

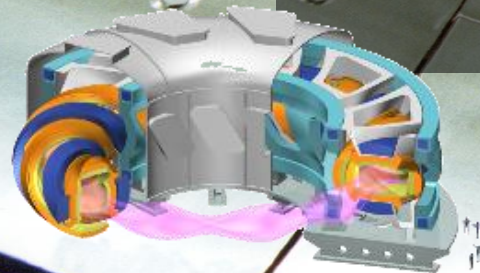
Progress of HTS STARS Conductor Development for the Next-Generation Helical Fusion Experimental Device

N. Yanagi¹, Y. Terazaki¹, Y. Narushima¹, N. Hirano¹, Y. Onodera¹,
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K. Takahata¹, D. Garfias²,
S. Ito³, H. Hashizume³

¹ National Institute for Fusion Science

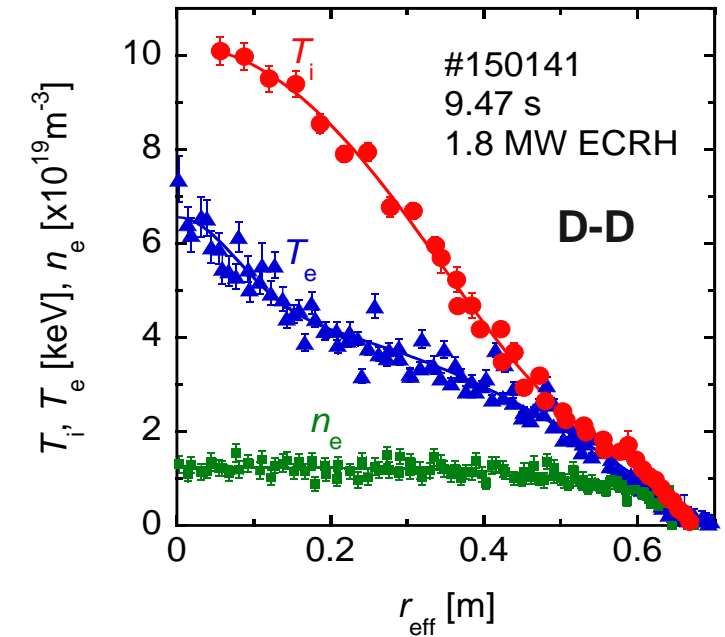
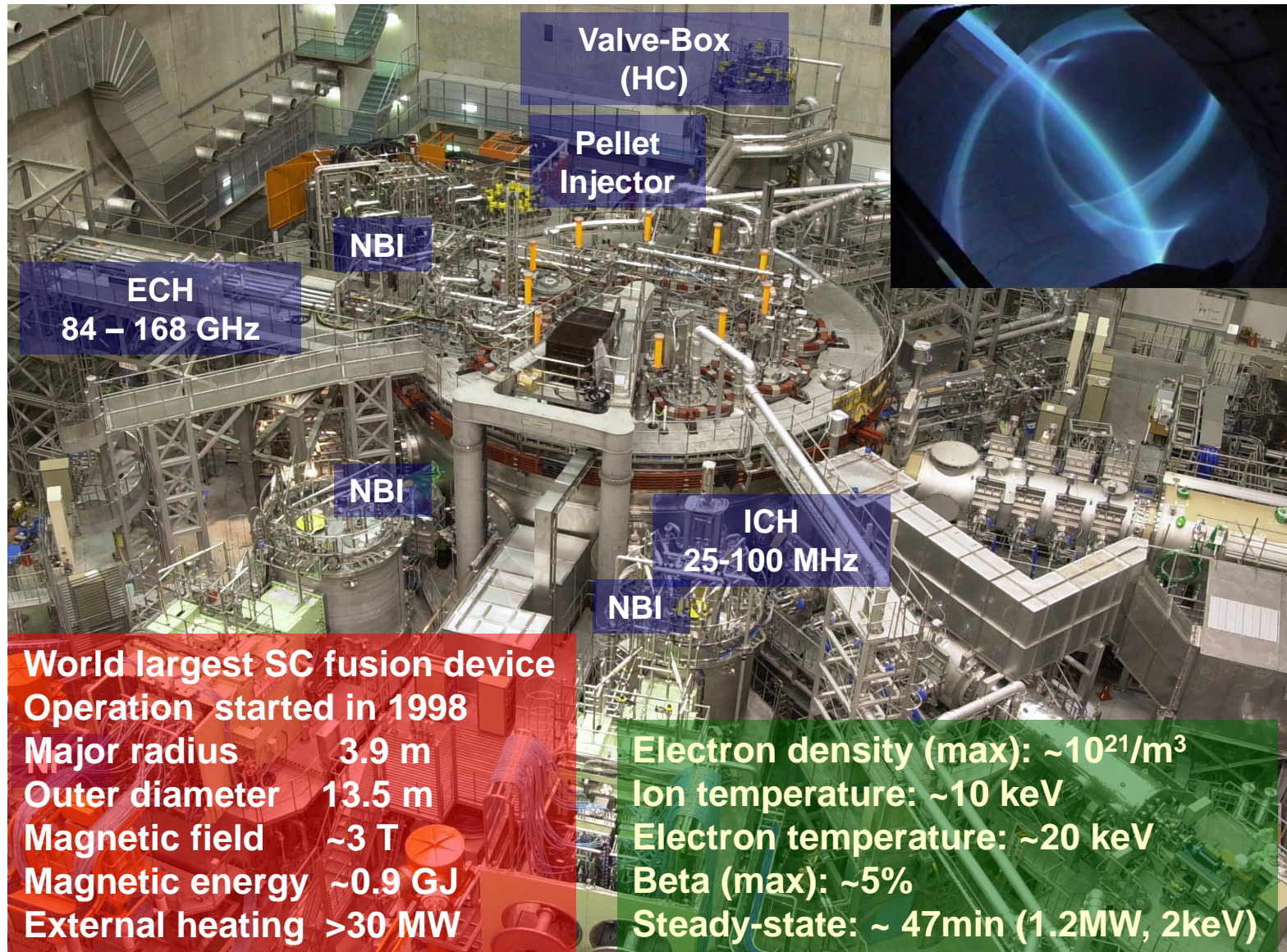
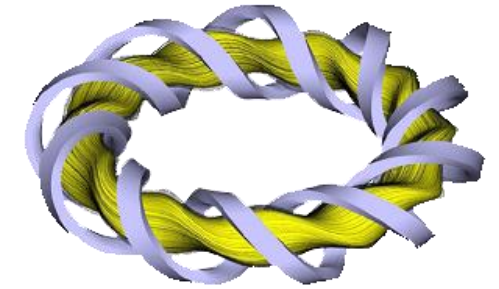
² The Graduate University for Advanced Studies, SOKENDAI

³ Tohoku University



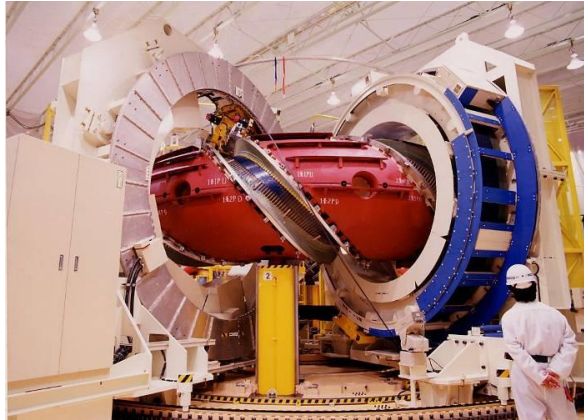
The Virtual CCA 2021
HF-4

The Large Helical Device (LHD)

