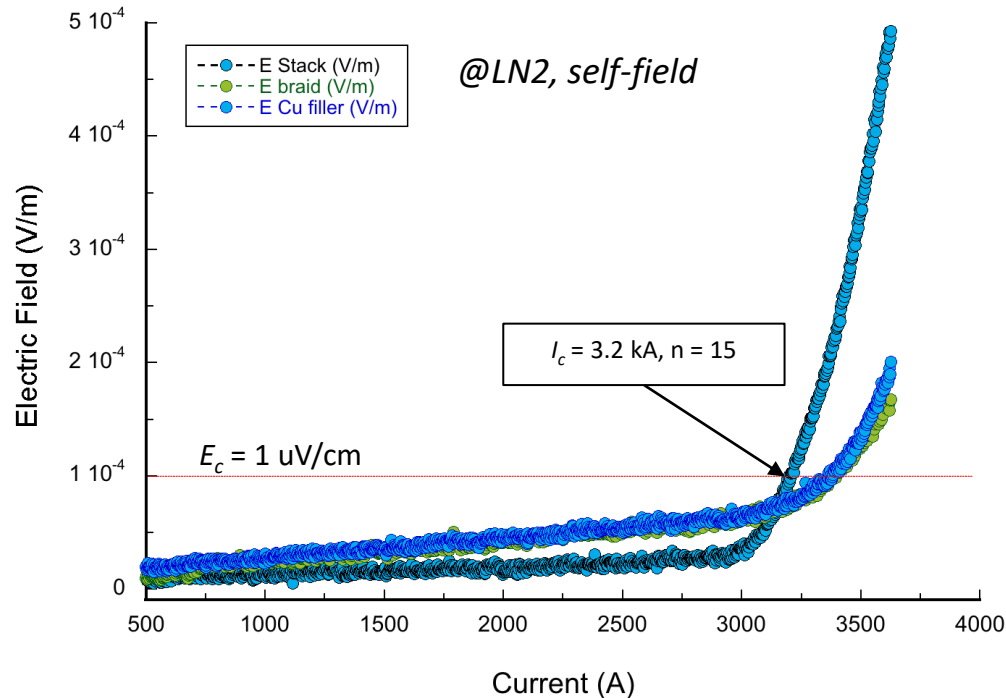
**Core:** Cu tube, dia. 38 mm, with machined spiral slot (Twist Pitch 1.2 m)  
**HTS strand:** BRAST 10 tapes (SuperOx Jp, 12 mm x 0.08 um), Braid: 144 Cu wires, dia. 0.15 mm  
**Jacket:** Circle-in-square SS tube (PF ITER cable), 54 x 54 mm, compacted with a 4 rolls mill @**CRIOTEC Impianti (Italy)**





## In line with calculated cable critical current by FEM model

De Marzi, et al., SuST 34 (2021)



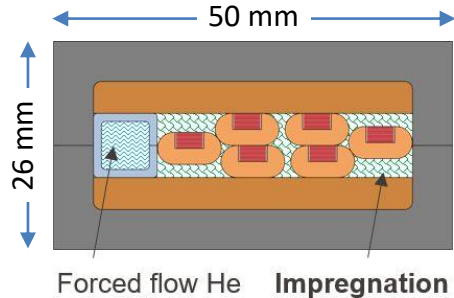
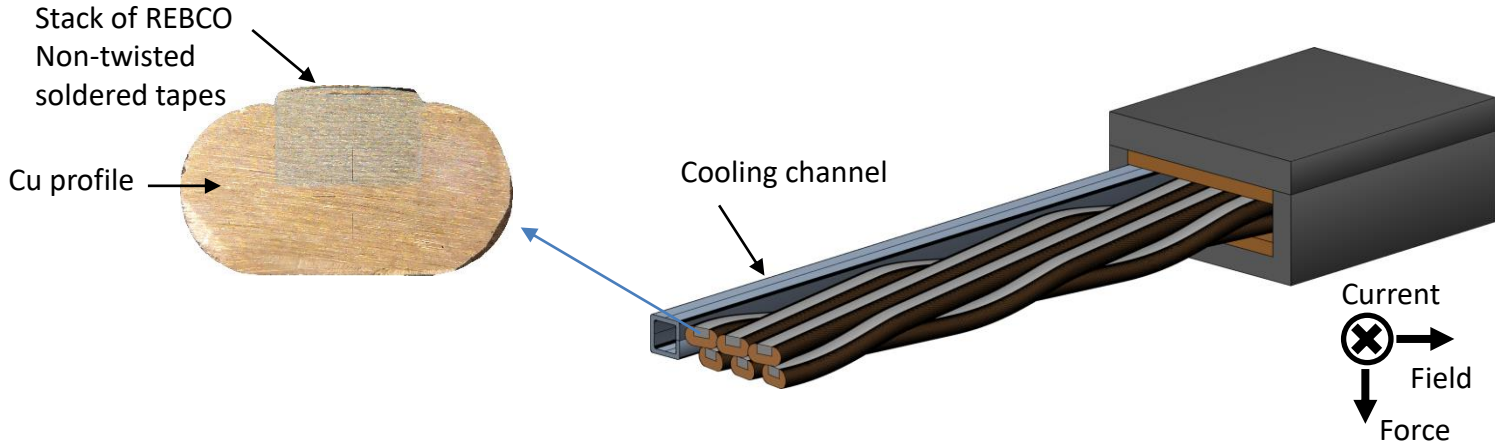
Sample TEST in LN2 @ the ENEA 20kA test facility

Next steps:

- Bending of the sample on a bending radius of 1.5 m
- Electric test to check if there is a degradation of the performance

