



# Rotating Machines Using High Temperature Superconductors

## Past, Present and Future

Swarn Kalsi

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# Superconducting Rotating Machines

## OUTLINE

- SC Machine Configurations
- High Speed SC Machines
- Low Speed SC Machines
- Airplane Machines
  - AC Homopolar
  - Wound Rotor
- Outlook

*Conventional motor*



# MOTIVATIONS FOR USING SUPERCONDUCTORS

## Current focus is on two specific applications:

- Highly power dense and efficient motors and generators for aircraft applications
- Offshore large wind turbine generators requiring high torque density and efficiency, and low cost
- Compared to Conventional Machines, Superconducting machines can;
  - Increase machine efficiency beyond 99% (reducing losses by as much as 50%)
  - Reduce size and mass by a factor of 3 or more
- Provide improved reliability with long lasting windings - nearly zero degradation of coil insulation at cryogenic temperatures

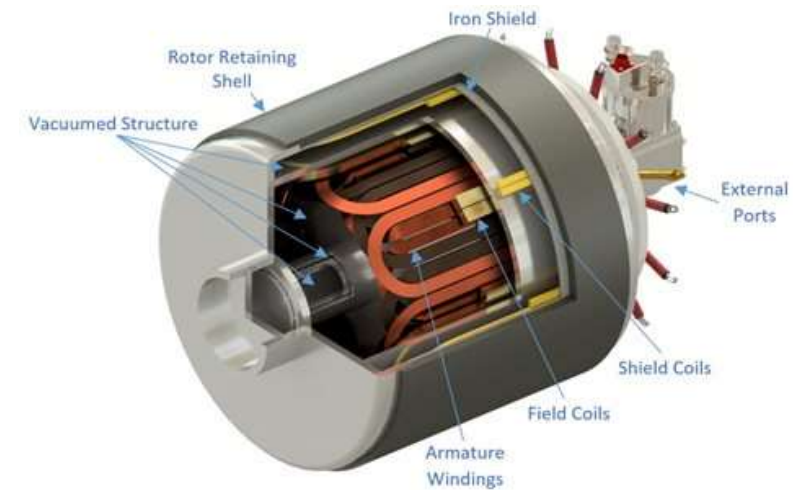
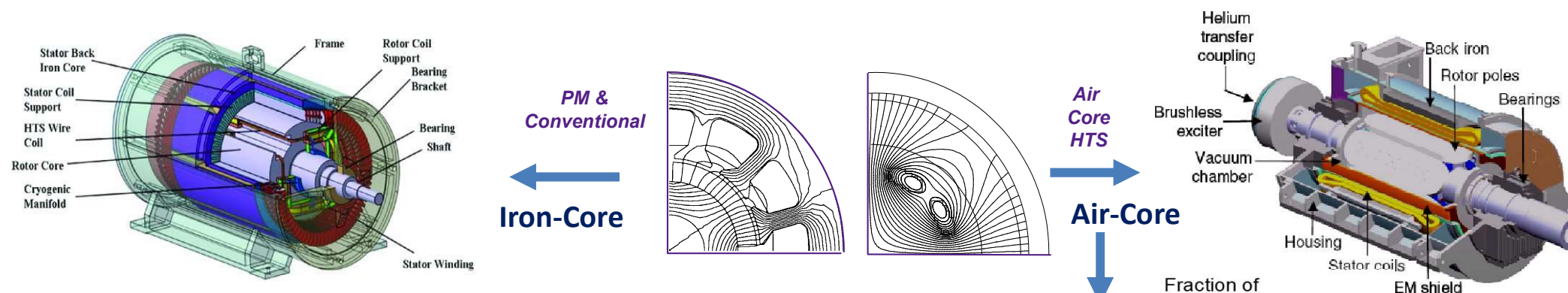


Photo: Fraunhofer Institute for Wind Energy Systems

**Docking Maneuver:** Workers prepare to link the 3.6-megawatt Ecoswing superconducting generator [blue] to a machine that simulates the torque and other aspects of a wind turbine [gray].

# SUPERCONDUCTING MACHINE CONFIGURATIONS



- Harmonics generated inside an air-core HTS synchronous machine are extremely small
- Lower harmonic content eases machine component design and simplifies external control systems

Harmonic Order	Fraction of Fundamental	Harmonic Order	Radial	Tangential
1	1	1	1	1
3	0	3	-0.057	0.116
5	$5.977 \cdot 10^{-4}$	5	$3.869 \cdot 10^{-4}$	$7.097 \cdot 10^{-3}$
7	$7.394 \cdot 10^{-6}$	7	$4.567 \cdot 10^{-5}$	$-1.153 \cdot 10^{-3}$
9	0	9	$-7.546 \cdot 10^{-5}$	$-4.378 \cdot 10^{-4}$
11	$6.074 \cdot 10^{-8}$	11	$4.55 \cdot 10^{-6}$	$-4.586 \cdot 10^{-5}$
13	$1.542 \cdot 10^{-10}$	13	$-8.935 \cdot 10^{-7}$	$1.027 \cdot 10^{-5}$
15	0	15	$5.559 \cdot 10^{-7}$	$4.827 \cdot 10^{-6}$
17	$1.032 \cdot 10^{-11}$	17	$-1.149 \cdot 10^{-8}$	$5.882 \cdot 10^{-7}$
19	$-3.381 \cdot 10^{-14}$	19	$-2.729 \cdot 10^{-9}$	$-1.475 \cdot 10^{-7}$

Harmonics generated by field winding in stator

Harmonics generated by stator AC winding on the rotor surface

*In iron core machines, flux jumps between teeth cause magnetostrictions, mechanical vibrations and noise*

### Examples of High-Speed Machines Built and Tested

- 1000 hp, 1800 rpm synchronous motor by Rockwell/AMSC (2000)
- 5000 hp, 1800 rpm synchronous motor by AMSC (2001)
- 8 MVAR, 1800 rpm synchronous condenser by AMSC (2004)
- 4 MW, 3600 RPM generator by Siemens (2007)
- 3.6 MW, 1800 RPM motor by TECO-Westinghouse (2015)



# HIGH SPEED MACHINES EMPLOYING HTS ONLY

# 1000 HP, 1800 RPM SYNCHRONOUS MOTOR (2000)

- First motor jointly built by AMSC and Baldor/Rockwell Automation
- 1000 HP, 1800-RPM, 4-pole
- Field Winding - BSCCO-2223 conductor @25 K
- Armature Winding – Diamond type copper coils
- HTS rotor coils cooled with liquid neon
- Tested in the Summer 2000
- Met performance expectations



Field Winding on the Rotor



AC Winding on the Stator

*Encouraging progress on this motor motivated AMSC to built 5000 HP motor*

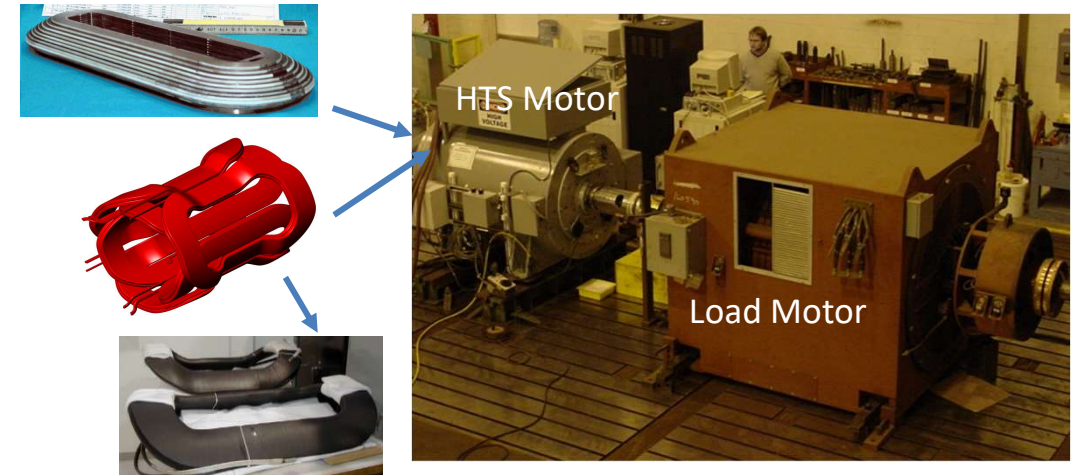
# AMSC 5000 HP CONSTRUCTION AND TESTING (2001)

## GOALS:

- 5000 HP, 1800-RPM, 60 Hz motor
- Line voltage 6.6 kV
- Air-Core machine – No iron in stator or rotor coils
- Field Winding – stacked BSCCO-2223 pancake coils
- Closed-loop cooling system used G-M cryocooler
- Armature Winding – Single layer copper coils
- Copper coils cooled with fresh water
- Frame dimensions:  
 1.1 m dia x 1.6 m long
- Weight – 6.8 ton
- Efficiency – 97.7%
- Copper coils cooled with fresh water

## TEST RESULTS:

- Factory load testing completed per IEEE 115
- Achieved motor efficiency: 97.7%
- 1/3 reduction in volume compared to the industry standard
- 40% reduction in losses compared to the industry standard



<u>Parameter</u>	<u>Design</u>	<u>Measured</u>
Line Voltage, kV	6.6	6.6
Phase Current, A	329	330
Rating, hp	5000	5000
Xd, pu	0.32	0.30
Xd', pu	0.28	0.23
Xd'', pu	0.16	0.17
Back EMF, pu	1.043	1.035

*World's most powerful HTS industrial motor to date*

# SIEMENS 4 MVA, 3600 RPM GENERATOR (2007)

## DESIGN PARAMETERS FOR THE 4 MVA SIEMENS MACHINE

Nominal power	4 MVA
Rated speed	3600 rpm
Rated voltage	3~60 Hz AC 6.6kV
Rated current	350 A
Nominal torque	10.6 k Nm
Degree of protection	Int. Protection Code 44
Bearings	Sleeve bearings
Rules	Germanischer Lloyd
Total dimensions of the machine (including cryocooler) LxWxH	3.7m x 2.5m x 1.8m
Shaft height	500mm
Foot print LxW	1.9m x 1.2m
Total weight	6.9 t

## ELECTRICAL PARAMETERS OF THE 4 MVA HTS MACHINE

Synchronous reactance $x_d$ , unsaturated	0.51 p.u.
Synchronous reactance $x_d$ , saturated	0.33 p.u.
Transient reactance $x_d'$	0.28 p.u.
Subtransient reactance $x_d''$	0.15 p.u.
Rotor inductance	28 H
Transient time constant $T_d'$	700 s
Subtransient time constant $T_d''$	0.01s