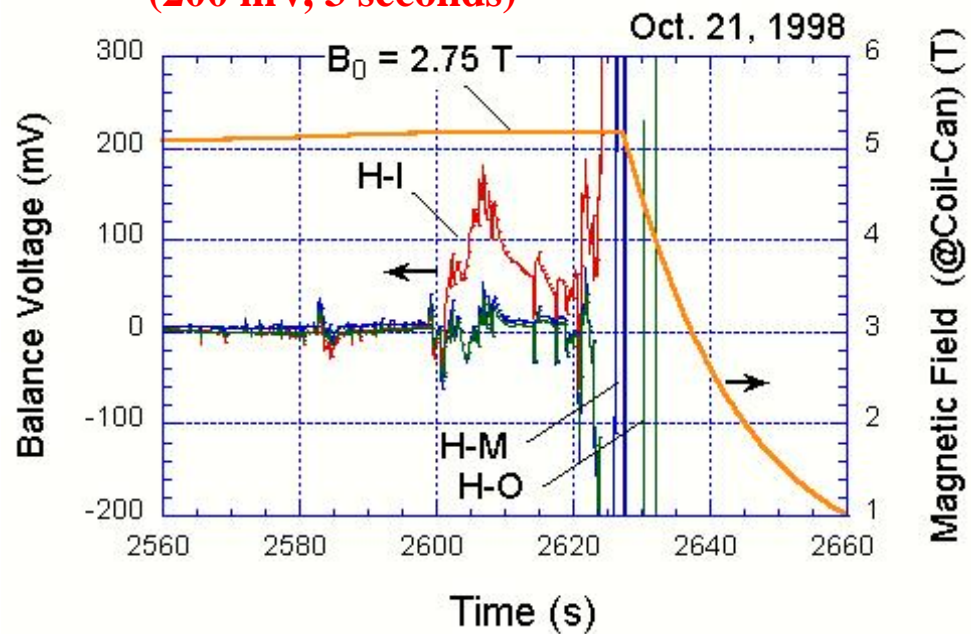


Quench Event in LHD

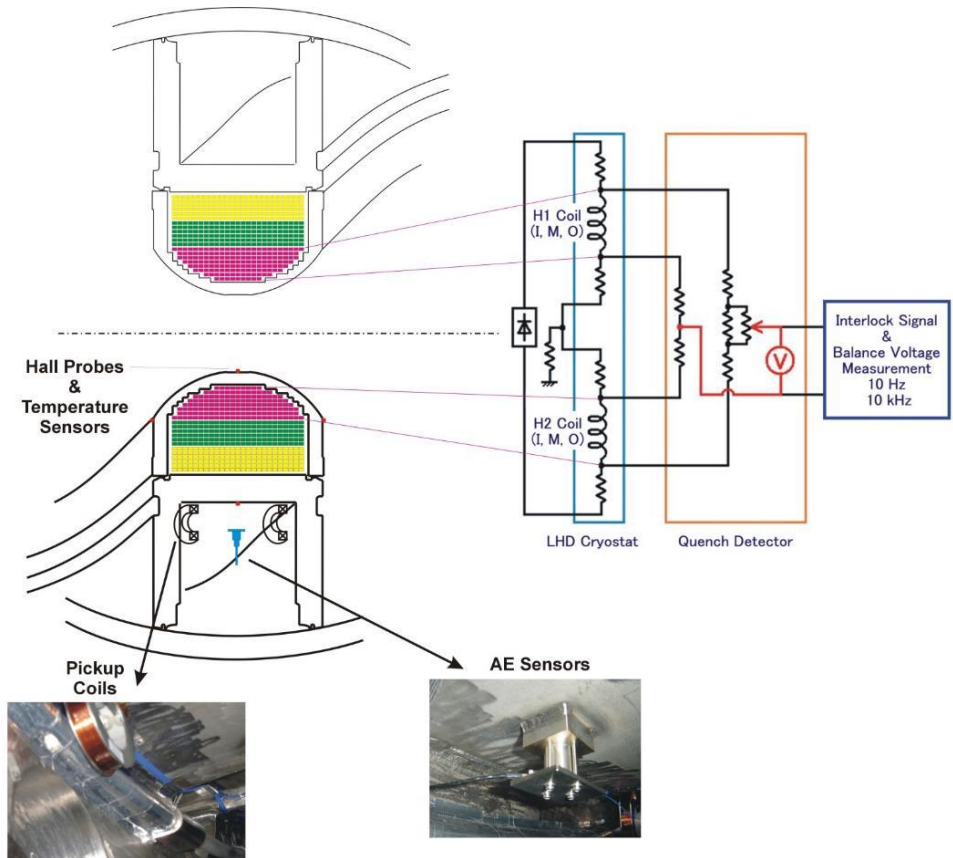
October 21, 1998



Quench Detection (200 mV, 3 seconds)



N. Yanagi, S. Imagawa, et al.,
 IEEE TAS 10 (2000) 610





25 Years of Design Studies on the LHD-type Helical Fusion Reactor, FFHR

Magnet

- Joint-winding by HTS conductor is possible in addition to continuous helical winding (LHD method)

Plasma

- Steady-state w/o. plasma current
- No disruption

Blanket

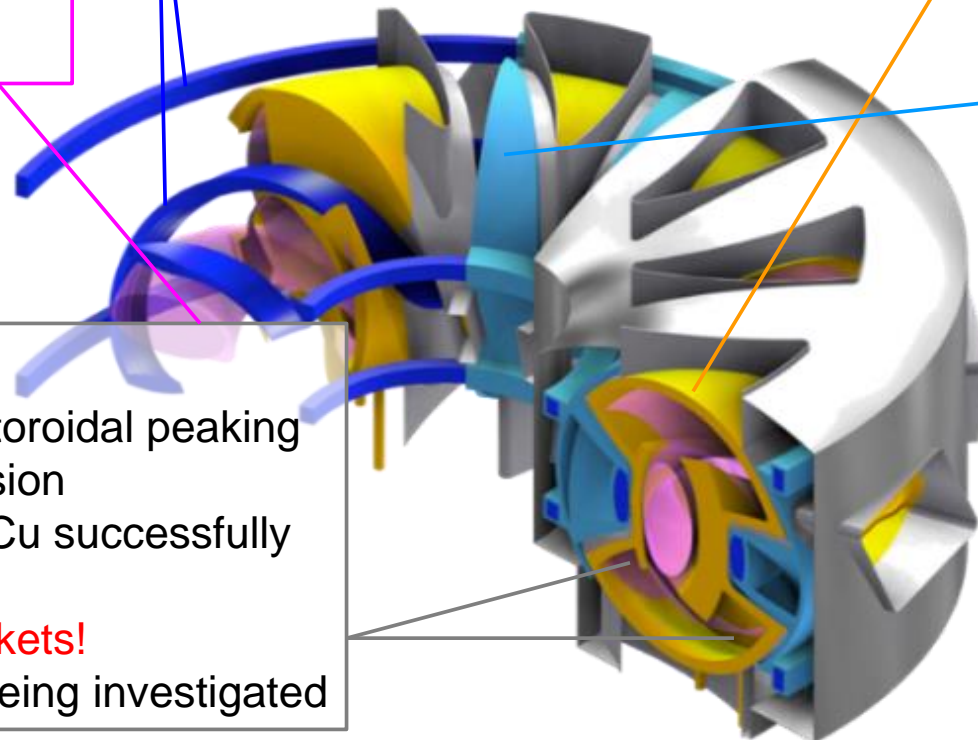
- Molten-salt and/or liquid metal blankets
- RAFM and/or Vanadium alloy
- Easy maintenance through large ports
 - Cartridge-type with external handling
 - Helically-shaped with remote handling

EM Support Structure

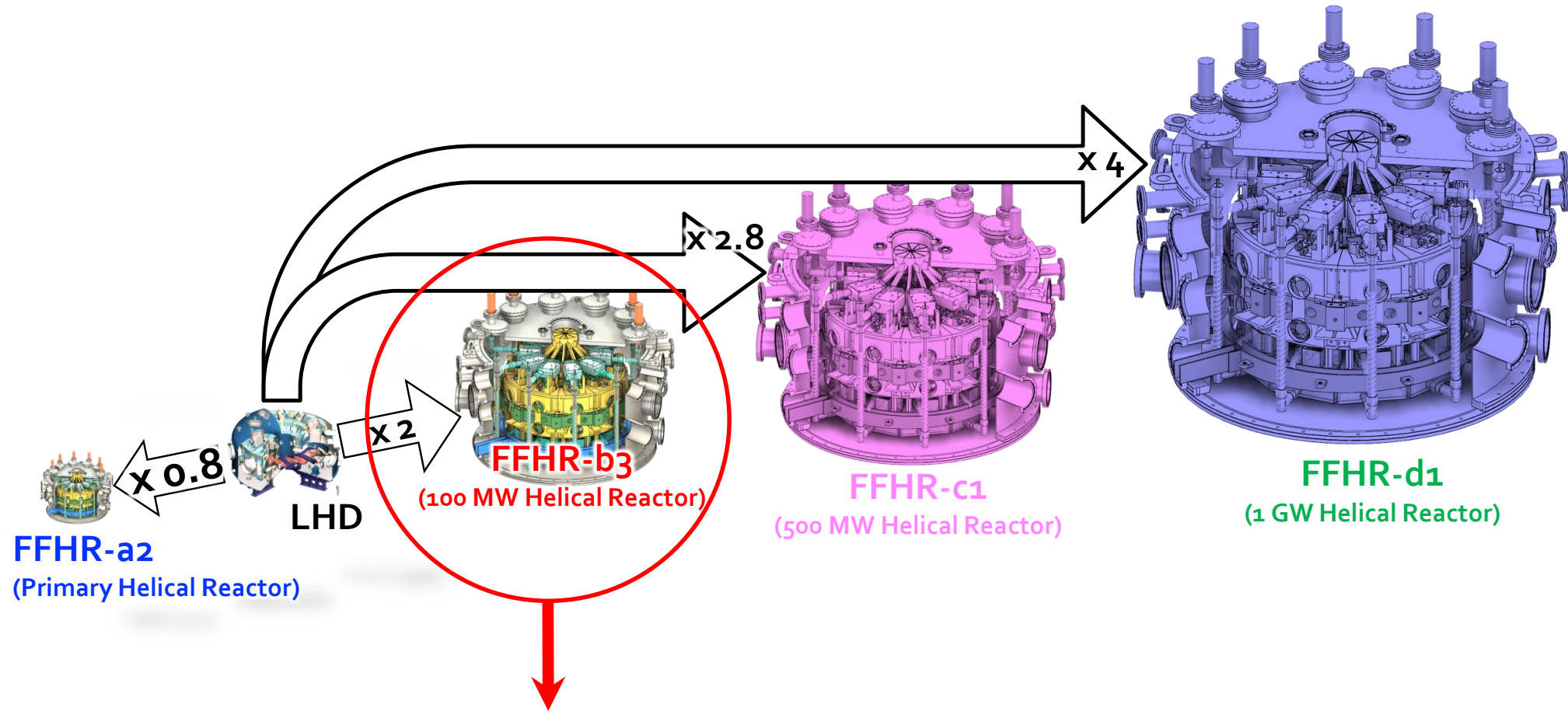
- Topology optimization reduces mass >25%

Divertor

- Large wetted area with reduced toroidal peaking <math><30 \text{ MW/m}^2</math> w/o radiation dispersion
- Advanced Brazing of W & ODS-Cu successfully achieved >math>30 \text{ MW/m}^2</math>
- **Divertors are placed behind blankets!**
- Pebble divertor concept is also being investigated



New Strategy for Early Realization of Helical Reactor



Slight improvement of plasma confinement / Innovation for reactor engineering

→ Early realization of a helical reactor with

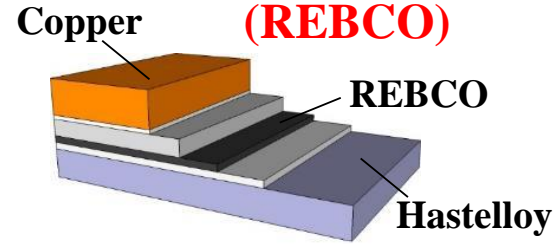
- **Double size of LHD ($R = 7.8$ m)**
- **100 MW net electricity production**

High-Temperature Superconducting Magnet Option

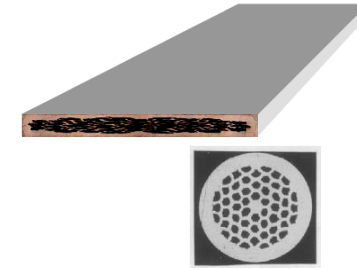
(0) Saving helium resources

- (1) High critical current to high field**
- (2) High cryogenic stability**
- (3) Low cryogenic power**
- (4) High mechanical rigidity**
- (5) Industrial production of tapes**