# ASTRA Conductor prototype: layout

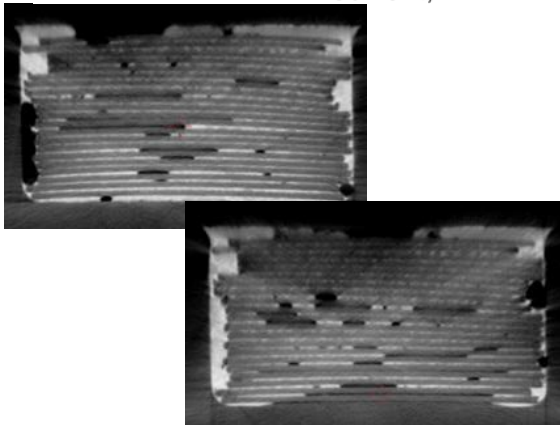
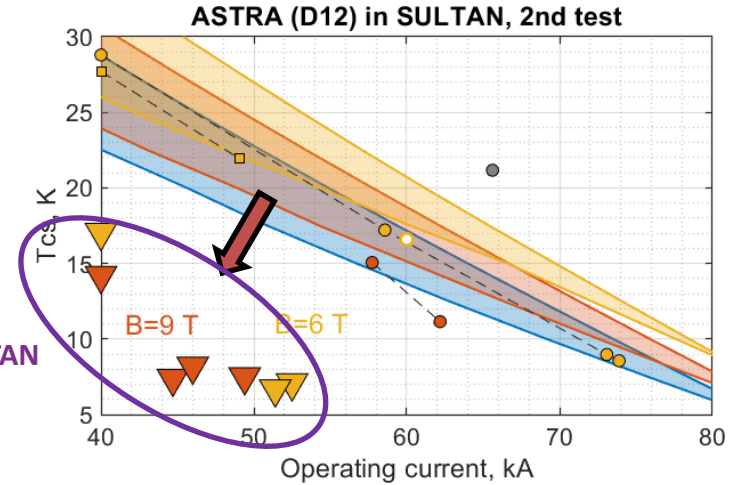
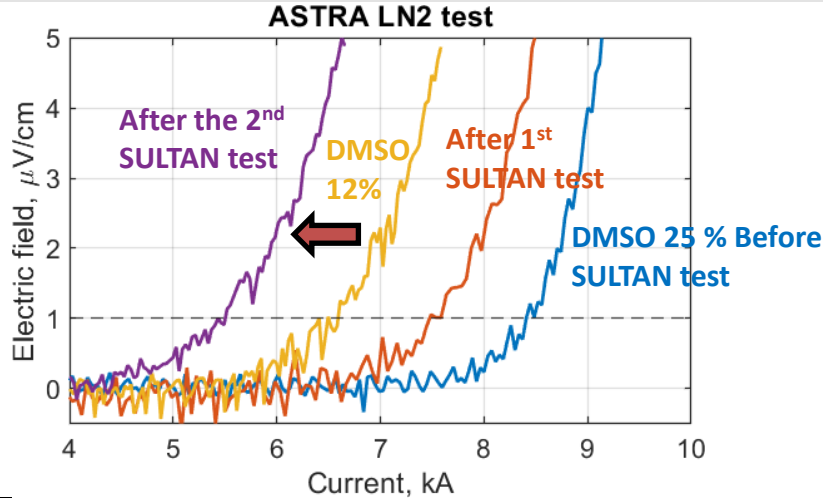
## Aligned Stacks Transposed in Roebel Arrangement (ASTRA)



- 3.3 mm SST tapes, 21-tape **soldered stacks**
- 6 **transposed** strands ( $L \sim 0.75$  m)  $\rightarrow$  reduce AC losses
- Aqueous DMSO (Dimethyl Sulfoxide) **impregnation** (for mechanical support)
- **Tight cooling channel**  $\rightarrow$  conduction cooling
- Operation in **parallel background magnetic field**  $\rightarrow$  reduce # tapes



# ASTRA Conductor prototype: test results

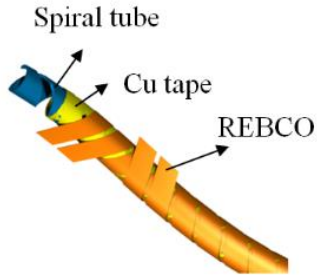


- Initial DC performance in-line with expectations both from LN2 bath and SULTAN testing.
- Strong performance reduction by EM load (at 9 T, 63 kA  $\sim 570$  kN/m) and thermal stresses by frozen aqueous DMSO due to its thermal expansion
- Voids in soldered stack might be the root cause, thus strand manufacturing is being revised trying either to improve soldering or avoid using it (using BRAST strands).

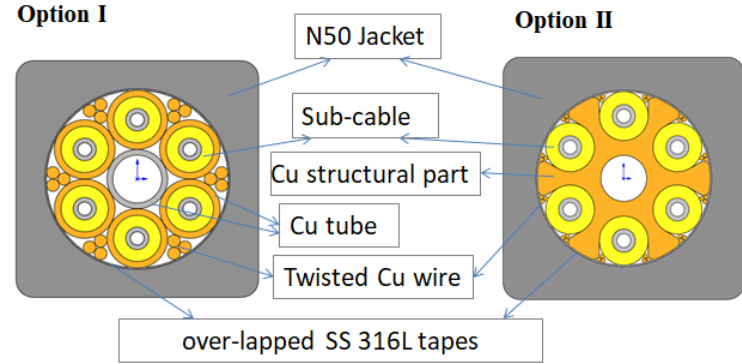
# ASIPP CICC specimen tested at Sultan



## ◆ HTS CICC under developing at ASIPP (Design and manufactured at ASIPP)



CORC®-like sub-cable concept and cabling



Item	Parameter
Tape No.	210
Cable OD	31.75±0.15mm
Twist Pitch	500±50 mm
Conductor OD	41.1±0.15mm
Conductor length	2.77 m