Data	
Output:	4 MVA
Voltage:	6,6 kV
Speed:	3600 rpm
Frame size:	500 mm
Efficiency:	98,7 %
HTS wire:	6 km



Hybrid machine – HTS rotor and Conventional Stator

Ref: W. Nick, M. Frank, G. Klaus, J. Frauenhofer, and H. Neumuller, "Operational Experience with the World's First 3600 RPM, 4 MVA Generator at Siemens", IEEE TAS, Vol. 17, No. 2, June 2007

*Generator was successfully tested*



# TECO-WESTINGHOUSE 3.6 MW 1800 RPM MOTOR (2015)

- REBCO field coil around salient rotor poles
- Conventional stator with iron teeth
- Table below compares volume, power density and efficiency with a conventional induction motor operating on the ship with those of the PM and HTS 2G motors
- HTS REBCO motor had higher efficiency and power density than both induction and PM motors

Type of Motor	Power Density (x 100 kN/m <sup>2</sup> )	Volume (m <sup>3</sup> )	Efficiency (%)
Induction	0.26	0.8	96.37
Permanent	0.42	0.56	97.62
HTS 2G Field Winding	0.53	0.41	98.72

*HTS motor offers little benefit over PM motor in iron-core machines*



Figure 7. 3.6 MW 1800 RPM ship propulsion motor. © 2015 IEEE. Reprinted, with permission, from [22].

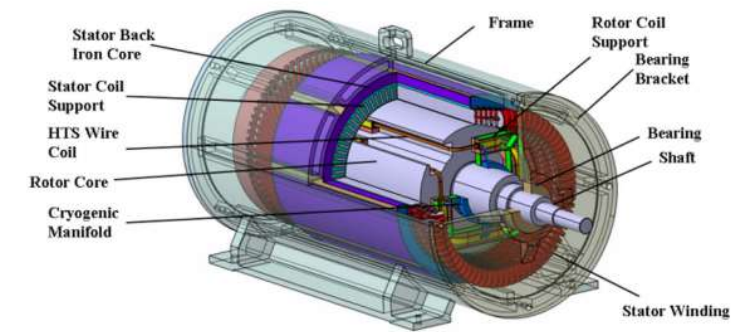


Figure 8. A conceptual design of HTS propulsion motor. © 2015 IEEE. Reprinted, with permission, from [22].

Ref: Supercond. Sci. Technol. 30 (2017) 123002

# *SuperVAR<sup>®</sup>* *Dynamic Synchronous Condenser*

**AMSC – 8 MVar  
Condenser** →



Hoeganaes, Tennessee

## **HIGH SPEED SC MACHINES**

# SUPERVAR<sup>®</sup> PROTOTYPE PROJECT DESCRIPTION (2004)

Similar to a conventional synchronous machine but with better performance

- Fast reacting transient dynamic voltage support and stability (leading and lagging VARS) at a multiple of the machine rating
- Reduced operating costs over conventional condensers - Low losses even at partial load
- Generates very low levels of harmonics - requiring no filters
- Operates at line voltage on the low side of transmission to distribution transformer
  - Stator provides distribution level voltages
  - No additional transformer needed in most applications



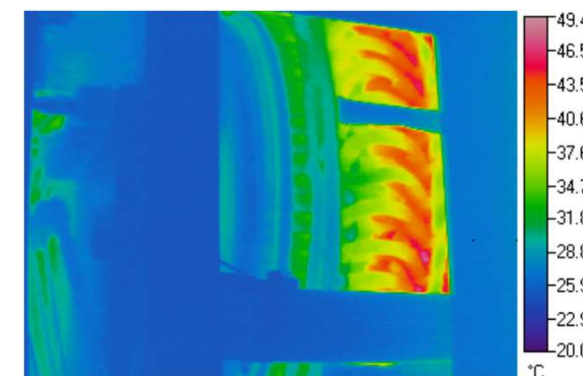
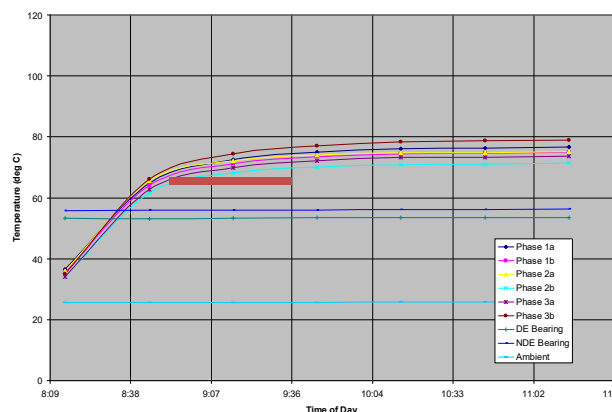
Rating	8 MVAR
Voltage	13.8 kV line to line
Ambient Temp	-30° to +40°C
Losses	1.5% rating at 8MVA
	Including 30kW 480V auxiliary power

*SUPERVAR has significant benefits over conventional machines*

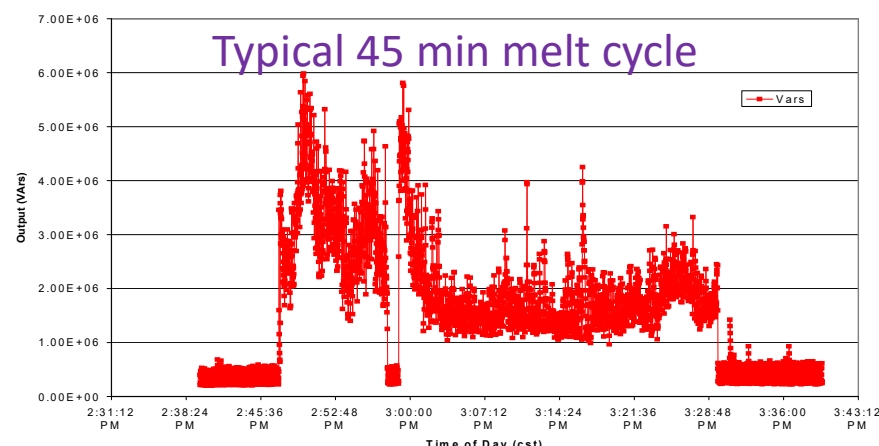
Ref: S. S. Kalsi, et al "Discussion of Test Results of a Superconductor Synchronous Condenser on a Utility Grid", IEEE TAS, Vol., 17, No. 2, June 2007

# REAL LIFE OPERATION ON TVA GRID (2004)

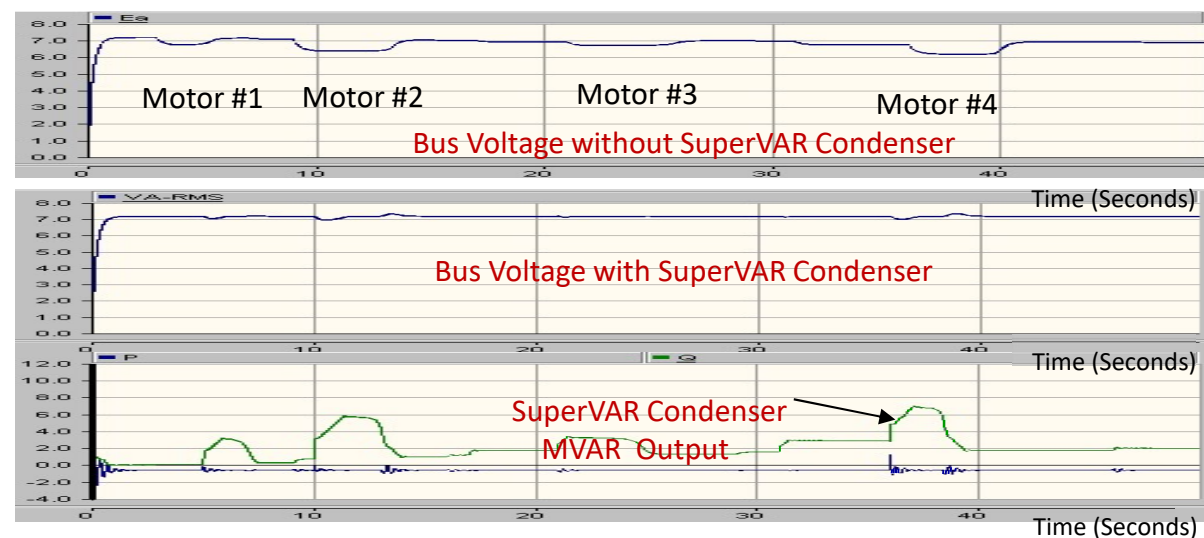
- Installed on TVA grid in Gallatin, TN on 10 October 2004
- Operated for 1 yr flawlessly
- $\pm 8$  MVAR capability verified
- Machine reacted quasi-instantaneously to transients due to arc furnace operations



- Designed temperature rise  $\leq 120^\circ\text{C}$  at  $40^\circ\text{C}$  ambient temperature
- Stator end turn temperature monitored using infrared camera