**Rare-Earth Barium
Copper Oxide
(REBCO)**



Bismuth-based HTS



Stability Margin

$$\Delta Q < C_p \rho \Delta T$$

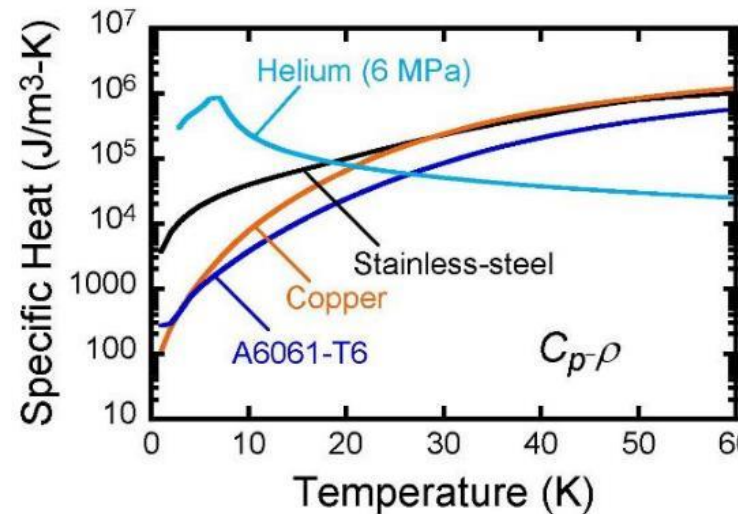
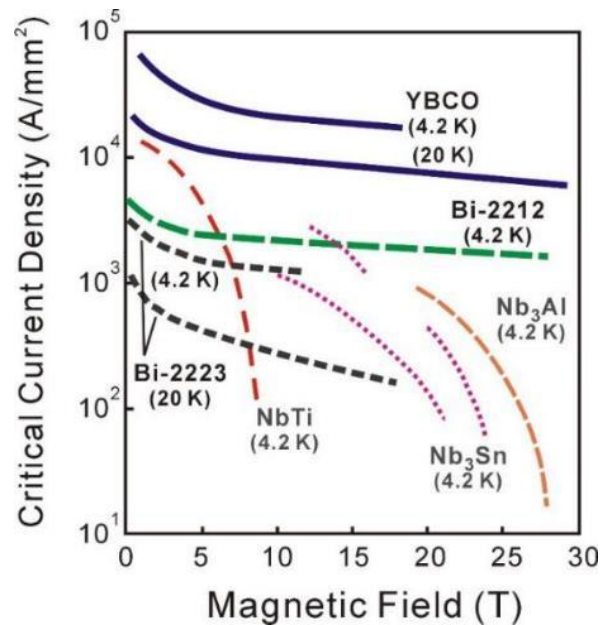
$$C_p \rho \Delta T \approx 2 \times 10^5 \text{ (J/m}^3\text{K)} \times 10 \text{ (K)}$$

$$\approx 2 \text{ (J/cc)}$$

Higher than CIC conductor

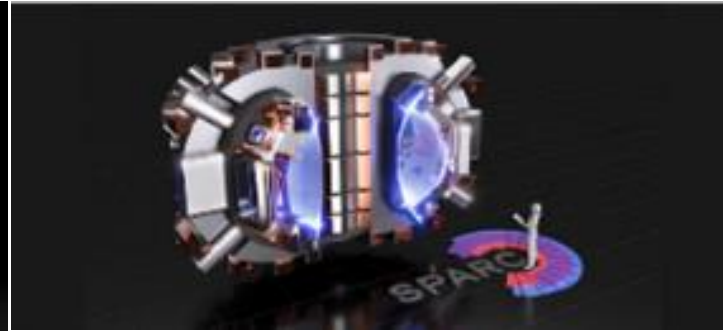
→ Low quench risk!

**N. Yanagi, S. Ito, et al.,
 Plasma and Fusion Research
 9 (2014) 1405013**



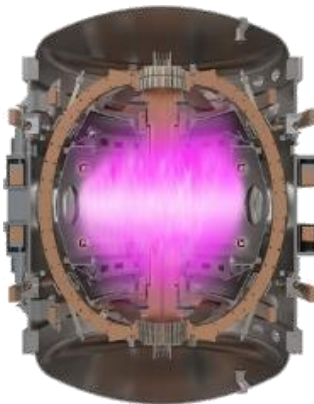
Fusion reactor designs with HTS magnet in the World

ARC & SPARC (MIT/CFS)

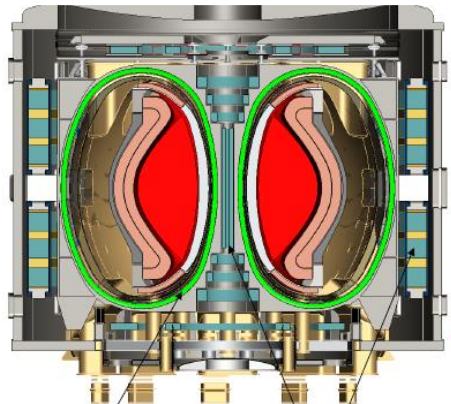


$B_t = 9-12\text{ T}$
 $B_{max} = 21-23\text{ T}$

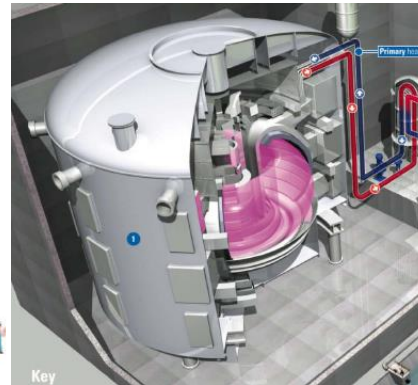
Tokamak Energy



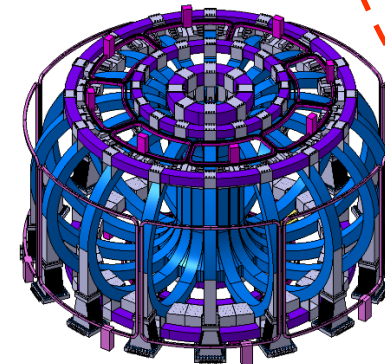
FNSF-ST (PPPL)



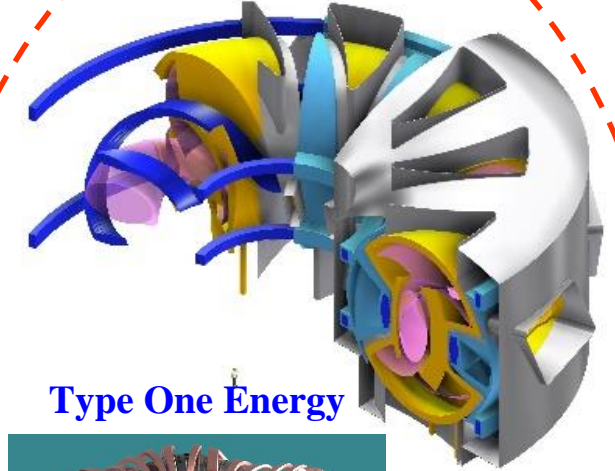
EU DEMO HTS option (EUROfusion)



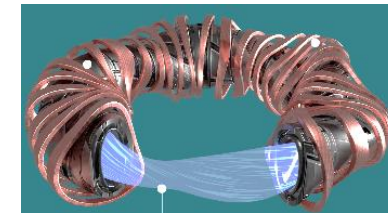
CFETR (ASIPP) for CS coils



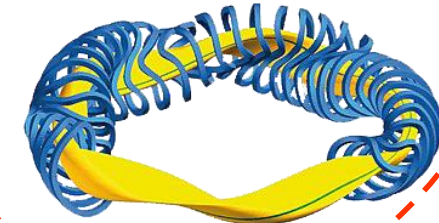
FFHR-d1 (NIFS)



Type One Energy



Renaissance Fusion



Large-current HTS conductors developed for fusion magnets

Twisted and Transposed REBCO Conductors



Simply-Stacked REBCO Conductors

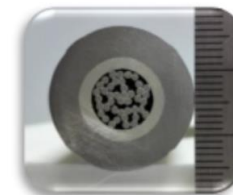


STARS (NIFS)



WISE (NIFS)

Bi-2212 CIC Conductors

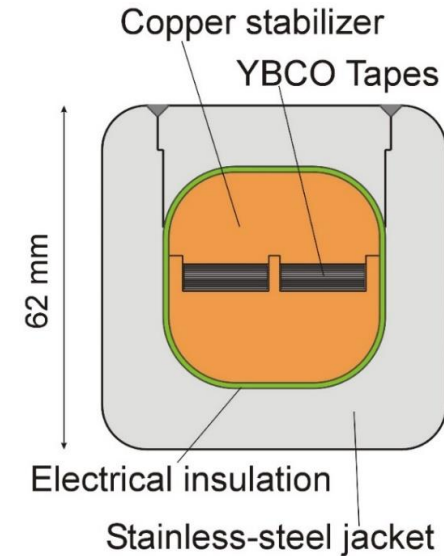


Bi-2212 (ASIPP)

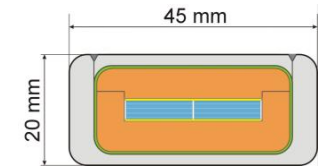
100 kA-class HTS Conductor for FFHR-d1 Helical Fusion Reactor

”STARS” (*Stacked Tapes Assembled in Rigid Structure*)

Operation current	94 kA @12 T
Operation temperature	20 K
Conductor size	62 mm × 62 mm
Current density	24.5 A/mm ²
Number of tapes	40
Cabling method	Simple Stacking
Stabilizer	OFC
Outer jacket	Stainless Steel
Electrical insulation	Organic or Inorganic
Cooling method	GHe / LH ₂
Superconductor	REBCO