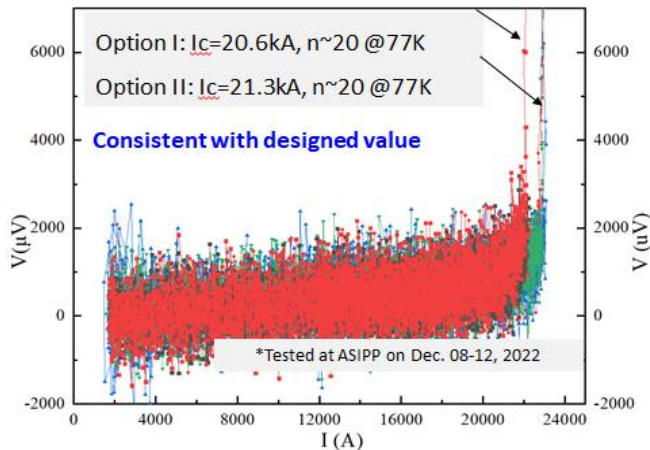




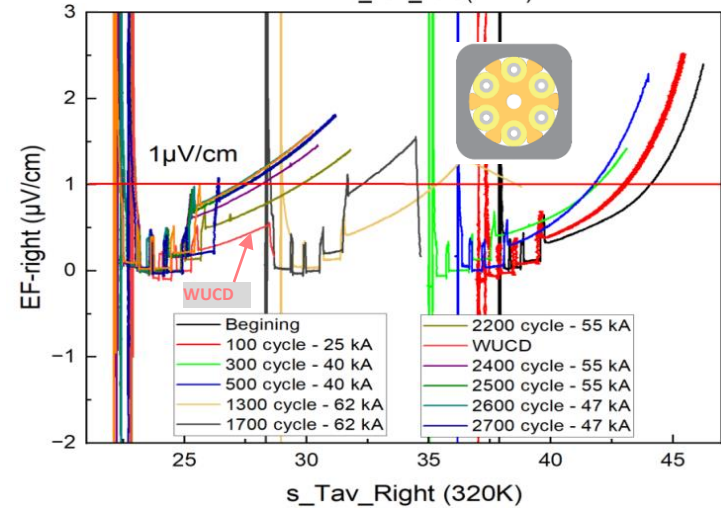
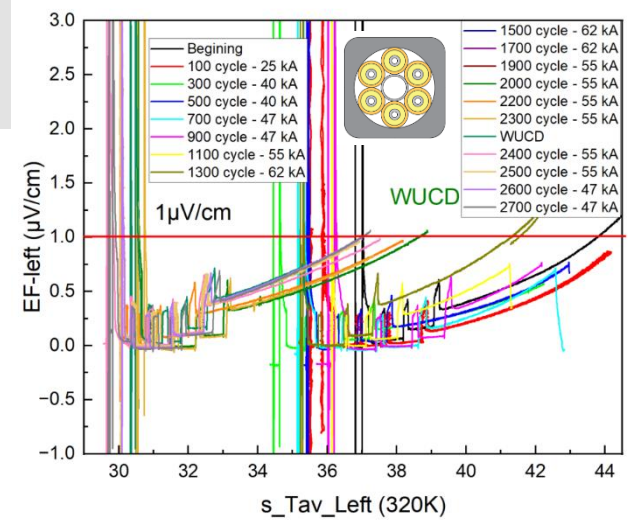


# DC test results of ASIPP sample

- Critical current are around 21 kA @77 K self-field (Tested at ASIPP);
- the predicted Tcs at 25kA, 10.8T is around 43K.
- Totally 2700 EM cycle with current from 25 kA to 62 kA @ 10.8T were carried out;
- The sample shows stable performance with EM cycling when the current  $\leq 47$ kA (option I) and 25 kA (option II). Progressive degradation is observed for higher currents;

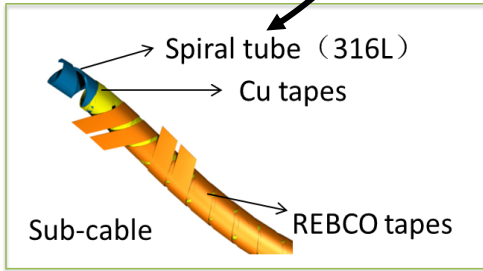
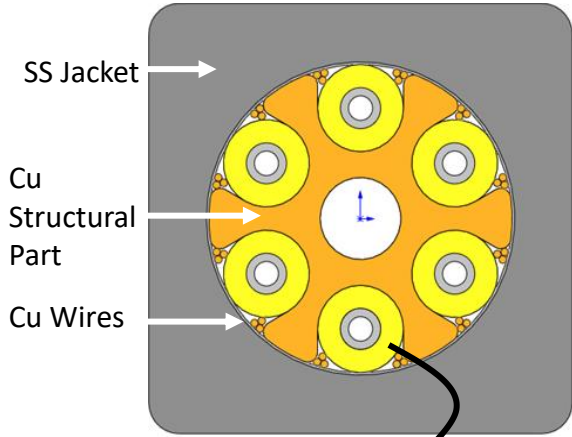