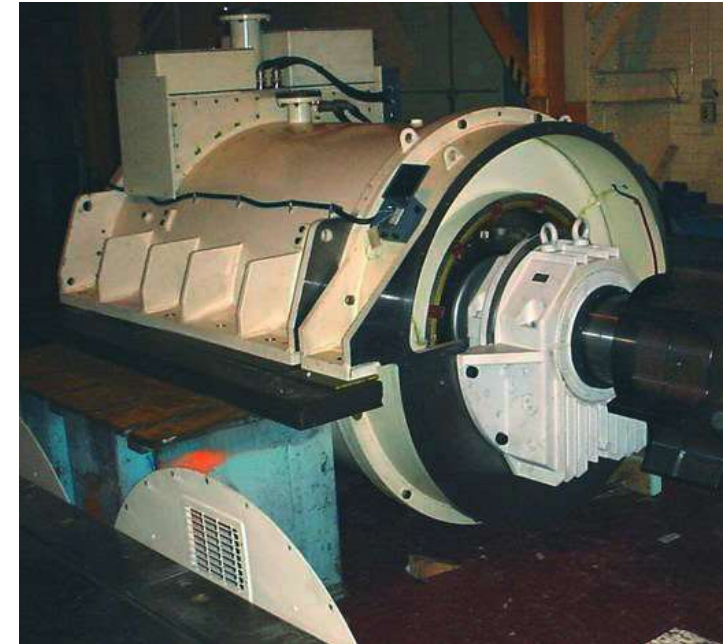


*Demonstrates that an HTS machine can handle substantial stator fed harmonics*

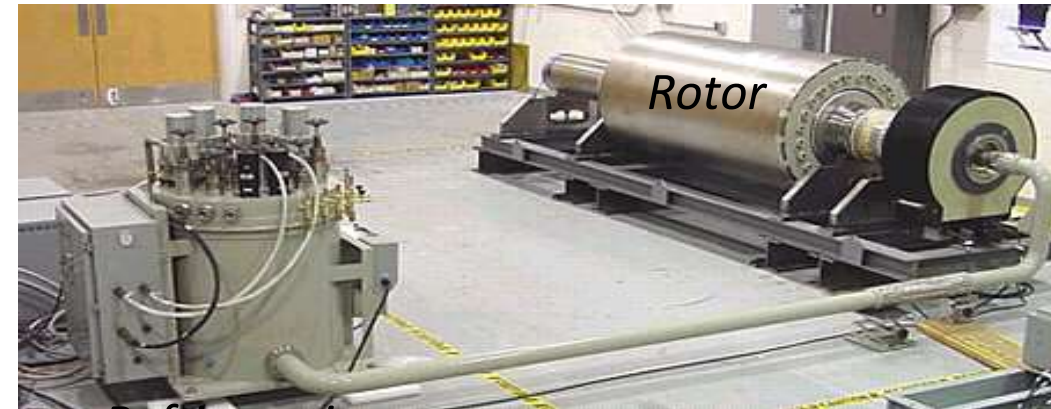
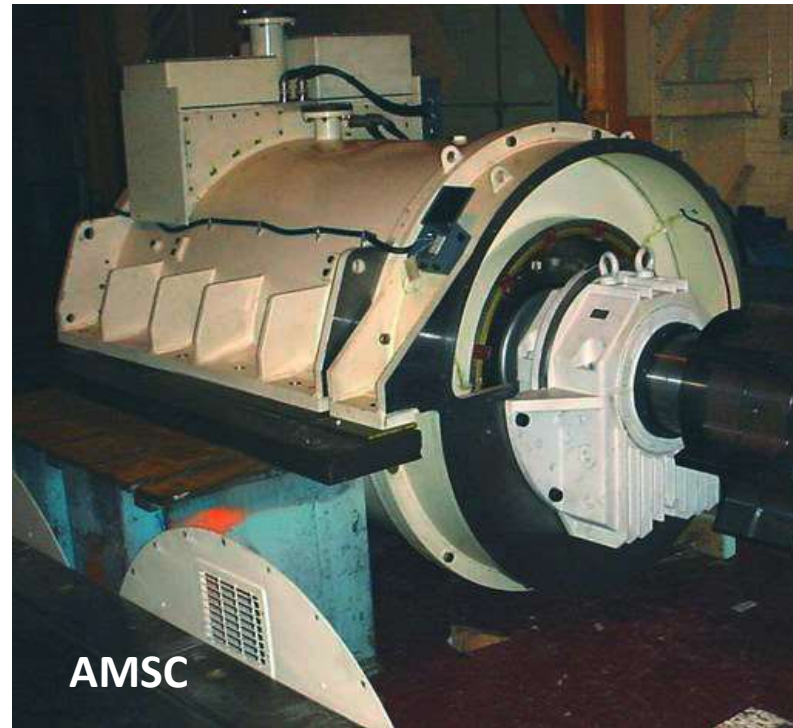


- 5 MW, 230 RPM Ship Propulsion motor (2003)
- 36.5 MW, 120 RPM Ship Propulsion motor (2008)

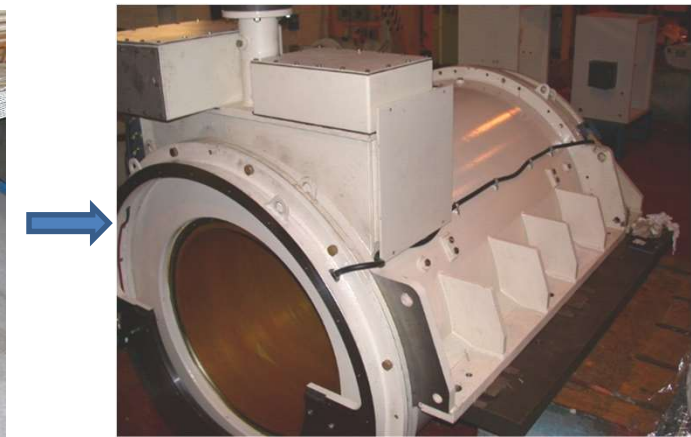
## LOW SPEED MACHINES



# AMSC 5 MW SHIP PROPULSION MOTOR (2002)



Refrigeration

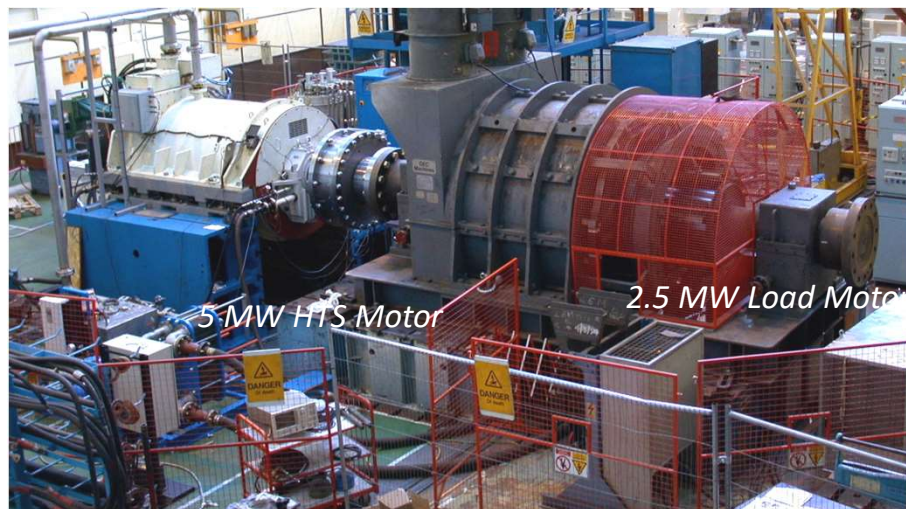


All subsystems were tested prior to assembling in the motor

# TESTING OF THE 5 MW SHIP PROPULSION MOTOR (2003)

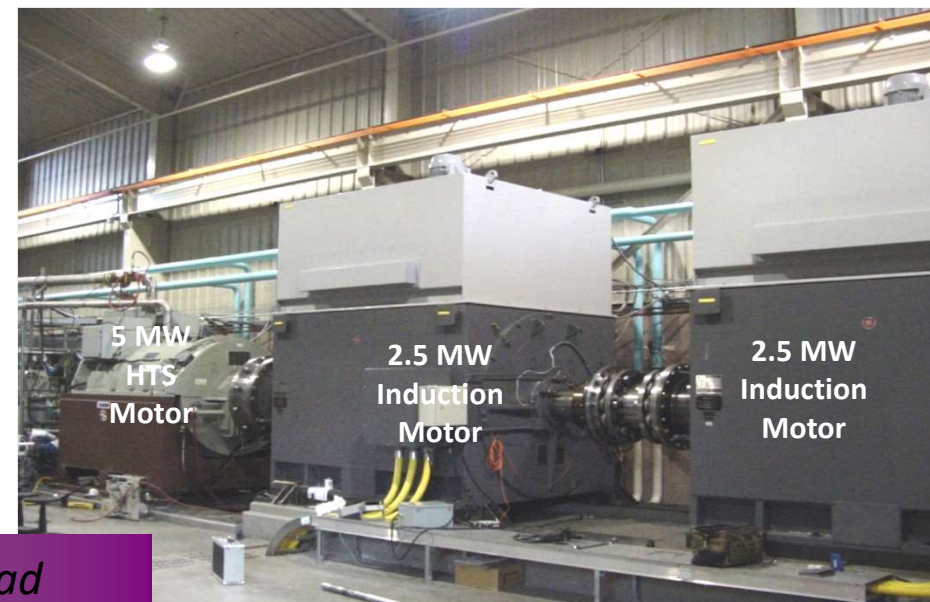
## Part-Load Testing in Factory

- No-Load IEEE 115 Std.
  - Motor Parameters
  - Efficiency
- Full torque at  $\frac{1}{2}$  speed
- Limited Structure borne Noise Data
- Operation on a Drive



## Full-load Testing at CAPS

- Motor was delivered to CAPS in July 2003.
- Motor was coupled to a pair of 2.5 MW squirrel cage induction motor dynamometers
- Motor load test results were reported at the ASC-2004 conference in September 2004

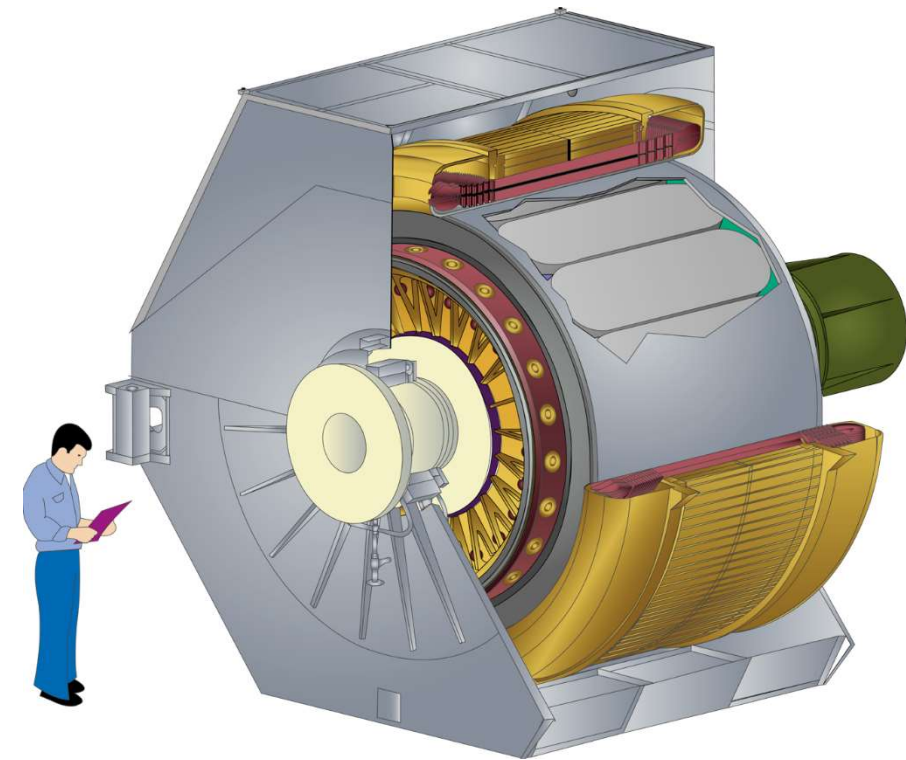


*Full-load testing was conducted by simulating ship propulsion load*

# Ship Propulsion – AMSC (2008)

## 36.5 MW, 120 RPM Motor

### LOW SPEED SC MACHINES





# BUILT 36.5 MW BASED ON 5 MW EXPERIENCE (2007)

- Designed and built the motor to power the next generation of Navy ships
- ONR contracted AMSC to deliver the 36.5 MW, 120 RPM motor, integrated with a commercial Variable Frequency Drive
- Attractive Feature: For the same torque, the motors are compared on basis of weights;
  - 75 tonnes HTS motor,
  - 280 tonnes<sup>1</sup> for an advanced induction motors
  - 400 tonnes<sup>2</sup> for a QE2 synchronous motor
- 36.5 MW motor design was based on the 5 MW motor technology.