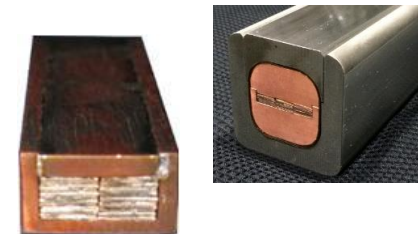
STARS
for FFHR-d1
94 kA, 25 A/mm²



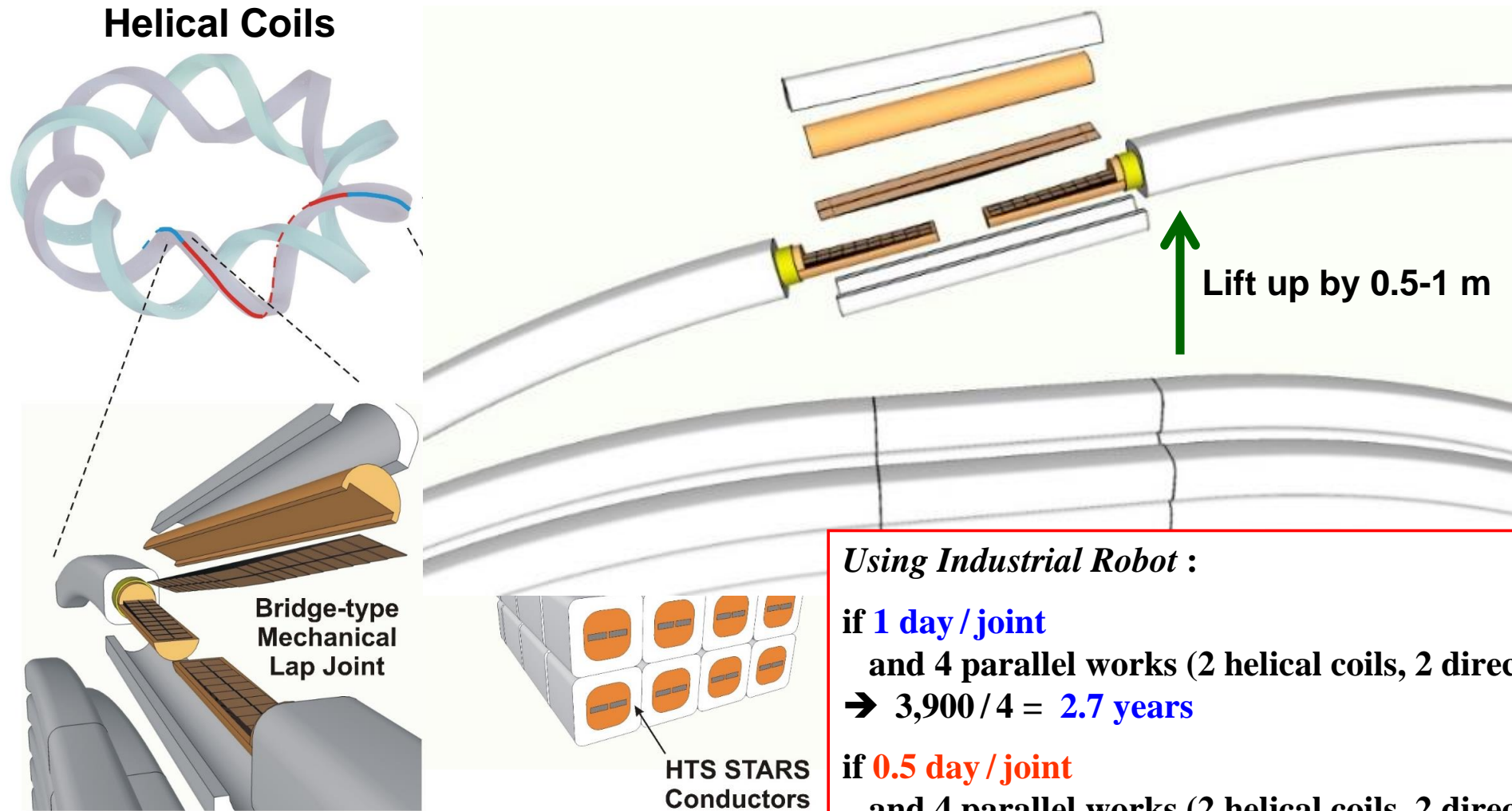
STARS
for FFHR-b3
66 kA, 80 A/mm²

Simply-stacked HTS conductor for DC helical coils

- Non-uniform current distribution may be allowed
- High mechanical strength (no void & no local deformation)
- Low cost / low-resistance joint



“Joint-Winding” of Helical Coils



390 turns × 5 segments × 2 coils
→ 3,900 joints

Using Industrial Robot :

if **1 day / joint**

and 4 parallel works (2 helical coils, 2 directions)

→ $3,900 / 4 = 2.7$ years

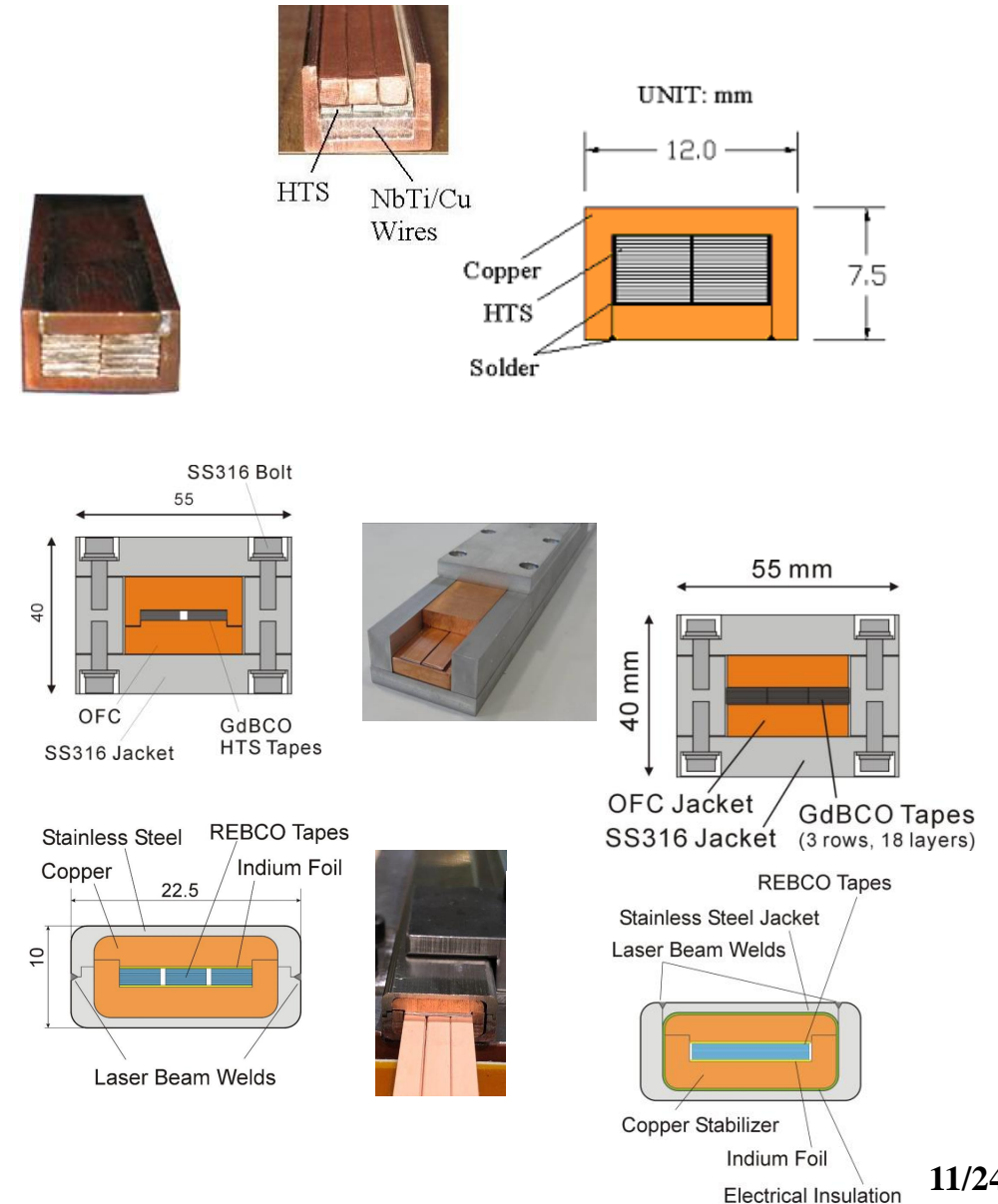
if **0.5 day / joint**

and 4 parallel works (2 helical coils, 2 directions)

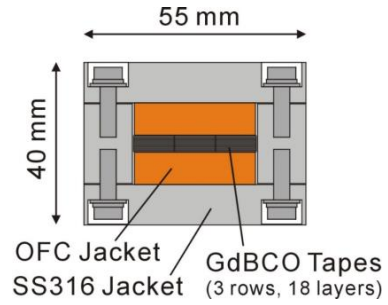
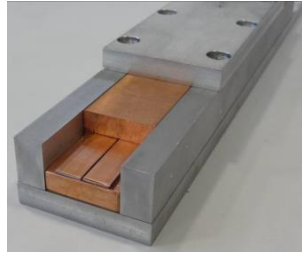
→ $3,900 / 2 / 4 = 1.3$ years

History of HTS STARS Conductor Development at NIFS

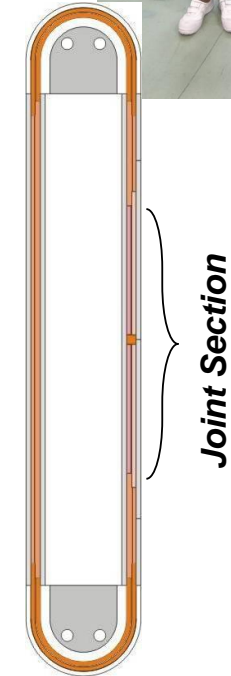
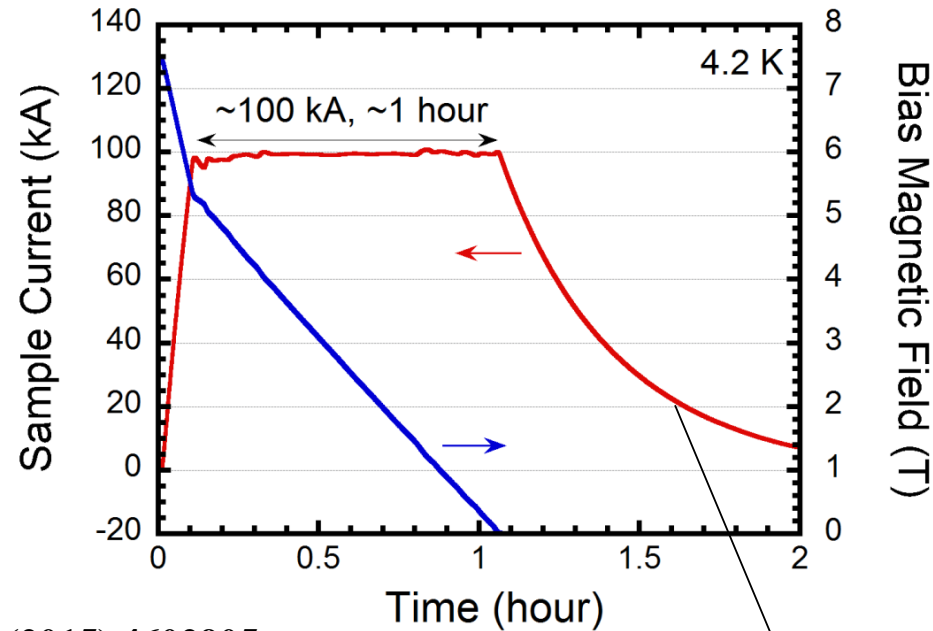
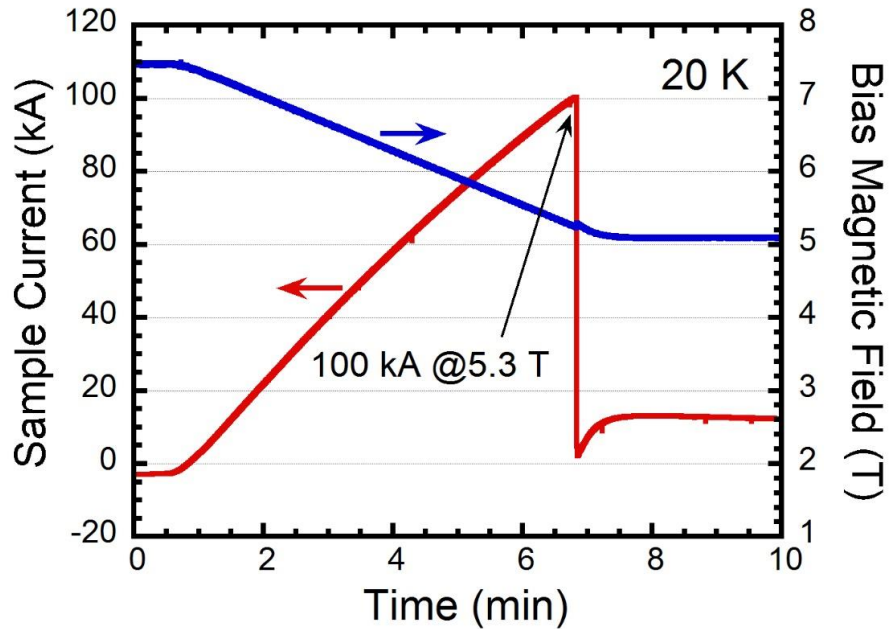
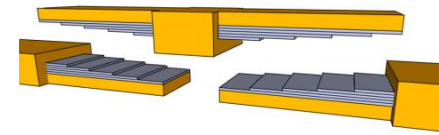
- 2003-2006** **LTS / HTS hybrid conductor sample**
 NbTi + Bi-2223 tapes + Cu (soldered)
- 2006-2007** **10-kA-class HTS STARS conductor sample**
 Bi-2223 tapes + Cu (soldered)
- 2007-2008** **15-kA-class HTS STARS conductor sample**
 YBCO / GdBCO tapes + Cu (soldered)
- 2012-2013** **30-kA-class HTS STARS conductor sample**
 GdBCO tapes + Cu + SS (bolted)
- 2013-2014** **100-kA-class HTS STARS conductor sample**
 GdBCO tapes + Cu + SS (bolted)
- 2019-2020** **20-kA-class HTS STARS conductor sample**
 EuBCO + Cu + SS (welded)
- 2020-2021** **20-kA-class HTS STARS conductor sample**
 GdBCO + Cu + Kapton + SS (welded)