Courtesy of Qin





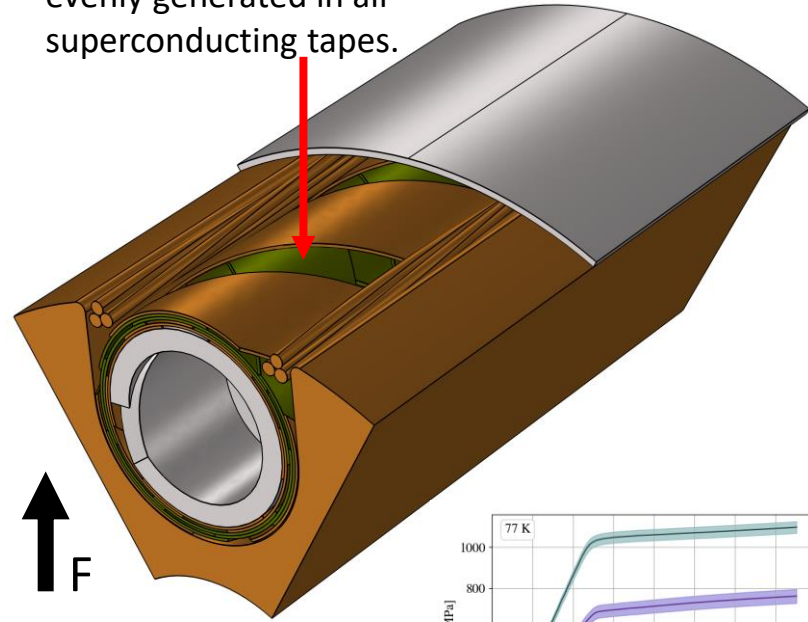
# Twente CICC Model of ASIPP sample



Sub-cable parameters	
Tape manufacturer	Fujikura
# SC Tapes	36
# Cu Tapes	7
# Layers	16 (3 Cu)
# Simulated Layers	3 (3 Cu)
Tape width	4 [mm]
Tape thickness	110 [ $\mu\text{m}$ ]
Substrate thickness	50 [ $\mu\text{m}$ ]
Copper thickness	23 [ $\mu\text{m}$ ]
Spacing	1.3/1.6 [mm]
Core	SS Spiral
Spiral Thickness	0.8 [mm]
Strain window	[-1.3 %, 0.29 %]

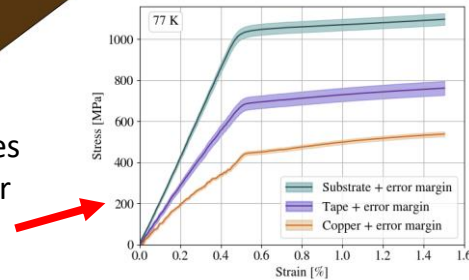
**EM load is equal to nominal one.**

EM-load simulated as body load, evenly generated in all superconducting tapes.



**F**

Axial stress-strain curves measured at Twente for use as model input parameter.



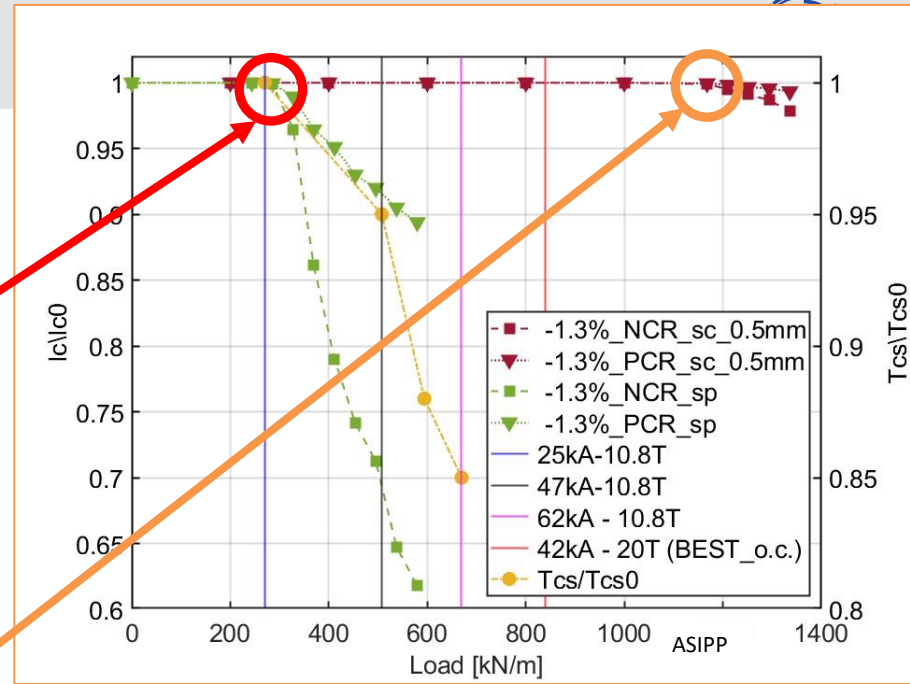
# Model & Sultan sample results

	I [kA]	B [T]	F [kN/m]
SULTAN (max)	100	10.8	1080
BEST CS	42	20	840
EU-DEMO CS	60	18	1080

Irreversibility starts @  $\sim 300$  kN/m (27 kA/10.8 T).  
Model prediction of first damage & SULTAN  $T_{cs}$  reduction coincide.

Damaged volume fraction ReBCO  $\sim 1.5\%$  at  
47 kA / 10.8 T Sultan  $I \times B$  condition.

Proposed optimization:  
Reducing gap from 1 mm to 0.5 mm  
leads to sufficient improvement.