1 Scaled from ALSTOM IPS Induction Motor

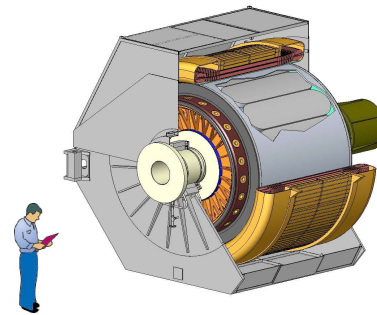
2 <http://www.qe2.org.uk/engine.html>

Parameter	Value
Rating	36.5 MW
Line Voltage	5.8 kV
Speed	120 RPM
Synchronous reactance, $X_d$	0.37 pu
Transient reactance, $X_d'$	0.32 pu
Sub-transient reactance, $X_d''$	0.24 pu
Efficiency	97.1%

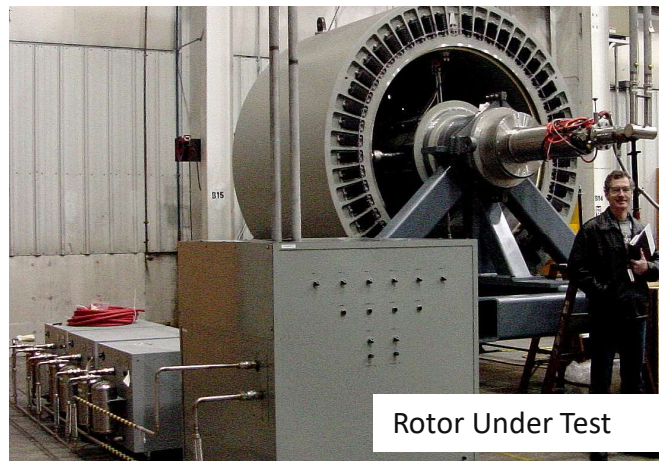
*This 36.5 MW motor still holds world record for being the largest capacity motor ever built in a single frame*

# 36.5 MW SHIP PROPULSION MOTOR COMPONENTS (2007)

- AMSC built a 36.5 MW, 120-RPM HTS ship propulsion motor for ONR
- Motor weighs 75-tonnes, including stator and rotor cooling systems
- Delivered to ONR in 2008



Refrigerator



Rotor Under Test



HTS Field Coil



Shaft



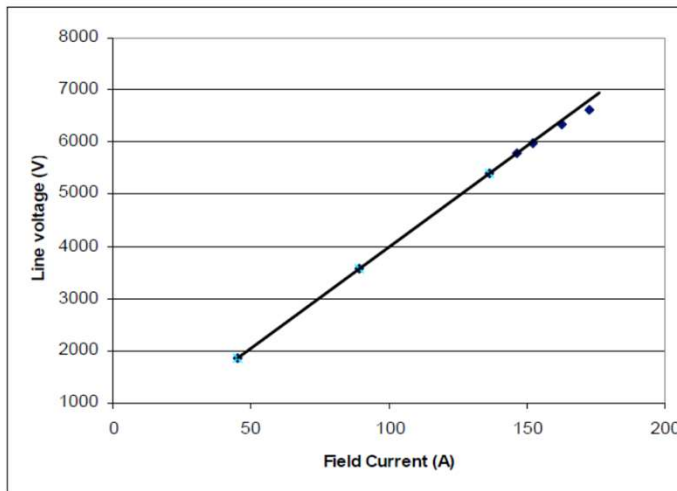
Rotor End Ring



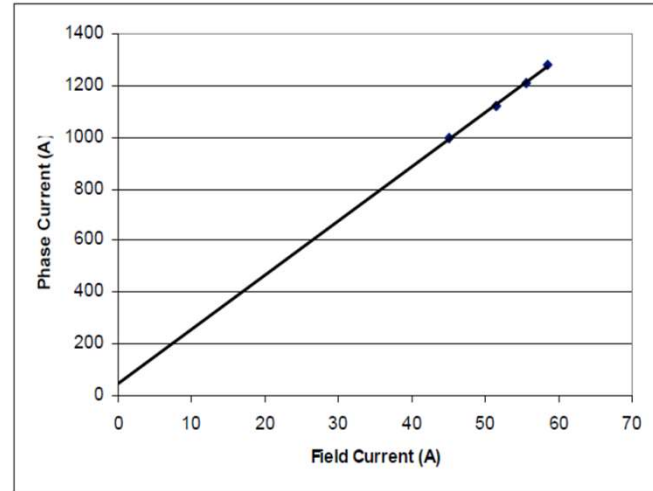
Stator

*All components were tested/inspected before releasing them for final assembly*

# 36.5 MW Motor –Test Results (2008)



**OPEN-CIRCUIT TESTING**



**SHORT-CIRCUIT TESTING**

Parameter	Design	Measured
Design Power	37.2 MW	---N. A.---
Voltage	5.8 kV	6.6 kV
Current	1.275 kA	1.28 kA
Stator Winding Temperature	Class F to meet Class B	80.5 C (based on resistance and scaled to 40C inlet)
Efficiency	97%	97%

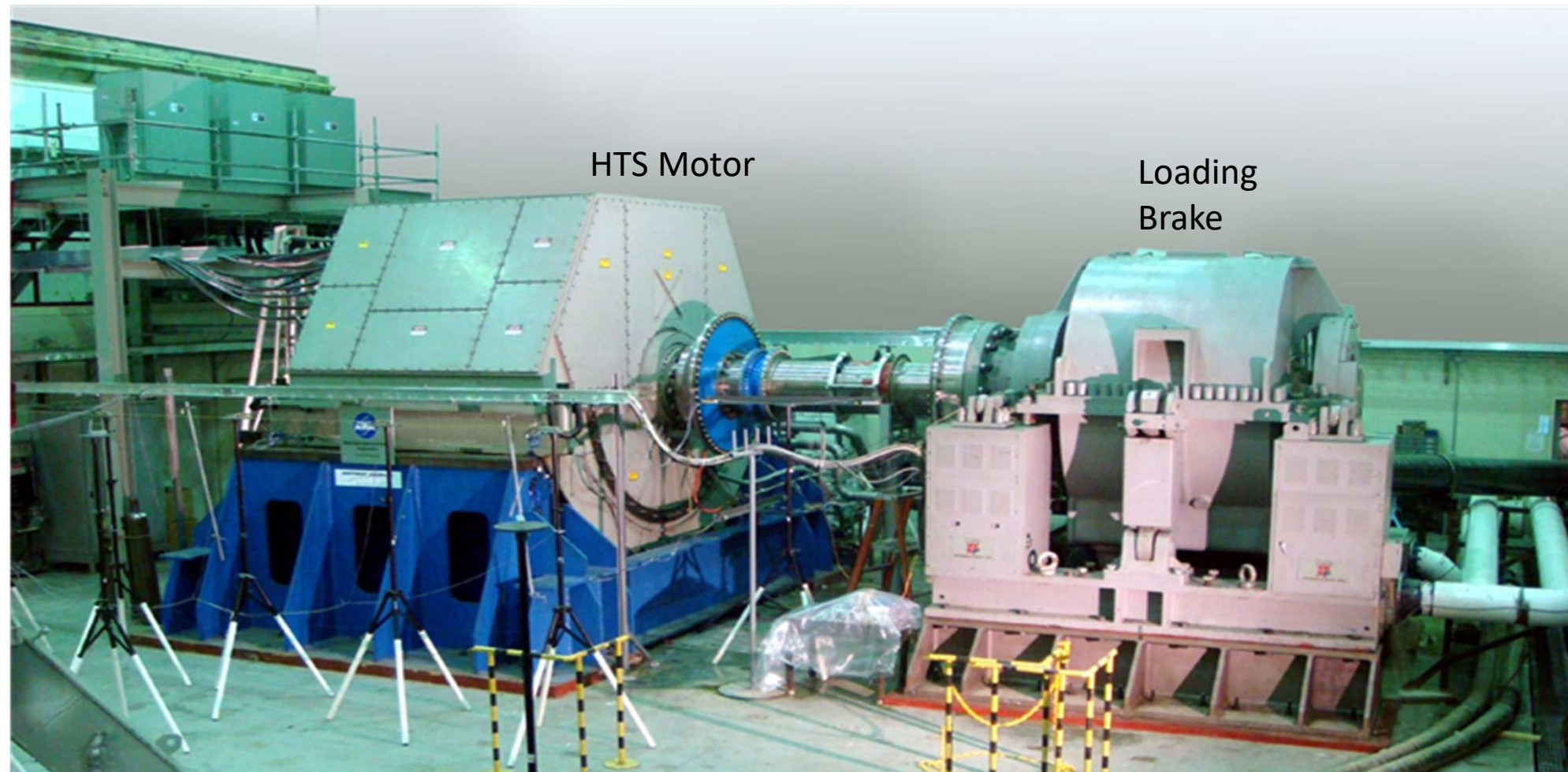
**DESIGN VS. MEASUREMENTS**

- Design, development and manufacture of the direct-drive ship propulsion motor was validated by the successful factory testing.
- The full power testing of the 36.5 MW HTS motor system was conducted by the Navy operated land-based test site in Philadelphia