100 kA-Class Prototype STARS Conductor Test



Bridge-type mechanical lap joint
 “Invisible joint”



N. Yanagi et al., Nucl. Fusion 55 (2015) 053021

Y. Terazaki et al., IEEE Trans. Appl. Supercond. 25 (2015) 4602905

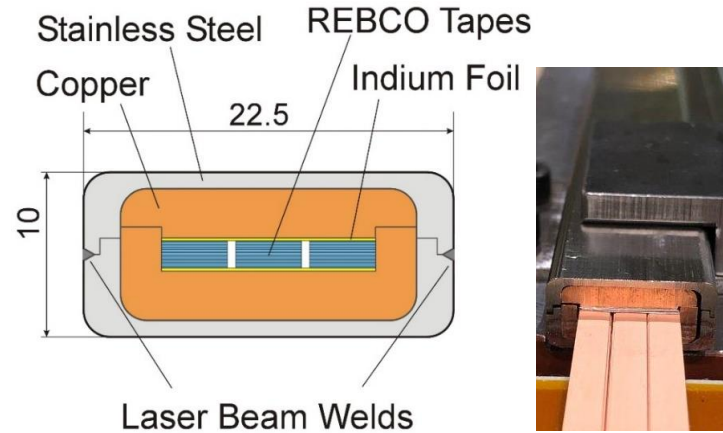
S. Ito et al., IEEE Trans. Appl. Supercond. 25 (2015) 4201205

Joint resistance
 ~1.8 nΩ

Practical HTS conductor development for the next-generation helical device

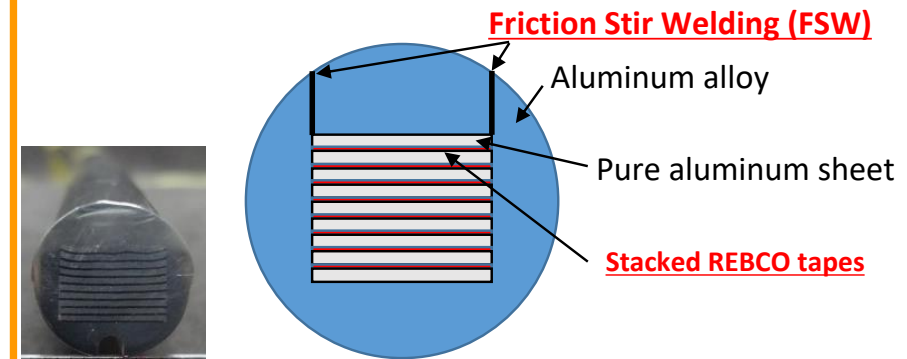
STARS

(Stacked-Tapes Assembled in Rigid Structure)



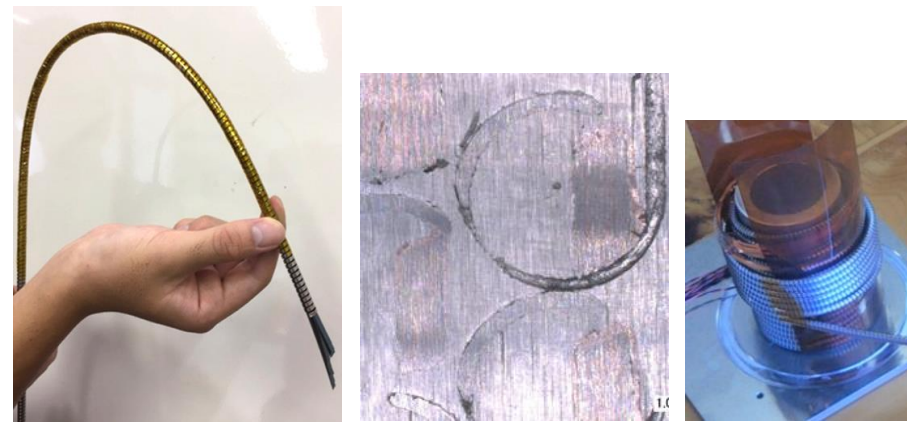
FAIR

(FSW, Al-alloy, Indirect-cooling, REBCO)



WISE

(Wound and Impregnated Stacked Elastic tapes)



- Current capacity: 10-20 kA @ 8 T, 20 K
- Current density: 80 A/mm²

20 kA-class STARS Conductor

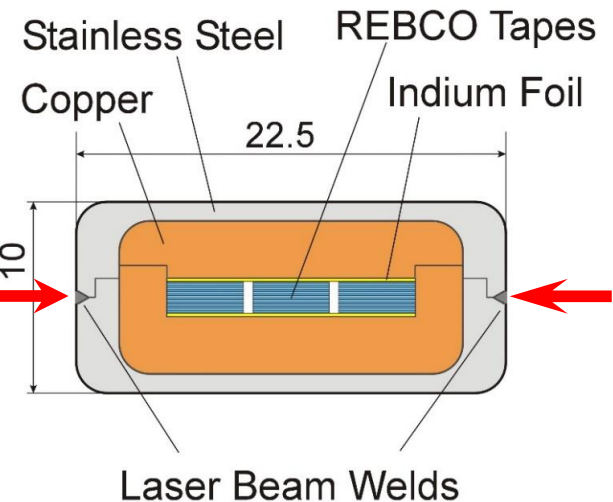
- ◆ HTS (REBCO) tapes (simply stacked) + Copper stabilizer + Stainless steel jacket
 - Suitable for DC magnet, high mechanical strength, low hot-spot temperature, simple joint
- ◆ Development since 2005 for the helical fusion reactor FFHR
- ◆ 10-kA class → 15-kA class → 30-kA class → 100-kA class (prototype samples)
100 kA@5.3 T, 20 K achieved (total length: 3 m, tested region: 0.3 m, bolted jacket)

- Next phase development of 20-kA-class conductor with long length to be applied to the next generation helical device
 - High current density of 80 A/mm² is a big target (former achievement: 25 A/mm²)
- A 3-m-long conductor sample
 - Fabricated by HITACHI Ltd.
 - 45 REBCO tapes (Fujikura FESC-SCH04)
 - Laser beam welding of SS jacket



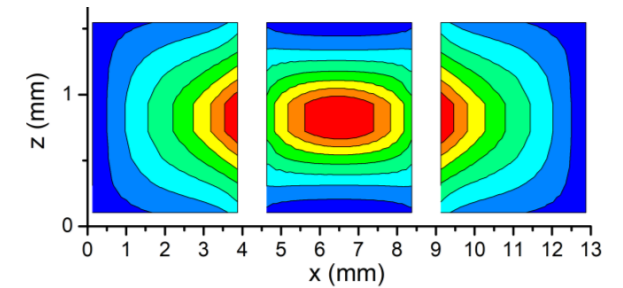
Temperature at the inner wall of Cu stabilizer was **44 °C** << 200 °C (allowable limit for REBCO tapes)