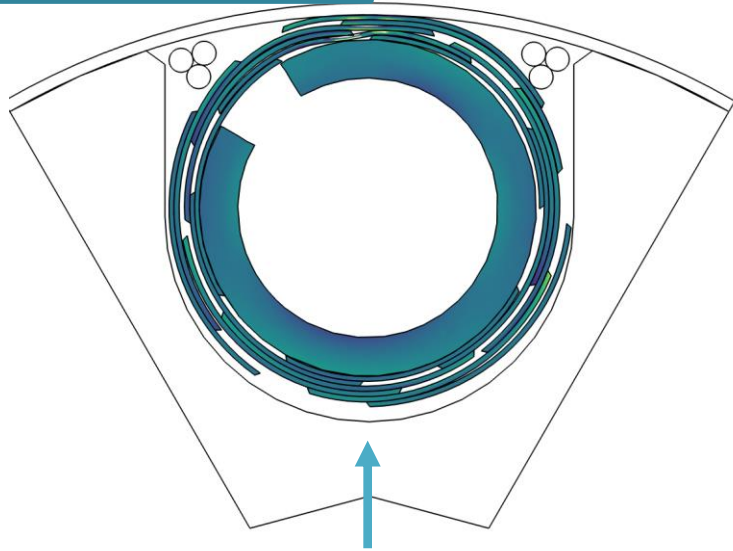
- $_{sp}$  = with spiral and 1 mm tape gap spacing (actual ASIPP sample)
- $_{sc\_0.5mm}$  = with solid core & 0.5 mm tape gap spacing
- NCR = no current sharing between tapes.
- PCR = perfect current sharing between tapes.
- Vertical lines: Sultan testing load levels ( $I \times B$ ).
- ASIPP o.c. = ASIPP CS coil operating condition.

# ASIPP CICC; Gap ~ 1 mm and ~ 0.5 mm

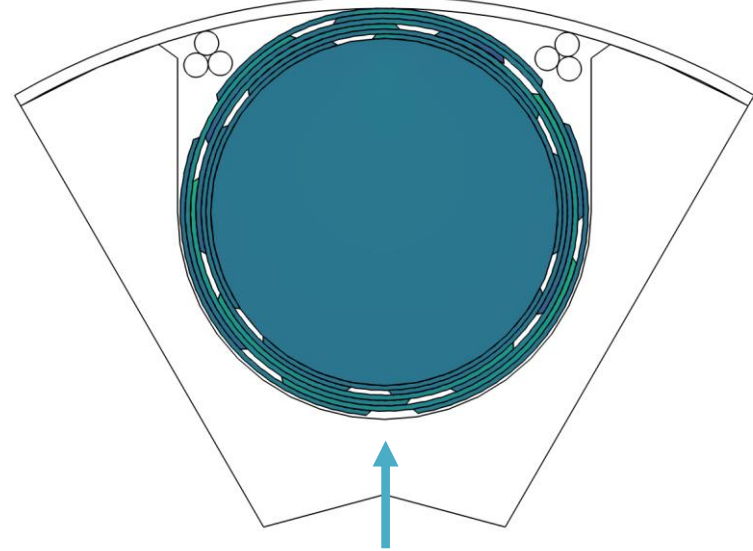
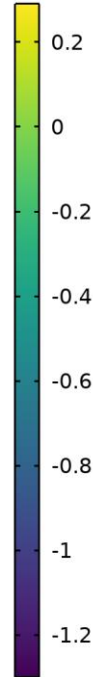


$\uparrow F = F(\text{Sultan})/6$

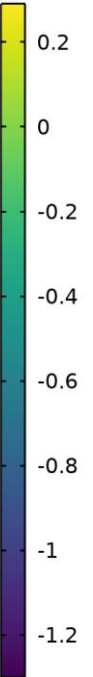
GAP= spiralling spacing between tapes from the same layer



Gap spacing = 1 mm

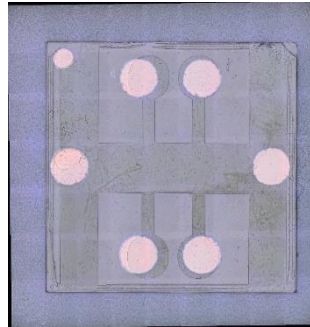
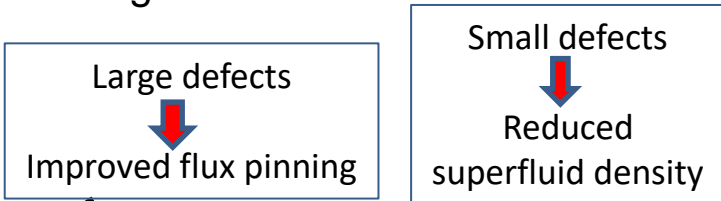