*Ref: Bruce Gamble, Greg Snitchler and Tim MacDonald, "Full Power Test of a 36.5 MW HTS Propulsion Motor", IEEE Transactions on Applied Superconductivity ( Volume: 21, Issue: 3, June 2011 ), pages:1083-1088*

*The most powerful motor ever was successfully load tested by the Navy satisfying all design requirements*

## 36.5 MW MOTOR UNDER LOAD TESTING AT NAVY TEST FACILITY (2008)



*The motor was successfully tested to full-load by US Navy - meeting all design objectives*



# WIND TURBINE GENERATORS

# HTS POLE FOR A WIND TURBINE GENERATOR (2011)

- A pole made for a 10 MW class wind turbine generator by AMSC
- Employed 2G REBCO wire
- The pole was built and tested in 2011
- Demonstrated feasibility of building large magnets with REBCO coated conductors

*Ref: G. Snitchler et al., "10 MW class superconductor wind turbine generators," IEEE Trans Applied Superconductivity, vol. 21, no. 3, p. 1089, June 2011*

*Coil manufacturing technology demonstrator for building large HTS pole with REBCO wire*



# ECO 5 3.6 MW WIND TURBINE GENERATOR (2018)



**3.6 MW, 12 RPM  
Generator  
by ECO 5**

Source:  
IEEE Spectrum,  
Aug. 2018

The Only tested superconducting  
wind power generator

Photo: Fraunhofer Institute for Wind Energy Systems

**Docking Maneuver:** Workers prepare to link the 3.6-megawatt Ecoswing superconducting generator [blue] to a machine that simulates the torque and other aspects of a wind turbine [gray].



Two kind of machines under consideration

- AC Homopolar
- Wound Rotor

## **AIRPLANE APPLICATIONS**



# NASA DEFINED REQUIREMENTS

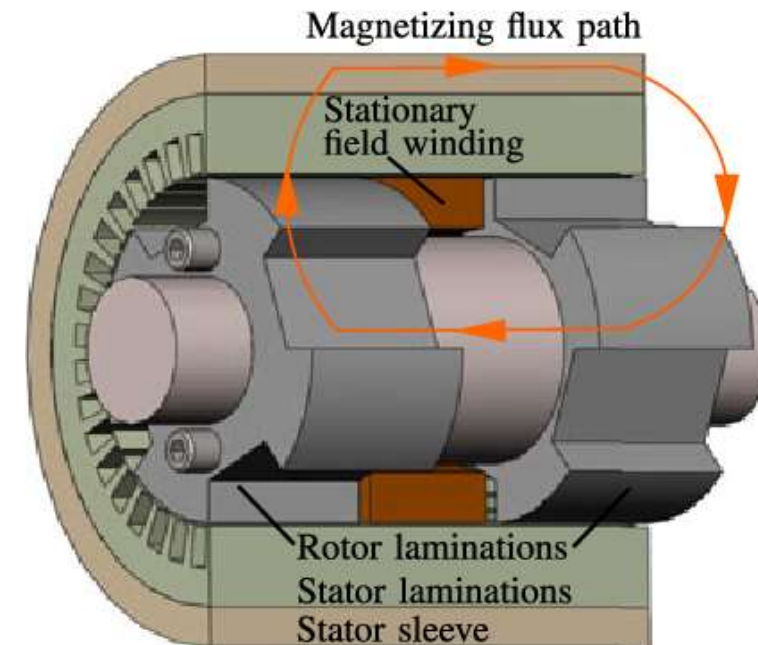
NASA's Fixed Wing Project (currently the Advanced Air-Transport Technology Project) has defined goals for the next three generations of aircraft for commercial aviation. Below are electrical machine requirements for an example turboelectric-aircraft concept.

	Generators	Motors
Number of units	2	15
Power rating	30,000 hp (22.4 MW)	4,000 hp (3 MW)
Assumed weight	2,200 lb (1,000 kg)	520 lb (236 kg)
Assumed efficiency	99.3%	99%
Rotational speed	6,500 rpm	4,500 rpm

Ref: Felder J L, Brown G V, Kim H D and Chu J 2011 Turboelectric distributed propulsion in a hybrid wing body aircraft Proc. 20th Int. Society for Airbreathing Engines (Gothenburg, Sweden, 12–16 Sept. 2011)

*These guidelines are being used for developing HTS motors and generators for airplanes*

- 5/1 MW, 35000 RPM generator by GE (2009)
- 10 kW, 24000 RPM motor by VUW (2022)



## AC HOMOPOLAR MACHINES – ULTRA HIGH SPEED

**NO WINDINGS ON THE ROTOR**

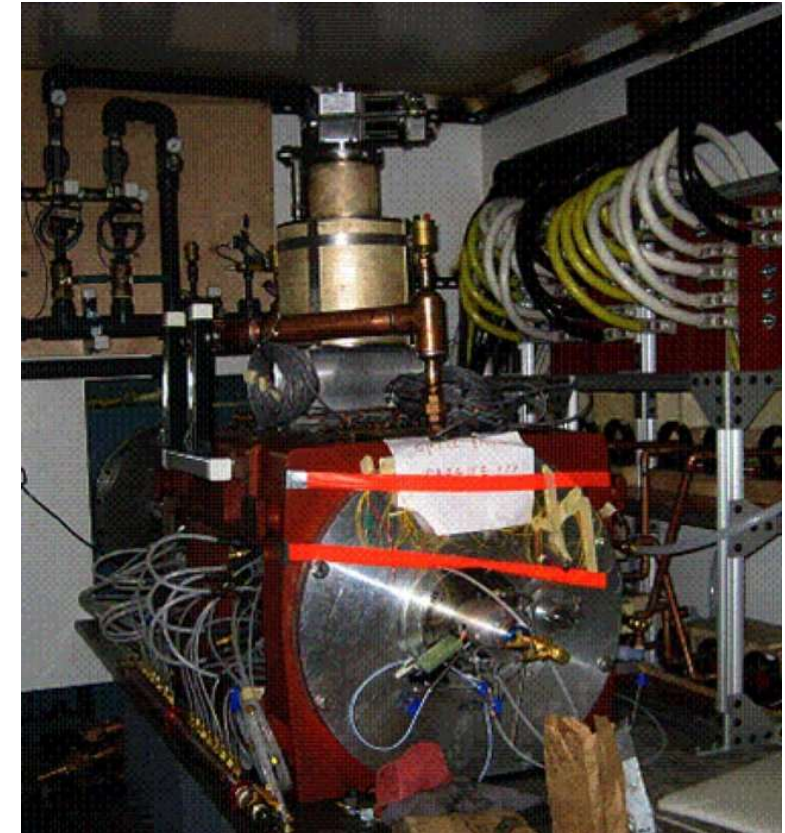
# GE 5 MW HOMOPOLAR GENERATOR (2009)

- 5 MW Homopolar Synchronous Generator for Air Force Research Lab
- Factory tested to 1 MW
  - Test speed 10,500 rpm
  - Resistive load
  - Efficiency at 1 MW = 97%
- Satisfied Airforce contract requirements

TABLE I  
DESIGN PARAMETERS OF AN AFRL HIGH-SPEED HTS HIA

Parameter	Value
Power, MW	5
Rated speed, rpm	35000
Voltage, V	670
Poles	6
Frequency, Hz	1750
Efficiency at FL, %	98
Synch reactance, p.u.	0.7
Gap flux density, T	1.8
Field Ampere-Turns	45,000
Diameter, cm	50
Length, cm	50
Active Length, cm	21.6
Machine weight, kg	500
Cryogenic weight, kg	45.5
Total Machine weight, kg	545

**Power Density = 9 kW/kg**



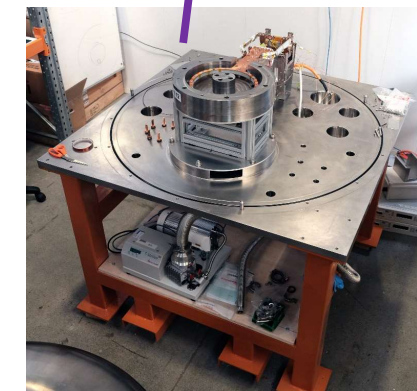
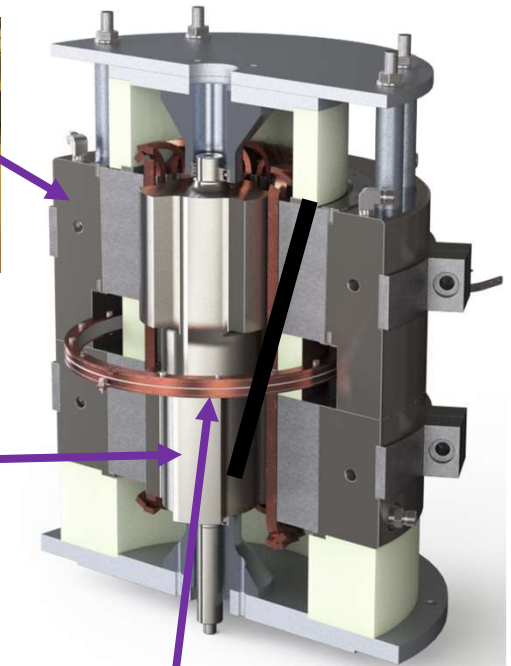
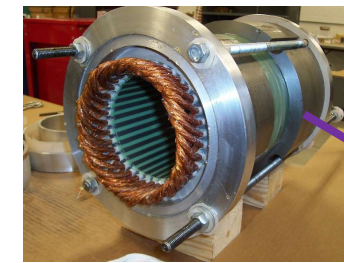
**Generator on test stand**

Ref: K. Sivasubramaniam, et al, 'Development of a High Speed HTS Generator for Airborne Applications', IEEE Trans. on Applied Superconductivity, Vol. 19, No.3, June 2009, p. 1656

# VUW-RRI 10 kW HOMOPOLAR MOTOR (2022)

- 10 kW, 25000 RPM homopolar synchronous motor is under construction
- All components have been built and bench tested
- Final assembly is progressing
- No-load testing for motor characterization will begin in January 2023
- Load testing will be conducted at an outside facility