Laser Beam Welding



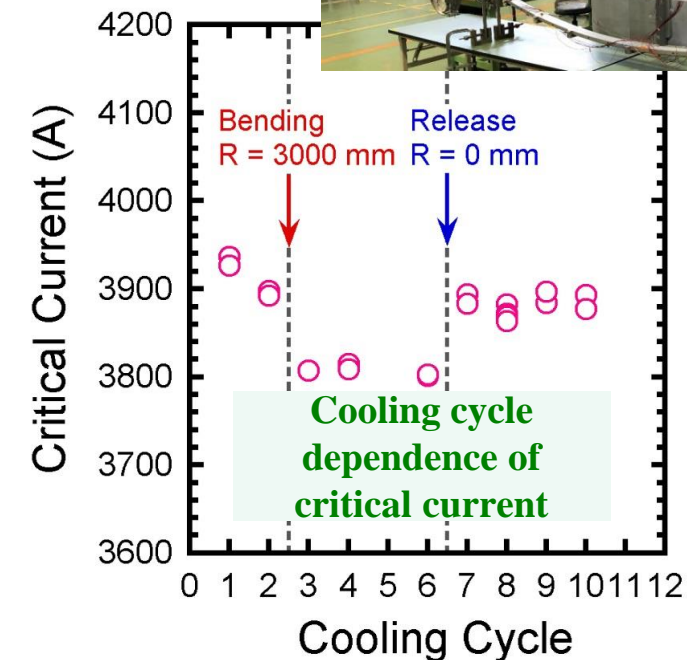
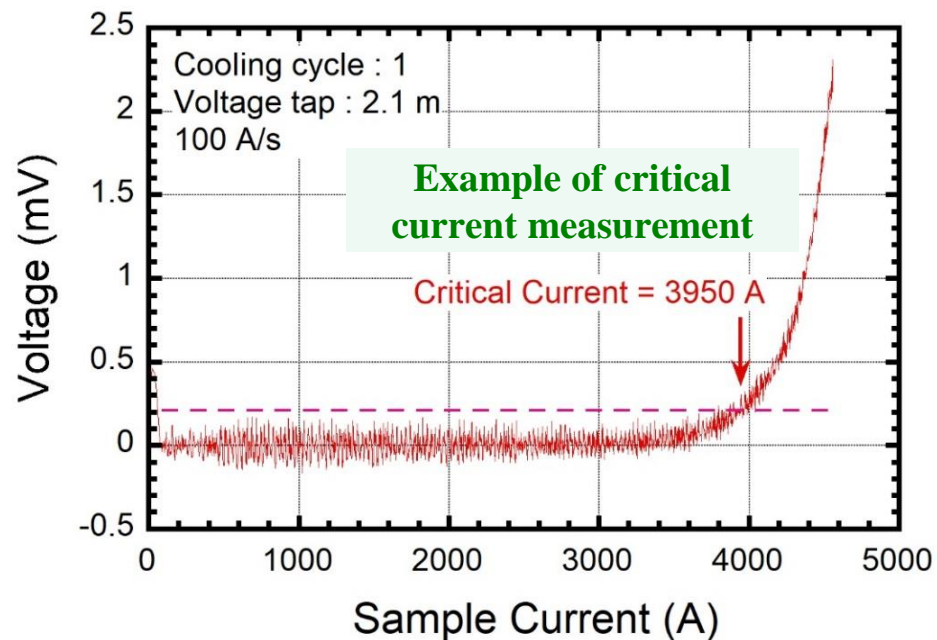
20 kA-class STARS conductor test in liquid nitrogen

- Short sample test in liquid nitrogen (77 K) and no magnetic field
- Critical current of **3,950 A** confirmed
 - Verified by numerical simulation with current density and magnetic field distribution, extrapolation to 20 kA at 20 K and 10 T
- Tolerable reduction (~1%) of critical current by cooling cycle
- Further reduction (~2%) with 3000 mm bending radius
- Recovery by releasing (straightening)
- ◆ Test in 4-50 K by helium cooling and <9 T magnetic field is planned



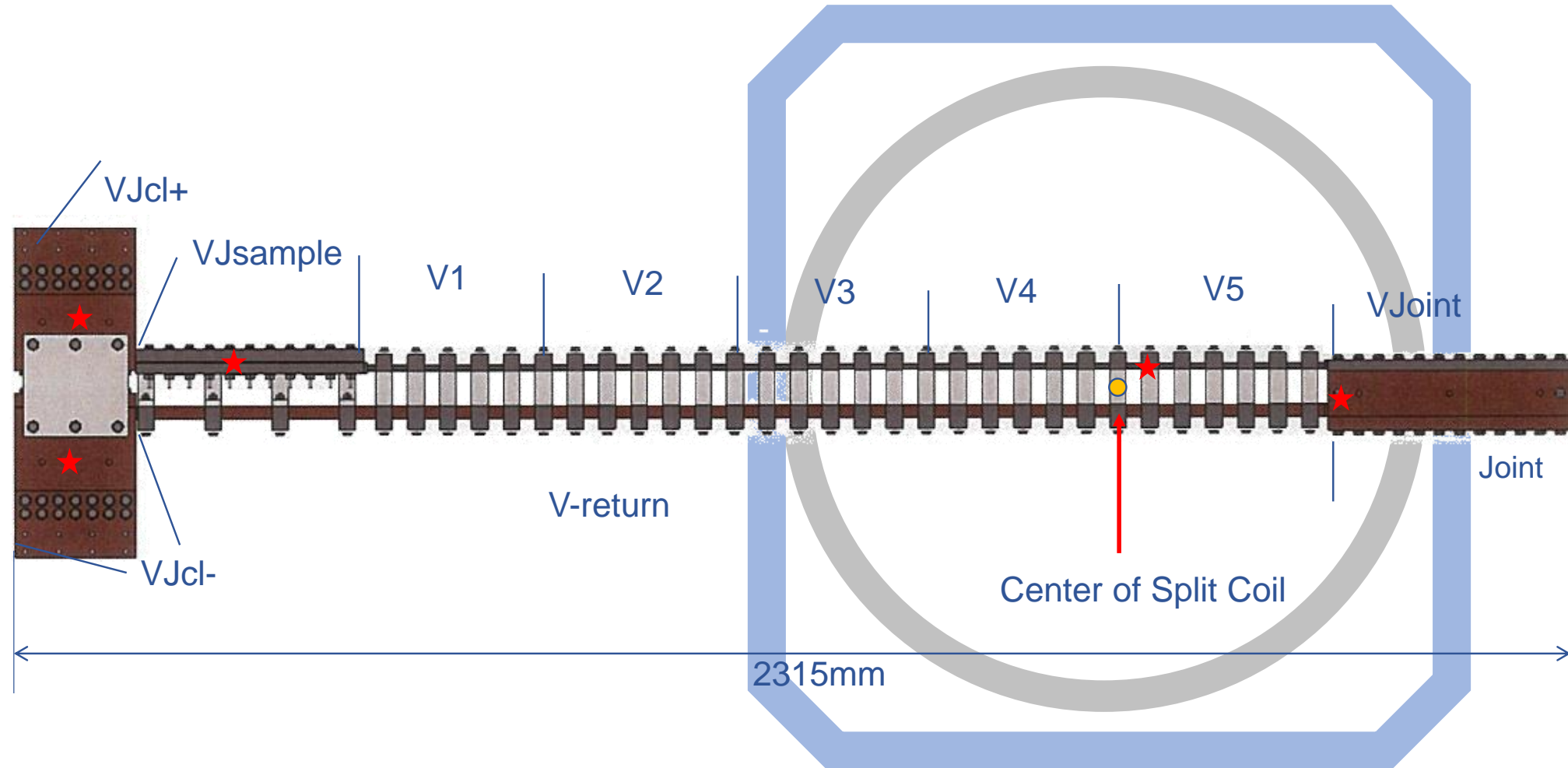
Numerical simulation of J and B distribution

Y. Terazaki



20 kA-class STARS conductor test in large-superconductor testing facility

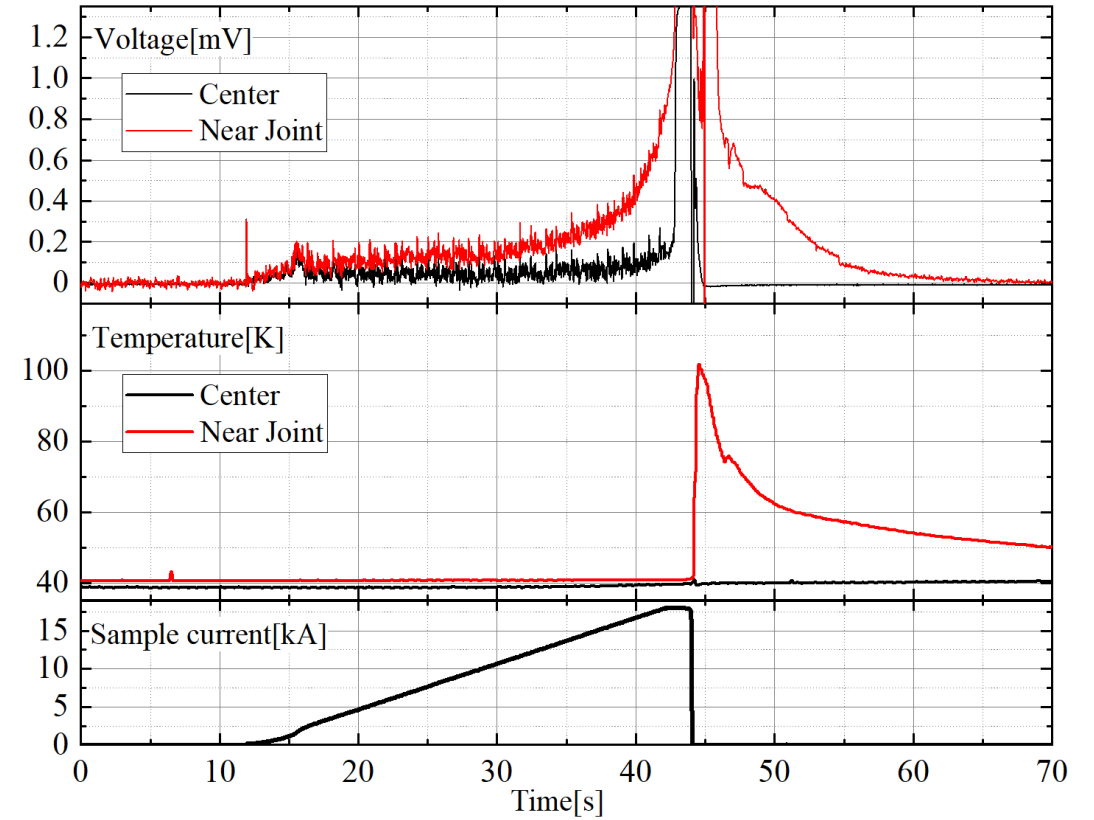
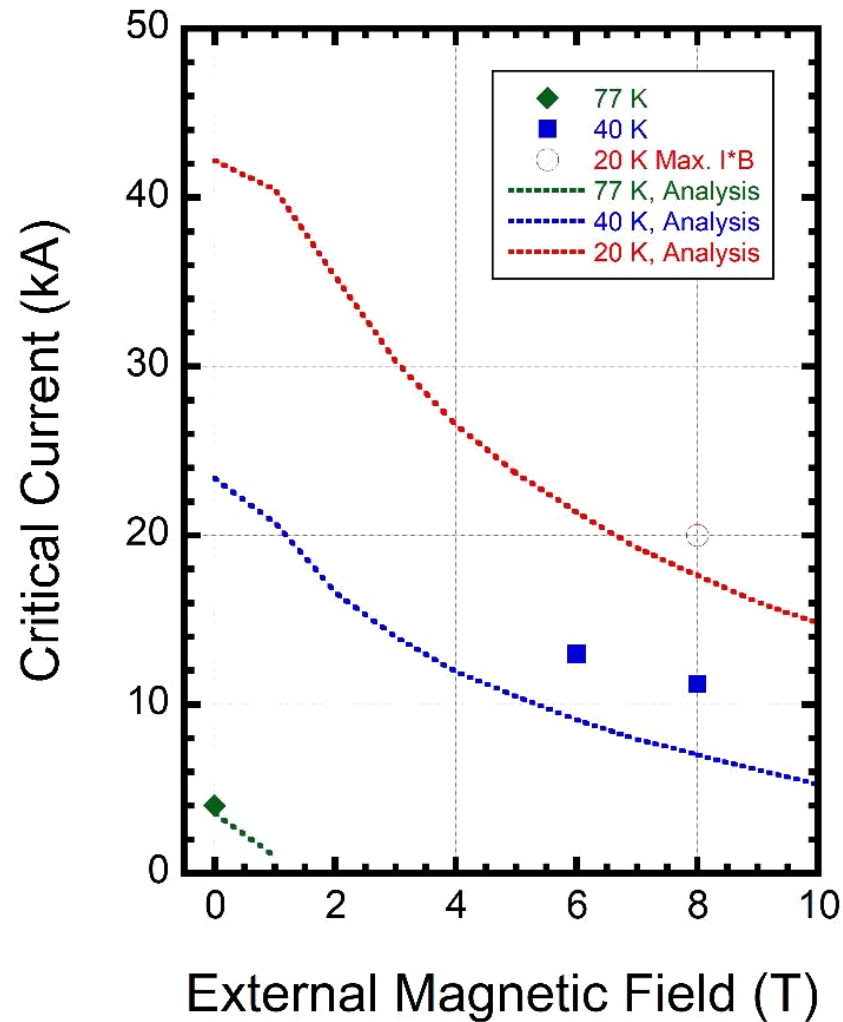
< 9 T, 20-50 K, <20 kA (for the present setup)