Gap spacing = 0.5 mm

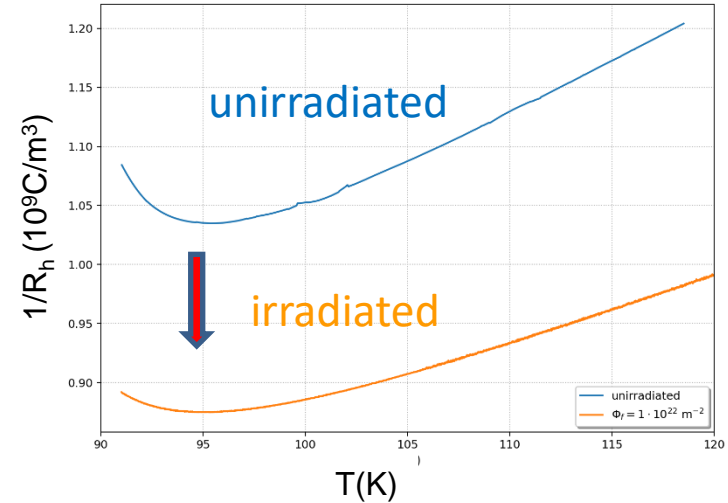
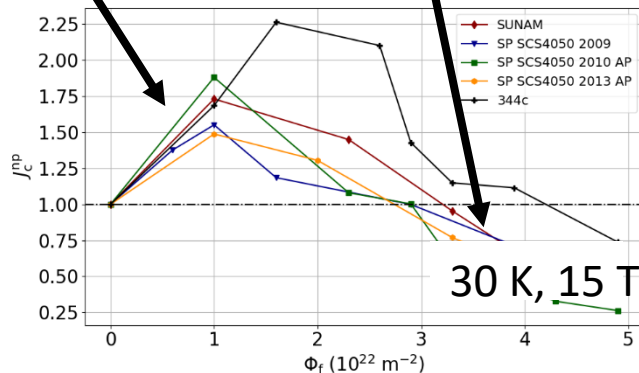


Reducing gap from ~ 1 to ~ 0.5 mm reduces voids and bending and significantly improves performance.

- Irradiation and characterization of coated conductors from commercial suppliers (SuNAM, SuperOx, SuperPower, Theva, D-nano)
- Understanding the reasons for the degradation at high fluences



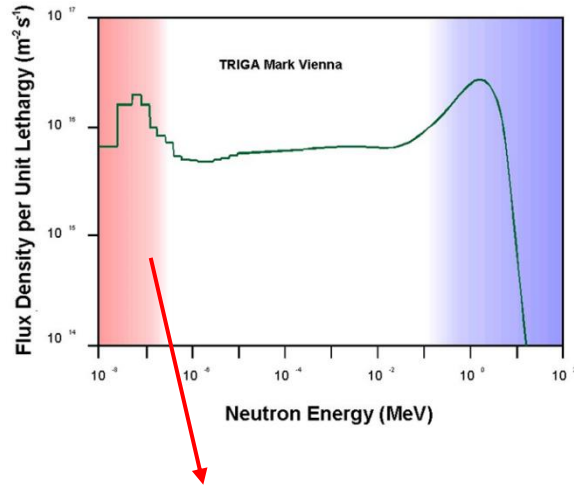
1  $\mu\text{m}$  YBCO (PLD)  
on 10mm x 10mm  
MgO substrate



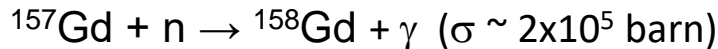
Hall resistivity is indirectly proportional to charge carrier density.

**Irradiated samples have reduced # of charge carrier  $\rightarrow$  Reduced Superfluid density**

## Understanding the reasons for the degradation at high fluences: Role of small defects

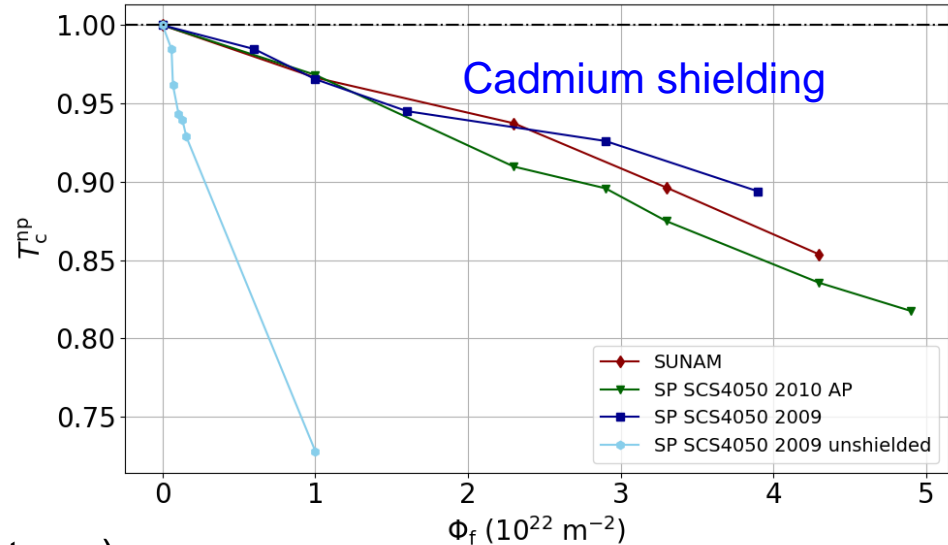


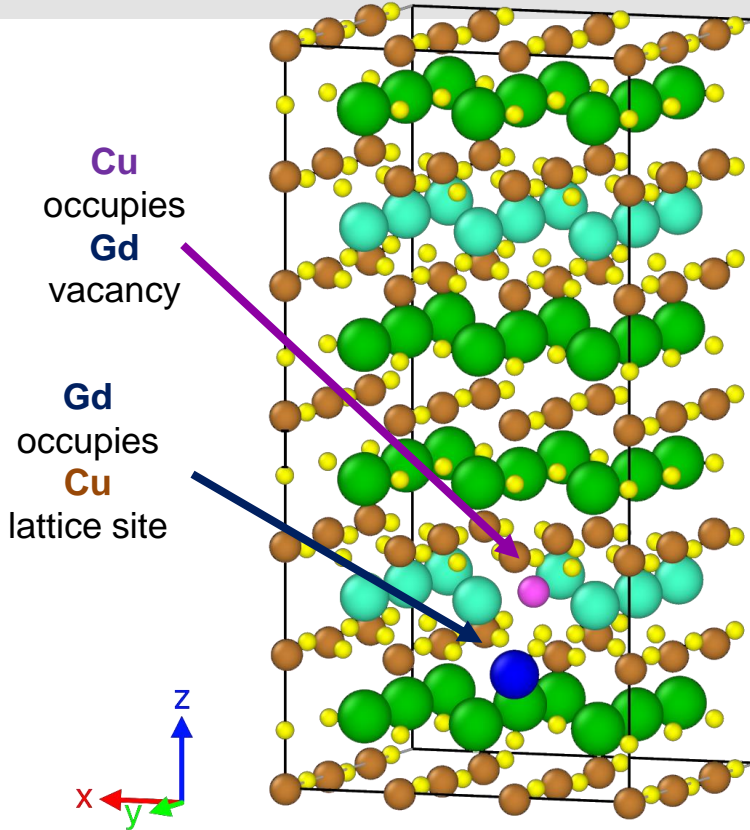
Neutron capture reactions (low energy neutrons)