Parameter	Value
Motor rating, kVA	15
Rated line voltage, V	264
Rated current, A	33
Number of poles	6
Rated speed, RPM	25,000
Rated frequency, Hz	1,250
Rated field current, A	370
Efficiency at rated load, %	85
Overall axial length, mm	394
Overall diameter, mm	410
Mass of machines, kg	334



Motor is being assembled for testing beginning Jan. 2023

Ref: K. A. Hamilton, S. S. Kalsi, J. G. Storey, D. A. Carnegie, and R. A. Badcock, "Design and Build of a High-Speed AC Homopolar Superconducting Motor", ISS-2022, AP3-1

Airplane motors and generators (compact lightweight efficient)

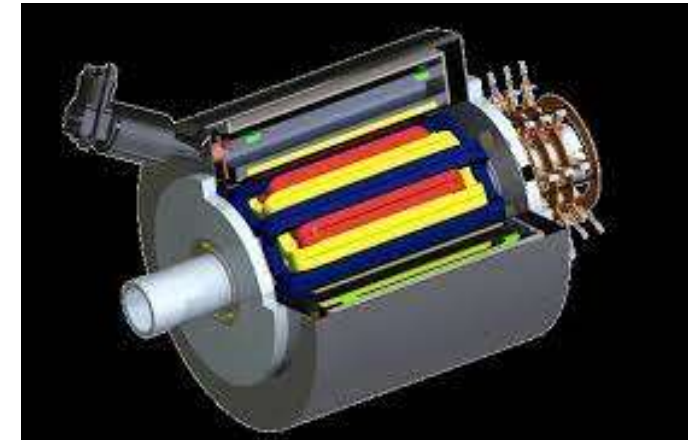
NASA 1.4 MW motor

VUW 3 MW, 4500 RPM motor

SOARING 2.5 MW, 5000 RPM motor

CHEETA 5 MW, 4500 RPM motor – INSIDE OUT CONFIGURATION

SAFRAN HTS Bulk Motor

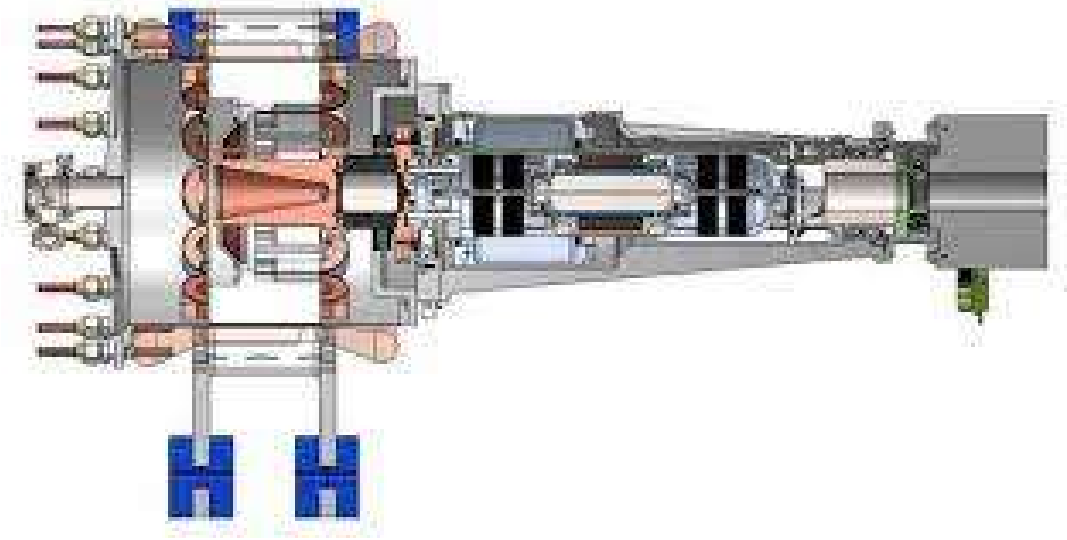


## WOUND ROTOR AIRPLANE MOTORS

**CURRENTLY UNDER DEVELOPMENT**

# NASA HIGH-EFFICIENCY MEGAWATT MOTOR (HEMM)

- NASA is constructing a 1.4 MW iron core motor
- Rotational speed 6,800 rpm (12-pole machine)
- Power density goal 16 kW/kg
- Efficiency target >98%
- Salient pole rotor with REBCO coils conduction cooled to 62 K
- In-shaft Stirling cryocooler for cooling the rotor
- Stator has conventional copper coils
- Expecting 3x lower losses and weight than current aircraft motors and generators



## Key Features

- Uses standard aircraft cooling systems
- Direct drive at optimal turbomachinery speeds (no gearbox)
- Can be shut off if fault occurs (wound field)

Ref: Scheidler, J.J. et al, "Thermal vacuum chamber demonstration of a cryocooled, HTS rotor for a 1.4 MW electric machine for electrified aircraft propulsion", Paper # 4LPo1E-01 Presented at ASC-2022



# VUW-RRI 3 MW, 4500 RPM MOTOR

- Robinson Research Institute (RRI) Victoria University of Wellington is developing superconducting motors for aircraft applications
- Final goal: Build all superconducting 3 MW motor at 4500 RPM using the following steps;
  - 100 kW, 4500 RPM motor with REBCO field coils and conventional copper stator
  - 3 MW, 4500 RPM motor with REBCO field coils and conventional copper stator
  - 3 MW, 4500 RPM motor with REBCO field coils and superconducting stator
- Field winding powered with flux pumps constructed in-house
- Cryocooler integrated with the shaft cools rotor coils
- Some features of these machines are included in the following viewgraphs

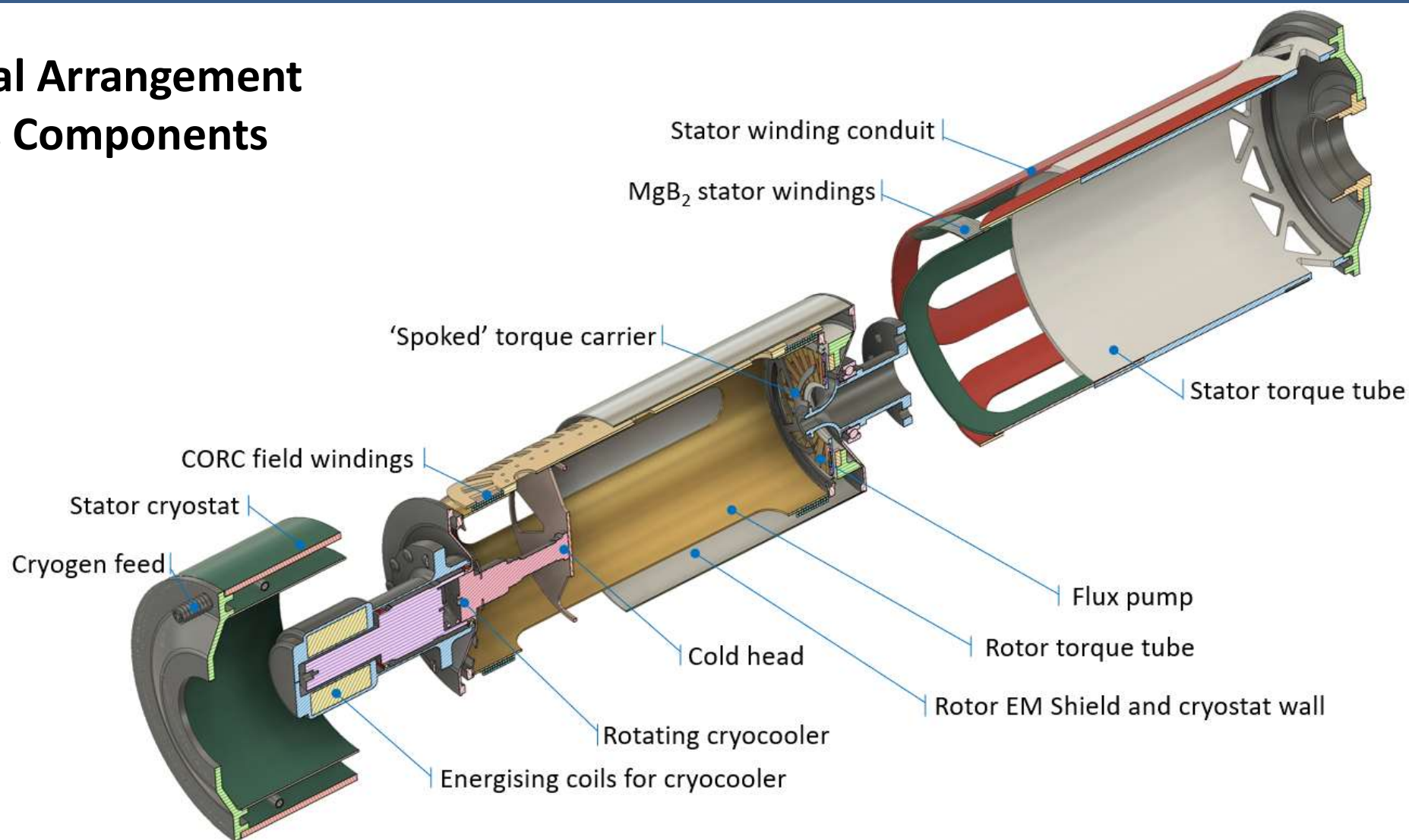
Parameter	3 MW Motor Specs.	100 kW Prototype Motor Specs
Nominal Rating, kW	3,000	100
Number of phases	3	3
Nominal DC bus voltage, V	1,500	1,500
Number of poles	4	4
Rated rotational speed, RPM	4,500	4,500
Rated frequency, Hz	150	150
Rotor field excitation coil temp., K	40	40
Stator operating temp., K	20	300
Power source	Electric Drive	Electric Drive

End goal: Build and test a 3 MW, 4500 RPM Motor



# VUW-RRI 3 MW, 4500 RPM MOTOR - LAYOUT

## Conceptual Arrangement of Various Components





# VUW-RRI 100 kW, 4500 RPM MOTOR (2023)

- 100 kW, 4500 RPM motor under construction to serve as a test-bed for evaluating different technologies
- Motor 360 mm in dia and 550 mm long (axially) has an efficiency target of 96.4%
- Race-track saddle coils used for both rotor and stator
- REBCO CORC cable used for the field coils on the rotor
- Field coils are conduction cooled to the structural support cylinder
- Support cylinder is cooled with a cryocooler integrated within the shaft
- Field coils powered with a 2.8 kA flux pump integrated on the rotor
- Stator race-track saddle shaped coils built using copper Litz wire
- Both rotor and stator coils have been practice built using copper cables