★:Temperature sensor



20 kA-class STARS conductor test in 20-40 K, <8 T



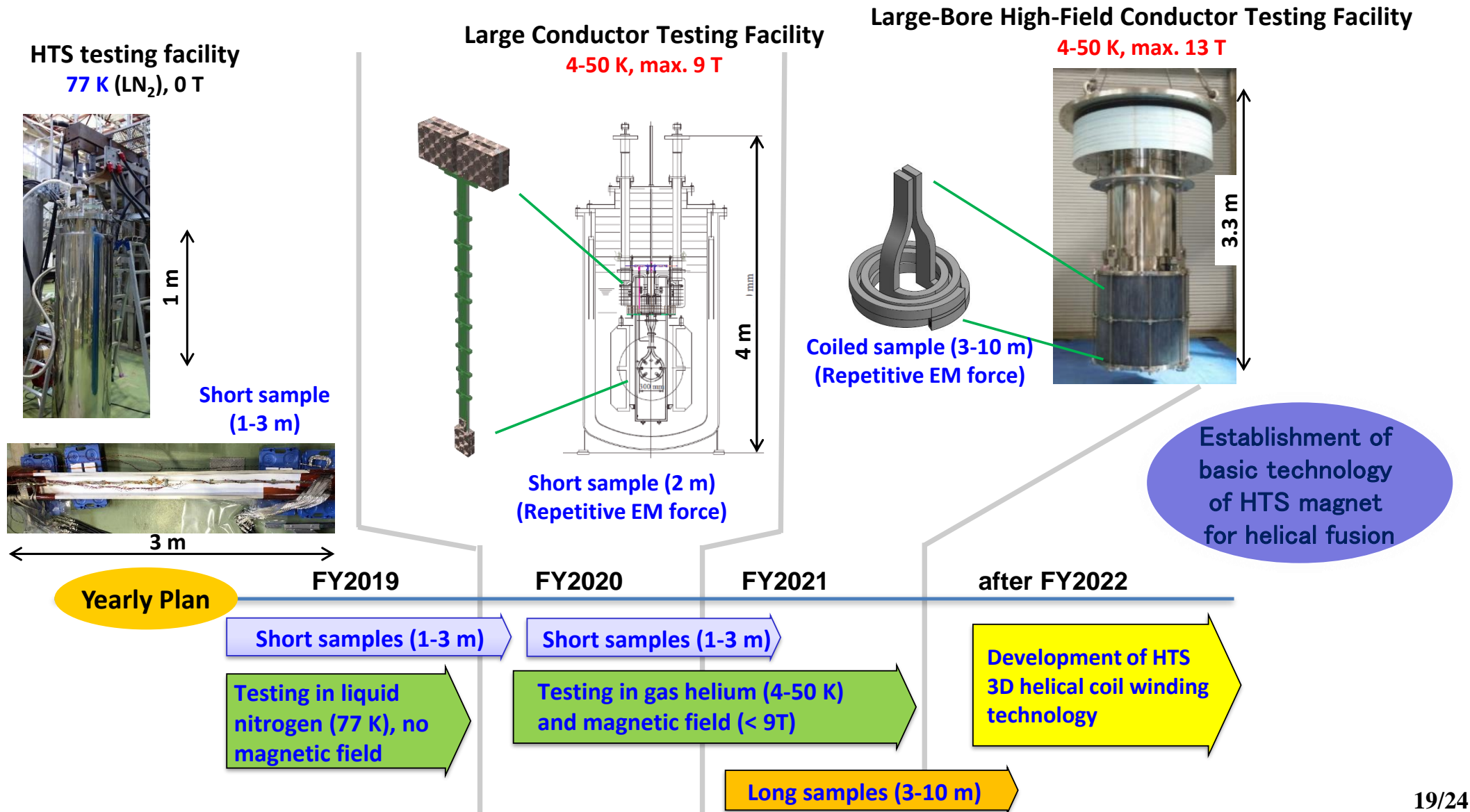
**Mistake in quench detection
→ sample melted locally**



Test in 8 T, 20 K confirms > 20 kA critical current

Critical current was observed at 11.2 kA@40 K, 8 T and 13 kA@40 K, 6 T

HTS conductor development for next generation helical device

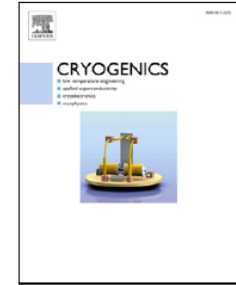




Contents lists available at ScienceDirect

Cryogenics

journal homepage: www.elsevier.com/locate/cryogenics



Research paper

Non-twisted stacks of coated conductors for magnets: Analysis of inductance and AC losses



Davide Uglietti^{a,*}, Rui Kang^{a,b}, Rainer Wesche^a, Francesco Grilli^c

^a *Ecole Polytechnique Fédérale de Lausanne (EPFL), Swiss Plasma Center (SPC), CH-5232 Villigen PSI, Switzerland*

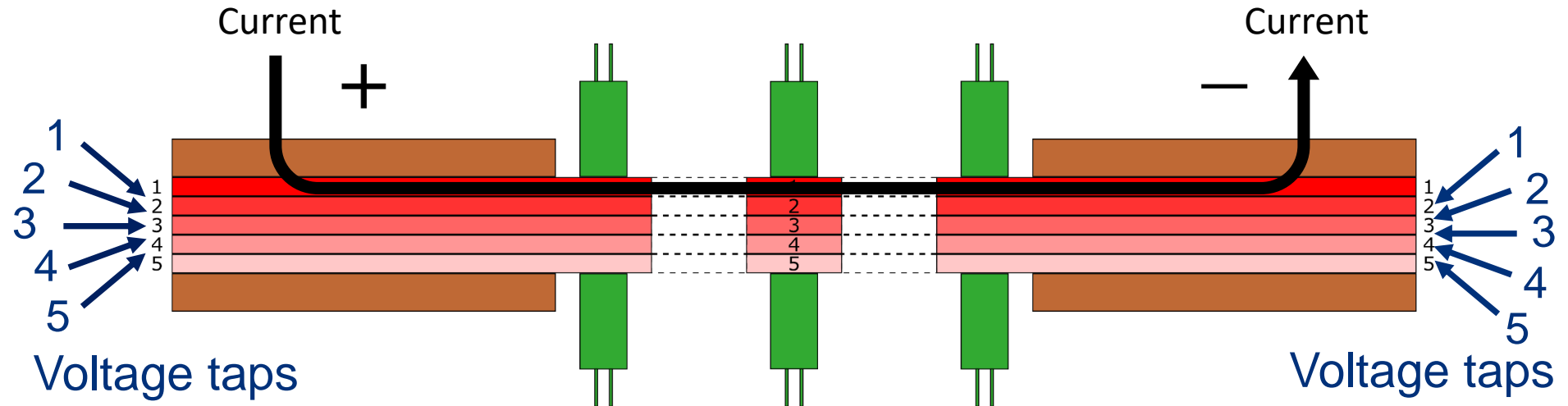
^b *Department of Engineering and Applied Physics, University of Science and Technology of China, Hefei 230026, China*

^c *Karlsruhe Institute of Technology, Karlsruhe, Germany*

A B S T R A C T

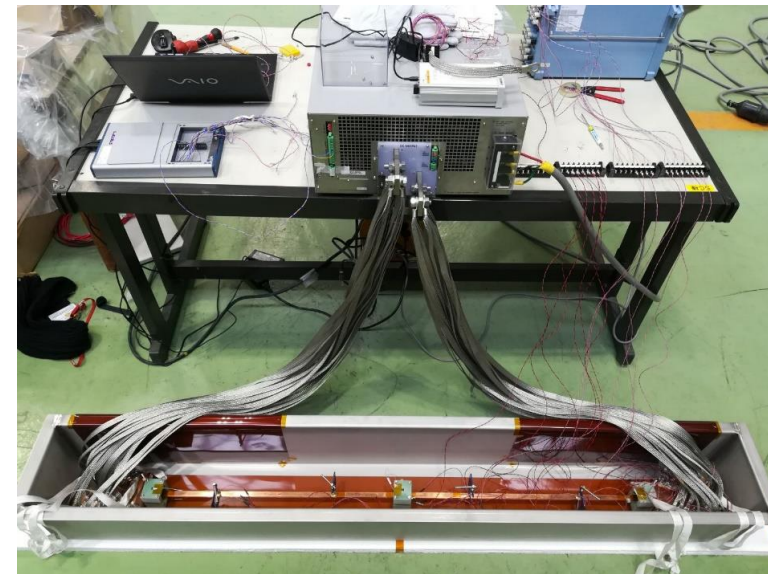
Almost all present High Temperature Superconducting (HTS) cable designs for magnets are based on twisted or transposed concepts that were developed for Low Temperature Superconducting (LTS) cables. However, requirements for LTS materials (like filament twisting) are in general not valid for HTS materials, which are extremely stable; for example, non-twisted multifilamentary Bi-2223 tapes have been successfully used in several magnets. Is twisting necessary for HTS cables? We investigated inductance mismatches and AC losses by numerical and analytical methods in twisted and non-twisted stacks of coated conductors; various experiments reported in the literature support the analysis. Large (hysteretic) losses are common in all magnets built with tapes and are far larger than in magnets built with LTS multifilamentary conductors, because of the aspect ratio and large width of the tape. In small magnets, losses and residual magnetisation could be reduced by replacing a wide tape with a non-twisted stack of narrow tapes. In large cables, we have found that twisting a stack of tapes reduces losses only marginally. Therefore, non-twisted stack cables could be designed to have losses comparable to those of twisted ones. Some examples of non-twisted large cables for fusion applications are discussed: non-twisted stack designs can be simpler, more robust and cost effective than twisted ones, but would require additional R&D.