Recoil energy:  $\sim 30 \text{ eV} \rightarrow$  single displaced atom

### Why are these defects so efficient in degrading the superconductor?





- Picture shows one of the potential defects
- Distortion in the **Oxygen** lattice very localized
- Very stable distortions of the lattice

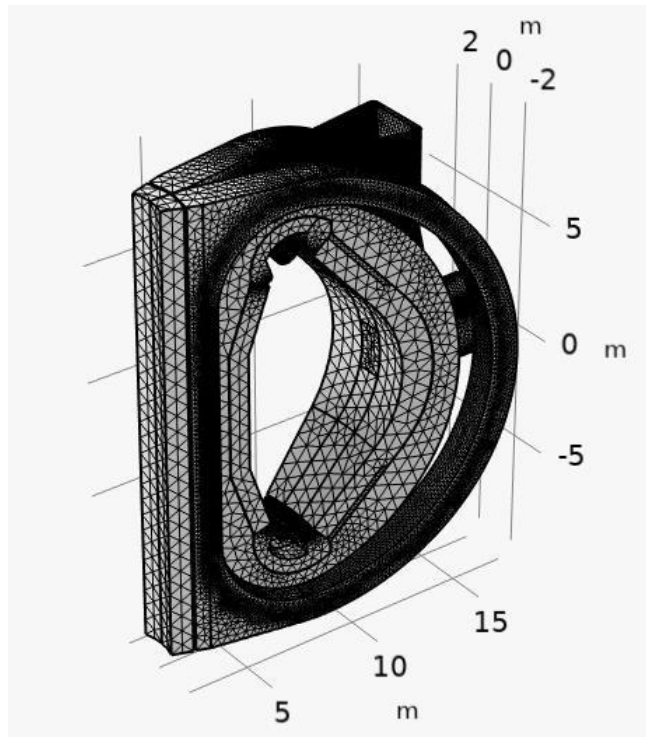
Collaboration with  
Davide Gambino (Linköping University)  
Francesco Laviano and Daniele Torsello  
(Politecnico of Turin)

*See the presentation of Raphael Unterrainer on  
Wednesday h. 9:00.*

Defects in the Cu-O planes!



- Monte Carlo calculations of neutron fluxes and spectra on SC cables of TF coils for **DEMO design**



- Detailed estimation of dpa in TF coils and also in HTS of CS coils will give an updated picture

reactor	total flux at TFC ( $\text{cm}^{-2}\text{s}^{-1}$ )	nuclear power at TFC	dpa at 10 Full Power Year
DEMO [1]	$5 \cdot 10^9$	$80 \text{ W/m}^3$	$3 \cdot 10^{-4}$
ARC-like [2]	$1.28 \cdot 10^{13}$	$32 \text{ kW/m}^3$	0.22

[1] P. Pereslavitsev et al., Fusion Engineering and Design 89 (2014) 1979–1983

[2] F. Ledda et al., submitted



Fast neutrons	Energy (0.1 MeV, 20 MeV)	Gradual fluence ( $10^{22} \text{ m}^{-2}$ )				
		Step 1	Step 2	Step 3	Step 4	Step 5
		0.6	0.16	3.0	0.57	1.83

Sample set	Cumulative fluence ( $10^{22} \text{ m}^{-2}$ )				
	Step1	Step2	Step3	Step4	Step5
1	0.6	0.76	3.76	4.33	6.16
2	n.a.	n.a.	3.0	3.57	5.4
3	n.a.	n.a.	n.a.	0.57	2.4

The last irradiation was done in another channel of the reactor, closer to the neutron source, at much higher irradiation speed (about 20 times)