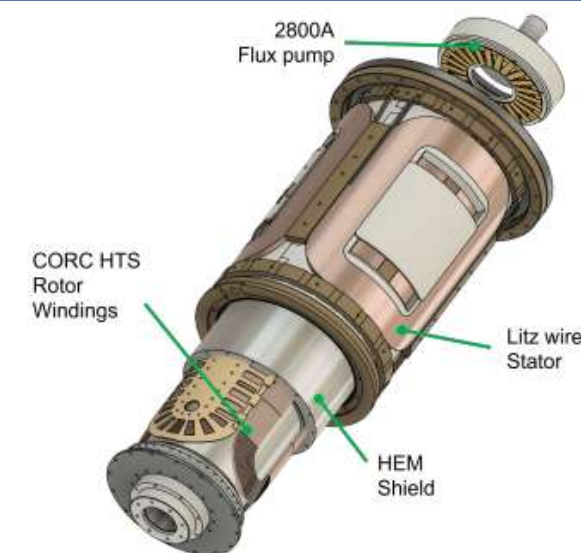
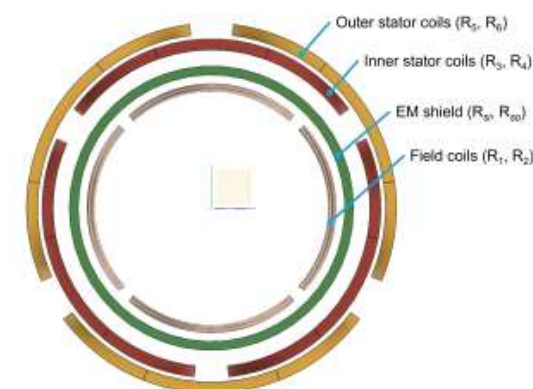


Fig. 1. 100-kW motor exploded view showing HTS rotor, litz wire stator and 2800A HTS Dynamo.



Ref: S. S. Kalsi, J. G. Storey, J. M. Brooks, G. Lumsden and R. A. Badcock, "Mechanical and electrical design of a synchronous superconducting aircraft motor", Presented at ASC-2022, Paper #ASC2022-4LPo1D-09

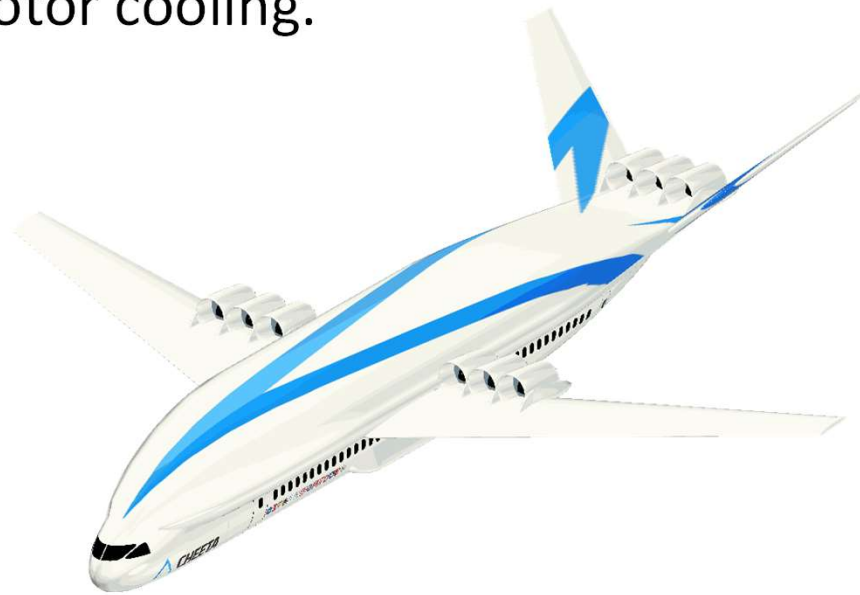
# RAYTHEON SOARING 2.5 MW, 5000 RPM MOTOR

- Raytheon is developing a 2.5 MW, 5000 RPM motor under an ARPA-e program
- Goal: build an ALL-SC-Motor -- both rotor and stator employ superconducting coils
- Field winding is powered with a flux pump integrated on the rotor
- Stator winding uses low AC loss superconductors operating at nominal 20 K
- Motor is cooled with a magnetic cryocooler

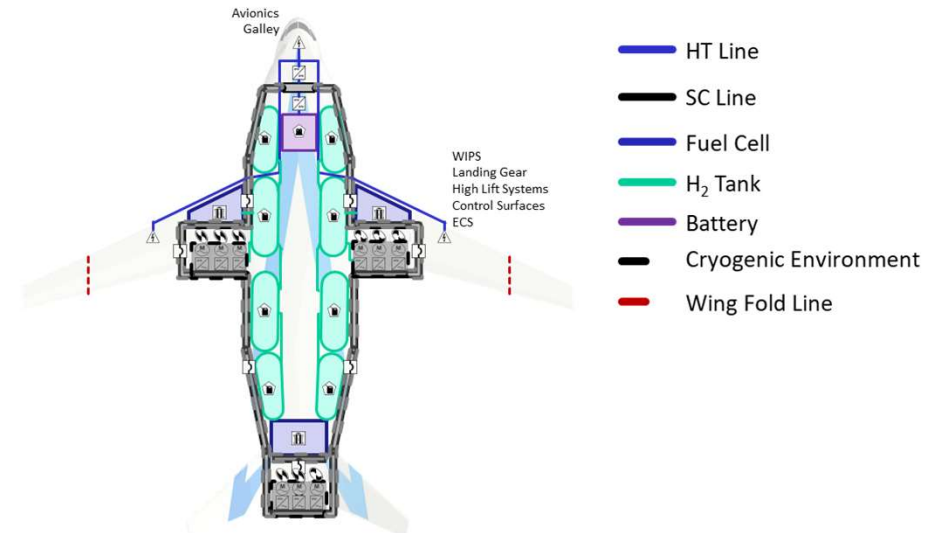
*Most Challenging Project: Opting for a fully superconducting motor*

# CHEETA – SC POWERTRAIN FOR HYDROGEN-ELECTRIC AIRCRAFT

- Hydrogen-electric aircraft with synergistic use of LH2 for energy storage and cryogenic cooling
- For all motors, assuming 68 % of available enthalpy of vaporization in fuel allocated for motor cooling.



Stautner, W., Ansell, P.J. and Haran, K.S., 2022. CHEETA: An All-Electric Aircraft Takes Cryogenics and Superconductivity on Board: Combatting climate change. *IEEE Electrification Magazine*, 10(2), pp.34-42.

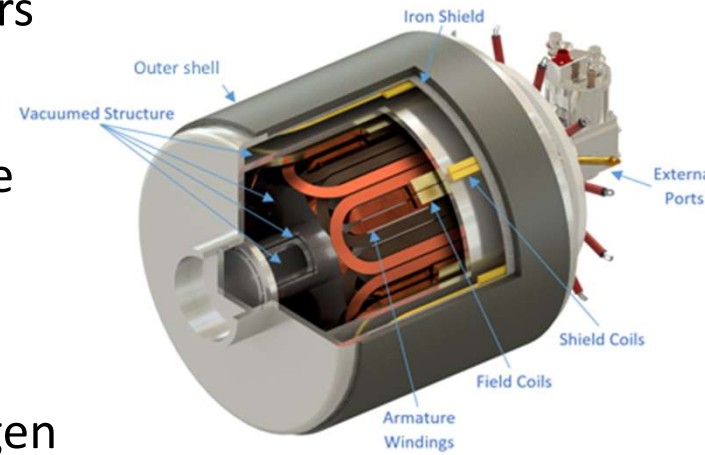


Main Parameters

Total Energy	1068 GJ
Propulsive power	40 MW
Mission length	8 hrs
Amount of fuel (LH2)	14833 kg
Number of motors	16
Motor Power	2.5 MW
Motor Speed	4500 rpm
LH2 Boil-off rate	0.01 kg/s
Cooling budget	4.3 kW

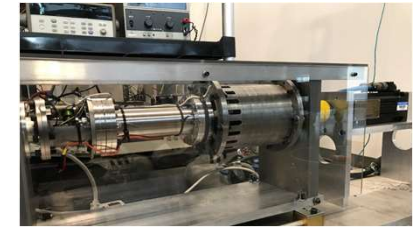
# CHEETA – FULLY SUPERCONDUCTING LH2 COOLED MOTOR

- CHEETA is developing 3 - 5 MW, 4500 RPM motors under a NASA-ULI program
- Motor specifications are summarized in the table
- Goal is to build an ALL-SC-Motor; both rotor and stator coils employing superconductors
- This motor configuration has a stationary hydrogen cooled, superconducting armature
- Stator winding uses MgB2 wire with fine filament diameter for reducing AC losses and operates at nominal 25 K
  - High conductivity aluminum is a possible alternative
- REBCO field coils operated at about 40-50K
- Component tests by 2022, motor prototype by 2024



Nominal power (MW)	2.5
Nominal speed (rpm)	4500
Number of poles	8
Outer Diameter [m]	0.5
Machine total length [m]	0.75
Active length [m]	0.87
Average torque [Nm]	7045
Air-gap flux density [T]	0.63
Total loss [W]	2656
Active weight [kg]	13