Does “simple-stacking” really work?

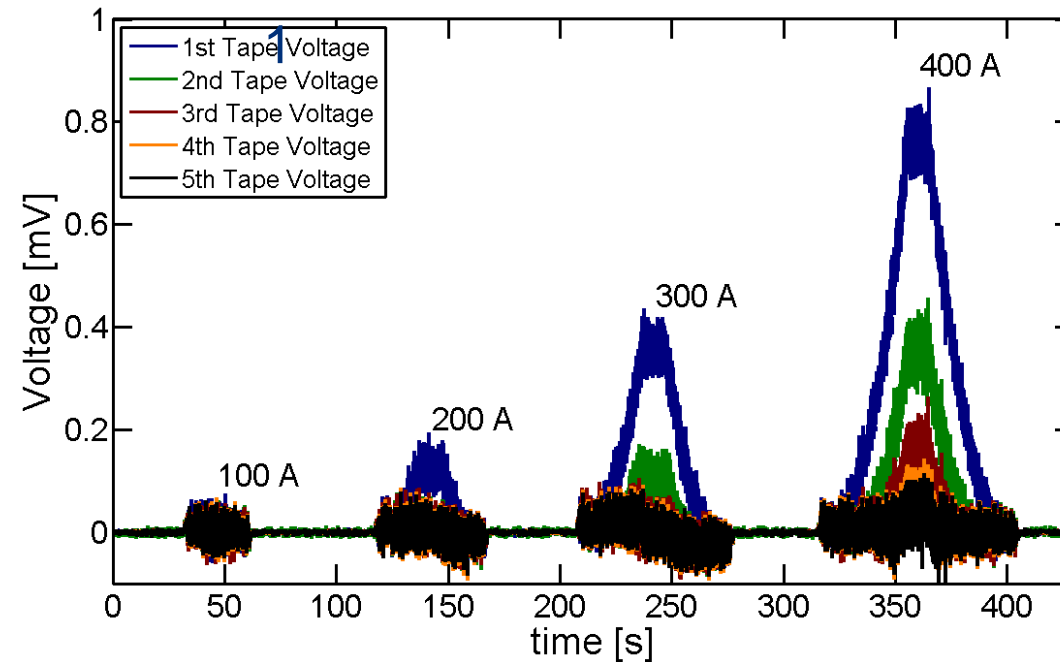
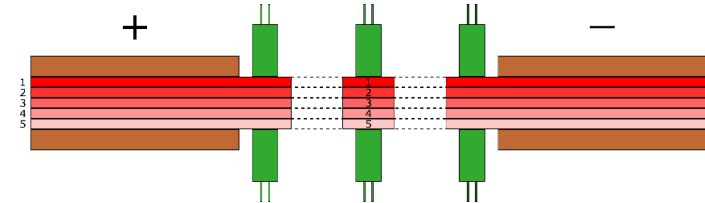
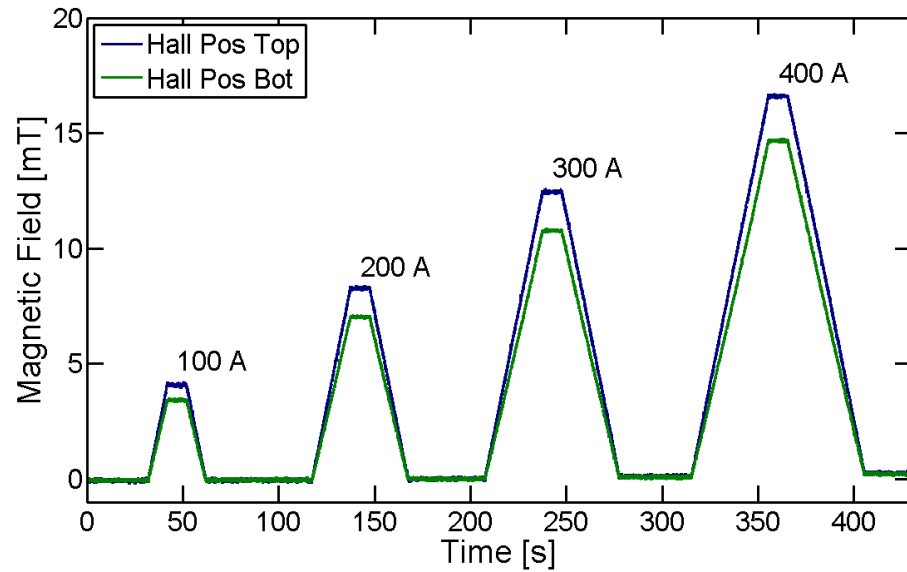


Compulsory formation of non-uniform current distribution in stacked HTS tapes

REBCO tapes: SuperOx ST-4-100 ($I_c \sim 130$ A @77K)

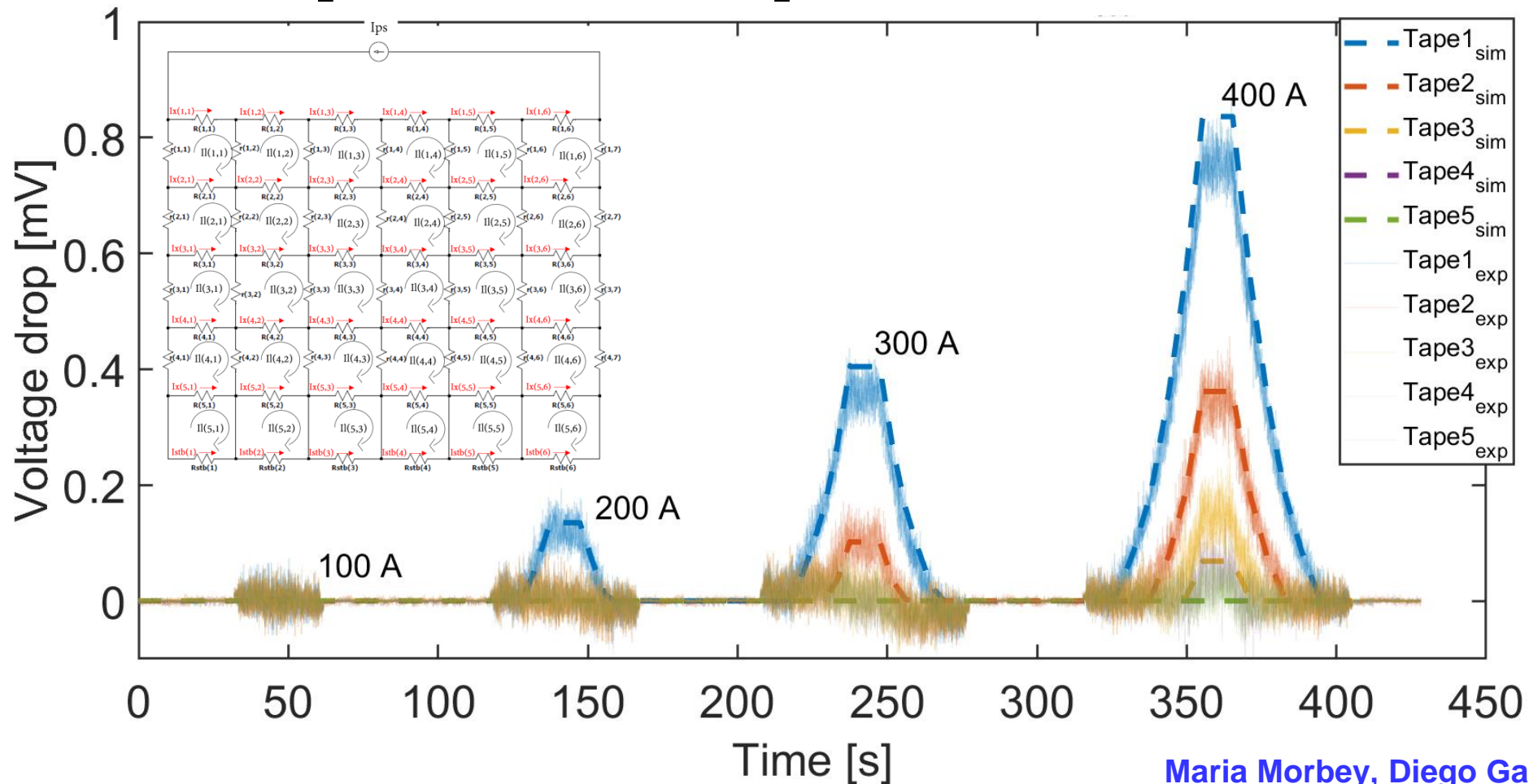


Examination of non-uniform current distribution in STARS configuration



Formation of non-uniform current distribution confirmed by Hall sensors and voltage signals
Nonetheless, stable operation up to critical current of the whole conductor!

Comparison between experiment and simulation



Maria Morbey, Diego Garfias

- Fairly good agreement between experiment and simulation
- Joint resistance may be $\times 100$ higher than the originally estimated value due to low contact pressure
- The numerical simulation will be expanded to long-length coiled structure by including the inductance of tapes, temperature change, magnetic field change

Summary

- The helical fusion reactor **FFHR-b3** is newly proposed as the latest version of the FFHR series, aiming at **100 MW electricity** production with double size the LHD and configuration optimization
- Three types of HTS conductors are being developed for the next-generation helical device (before FFHR-b3) with high current density **80 A/mm²**

STARS conductor

20 kA conductor is developed with simple stacking of REBCO tapes and laser welding of SS jacket
Tests in LN₂ show <1% degradation over ten cooling cycles
Test in 8 T, 20 K confirms > 20 kA critical current
Test in 13 T, 20 K will be carried out in the next step; sample being prepared

FAIR conductor

10 kA conductor is developed with friction stir welding of Al-alloy jacket
Tests in LN₂ show fabrication improvement with twisting of REBCO tapes
Test in 8.5 T, 20-60 K shows lower critical current than expected; further improvement planned

WISE conductor

10 kA conductor is being developed with low-melting temp. metal impregnation
Coiled samples tested in LN₂ show improvement with non-insulation concept
Test in <8.5 T, 20-50 K shows $I_c = 7.9 \text{ kA}@8\text{T} - 11.1 \text{ kA}@5 \text{ T}$ for 40 K

- **Quench protection is a crucial issue for all conductors; effective methods examined**