→ Intense irradiation heating by neutrons and gamma rays

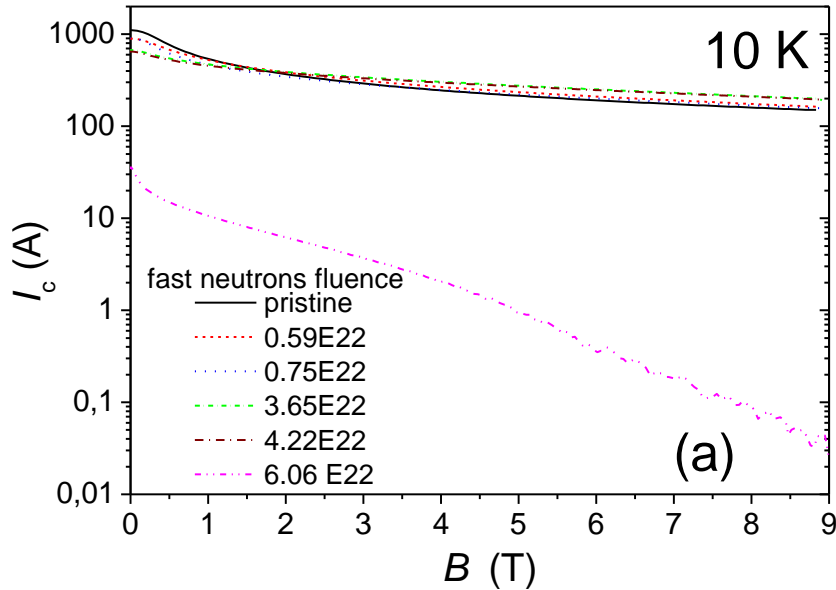
→ Insufficient sample cooling

→ Degradation of HTS tapes due to overheating

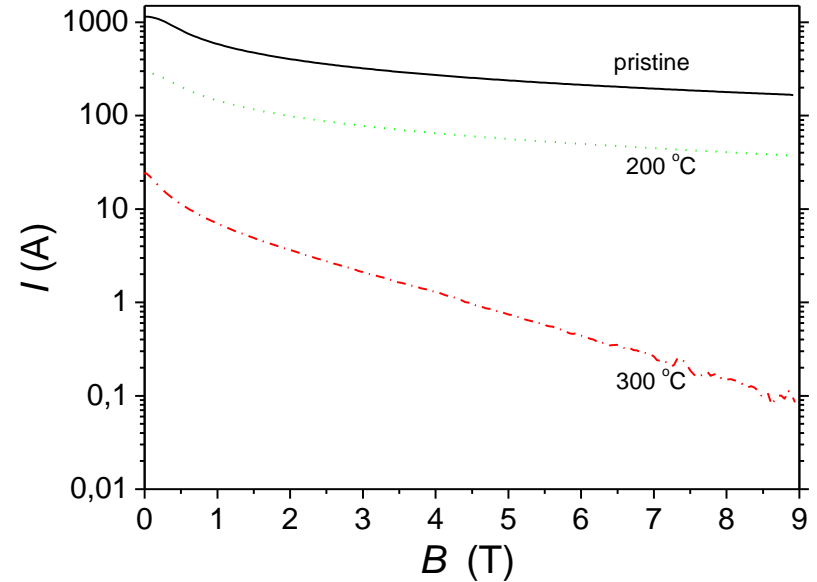


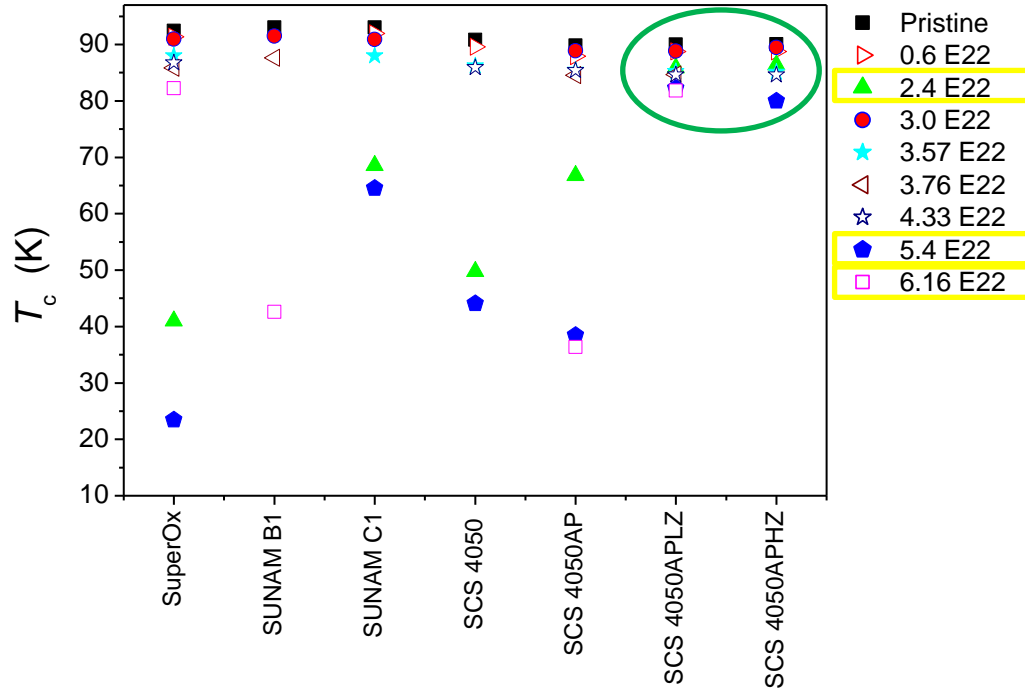
## Modelling the effect of samples overheating by annealing samples at high temperatures

SuperOx 1



SuperOx annealed in Ar





1. Limiting temperature of the tape handling is about 200 °C.
2. The tapes doped by Zr possess much higher thermal stability than others. It originates from a more stable crystalline structure of ZrBO<sub>3</sub> (TEM).
3. For further irradiation experiments, the thermal contact of samples with the glass envelope cooled from outside to 55 °C must be improved.



- ❑ All HTS conductor prototypes have initial performances in line with expectations
- ❑ The degradation of the performances of HTS full-scale conductors with electromagnetic cycles requires improved technical solutions
- ❑ Irradiation experiments indicate that:
  - 1) degradation at high fluences are due to small defects that reduce superfluid density
  - 2) Intense Irradiation heating, causing a sample overheating above 200 °C, can degrade the HTS tapes (but Zr-doped samples are more robust)



Thanks for your attention