## Component development:



Rotor mounted cryogenics



Superconducting coils

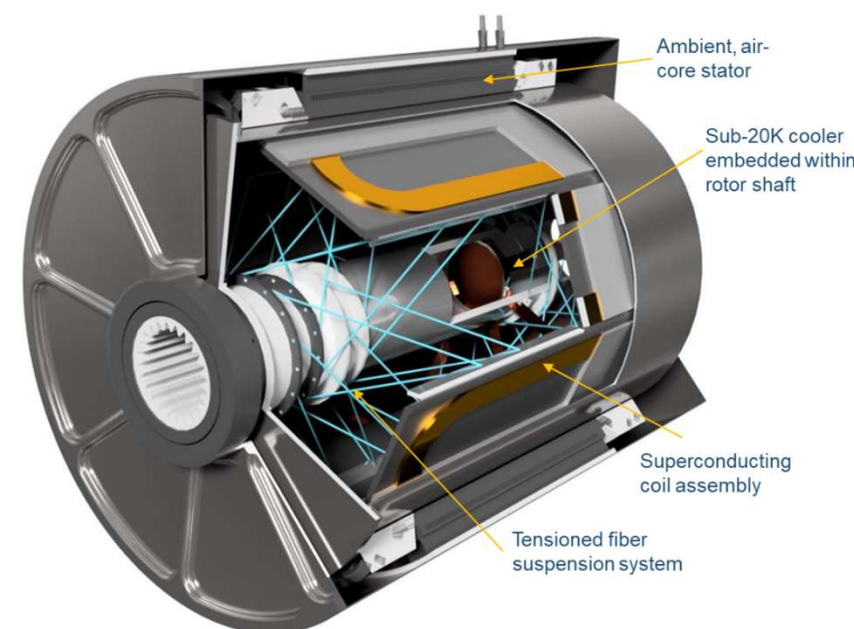


LH2 heat exchangers

# ARPA-E CRUISE: PARTIALLY SUPERCONDUCTING MOTOR

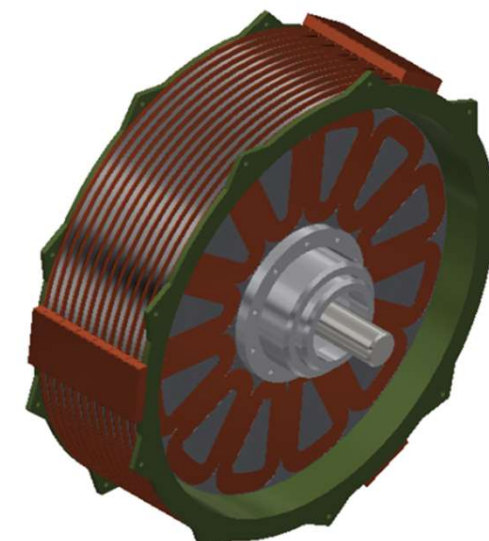
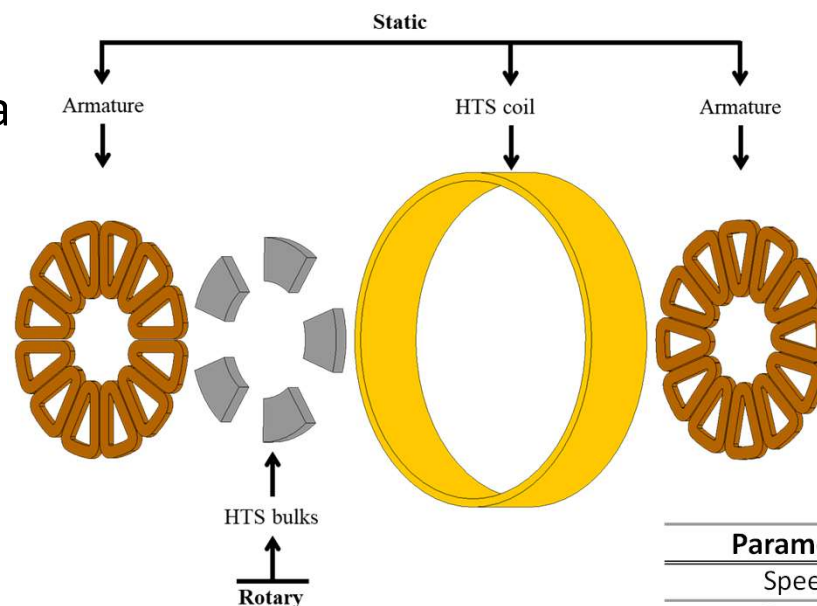
- Partially superconducting air-core synchronous motor
- Conduction cooled field winding
- Stirling-cycle cooler integrated with a low-loss rotor
- Magnetic fields an order of magnitude higher than conventional machines
- Coil suspension and torque transfer system with tensioned fibers
- Increase specific power with higher ‘ampere-turns’ of excitation and “armature” windings, featuring
  - Removed ferromagnetic components
  - Increased air gap flux density
  - Increased electrical loading
- Goal: 10 MW, 3000 RPM propulsion motor weighing less than 250 kilograms. Demonstrate 5 MW motor by 2025

Metric	State of the Art	Target
<i>Specific power (active)</i>	10 kW/kg	50-60 kW/kg
<i>Efficiency</i>	96%	99.4%
<i>Single stage cryocooler</i>	35 K (no load)	<20 K (no load)
<i>Cryogenic rotor heat-load</i>	100 W	10 W
<i>Airgap flux density</i>	1 T	3-4 T
Armature ac field	500 T/s	5000 T/s



# SAFRAN FLUX MODULATION MOTOR

- Large magnetic field can be produced from HTS wires and magnets without a need for iron core
  - $\frac{R^2L}{M}$  is increased by the removal of iron
  - $B$  can be increased or kept constant
- Large current density can be carried through and HTS or cryogenically cooled armature
  - $H$  can be increased with reduced losses
- **Specific power can be increased without increasing the speed**



Parameter	Value
Speed	5000 tr/min
Power	261 kW
Mass (active)	21.4 kg
Mass (passive)	~127 kg
Specific power	~1.8 kW/kg
Efficiency	95,3 %
Voltage	310 V
Current	280 A

Construction and Testing in 2023

References:

1. R. Dorget, S. Ayat, R., A. Cipriani, J. Leveque, J. Labbe, T. Lubin, M. Sitko, J. Tanchon, and J. Lacapere, "Construction of a 250 kW Superconducting Flux Modulation Prototype for Aircraft Application", Presented at ASC22 in Honolulu 23-28, 2022
2. R. Dorget, S. Ayat, R., Biaujaud, J.M. Gaillard, A. Cipriani, J. Tanchon, J. Lacapere, T. Lubin and J. Leveque, "Superconducting flux modulation machines for Aircraft propulsion", EFATS-2021
3. R. Dorget, S. Ayat, A. Cipriani, J. L ev eque, J. Labb e, T. Lubin, M. Sitko, J. Tanchon, J. Lacap ere, "Superconducting flux modulation machines for hybrid and electric aircraft", EFATS-2022

# AIRBUS ASCEND TESTING FACILITY

- Airbus test stand 'ASCEND' for testing motors and other supporting sub-systems needed for an aircraft
- Three-year project includes the following features;
  - Cryogenic electrical protection systems
  - AC and DC distribution utilizing superconducting cables
  - Motor control unit cooled to cryogenic temperature
  - Superconducting motor
  - Cryogenic system based on cryocoolers; could be converted to LH2 storage for future aircrafts (large cooling power)
- Motor test capability includes;
  - Mechanical power of 500 kW at 5000 RPM
  - DC supply bus at 300 V
  - Limit switching current to < 2000 A
  - Available coolant temp. of 25 K and conductor temp. < 35 K

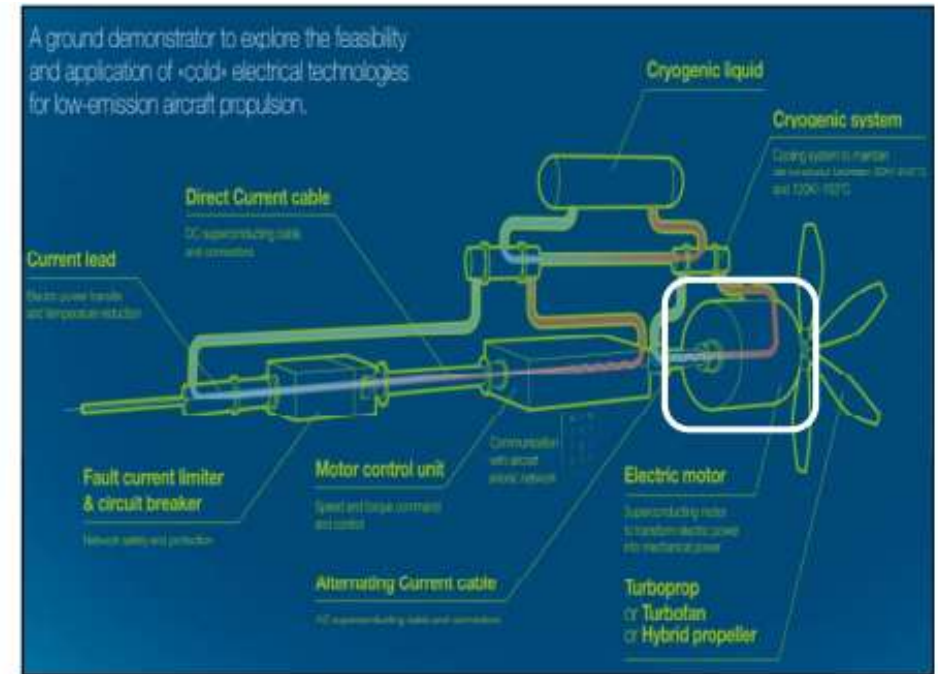


Fig 1. All components of the cryogenic powertrain

UpNext

This facility is expected to test emerging technologies for aircraft applications

# GE ~15 MW WIND POWER GENERATOR

- GE is developing a ~ 15 MW wind power generator under a DOE program
- Generator employs stationary DC field winding constructed using low-temperature NbTi coils
- Field coils are cooled with a stationary cryocooler, thus avoiding complications of coolant and power transfer to the rotor
- AC armature winding rotates inside the field coil assembly – it is constructed and cooled using established industry practices
- Power is collected from the rotating armature through brushes



Ref: M. Parizh, et al, "High-power Superconducting Wind Generator", ISS-2022  
29 November 2022

GE believes generators rated > 15 MW could compete with the conventional technology



# WHAT WILL MAKE HTS MACHINES ATTRACTIVE?

- HTS technology amply demonstrated – need for economic viability:
  - Low-cost HTS wire and
  - Reliable and affordable cooling system
- **MUST:** Improve wire performance (e.g., extended window of operation in terms of higher temperature and magnetic field and lower cost)
- Building HTS machines by leveraging synergies of off-the-shelf-components
- Designing machines by including dynamic variation of operating parameters (e.g., temperature, excitation, amount of fuel and environment)
- HTS machines may have sweet applications where other technologies are not feasible; Example: Aircraft Motors and Generators, and > 20 MW wind power generators
- An affordable and reliable HTS technology may extend its applications to central power stations, wind turbine generators, ship propulsion and industrial motors

*Future of the HTS technology looks very promising*

# Questions

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