



**UNIVERSITÉ
DE GENÈVE**

FACULTÉ DES SCIENCES



FONDS NATIONAL SUISSE
DE LA RECHERCHE SCIENTIFIQUE

Field and temperature scaling of the critical current density in commercial REBCO coated conductors

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Outline

- *Research on coated conductors @ UNIGE*
- *Overview of the industrial REBCO CCs*
- *$J_c(B, T, \theta)$ surface, **scaling** relations for the **temperature** and **field** dependences*
- *Critical current under mechanical loads*
- *Thermo-physical properties: thermal conductivity and normal zone propagation velocity*



Motivation

Towards **20 Tesla** accelerator magnets for HEP



Today : the record collision energy in LHC is 8 TeV

Scope : Future Circular Colliders, collision energy up to 100 TeV
Shed light on the physics beyond the Standard Model

Towards all-superconducting **30 T-class** solenoidal magnets



Today : commercial systems with $B_{max} = 23.5 \text{ T @ } T = 2.2\text{K}$

Scope : high resolution NMR spectrometers, high field laboratory magnets

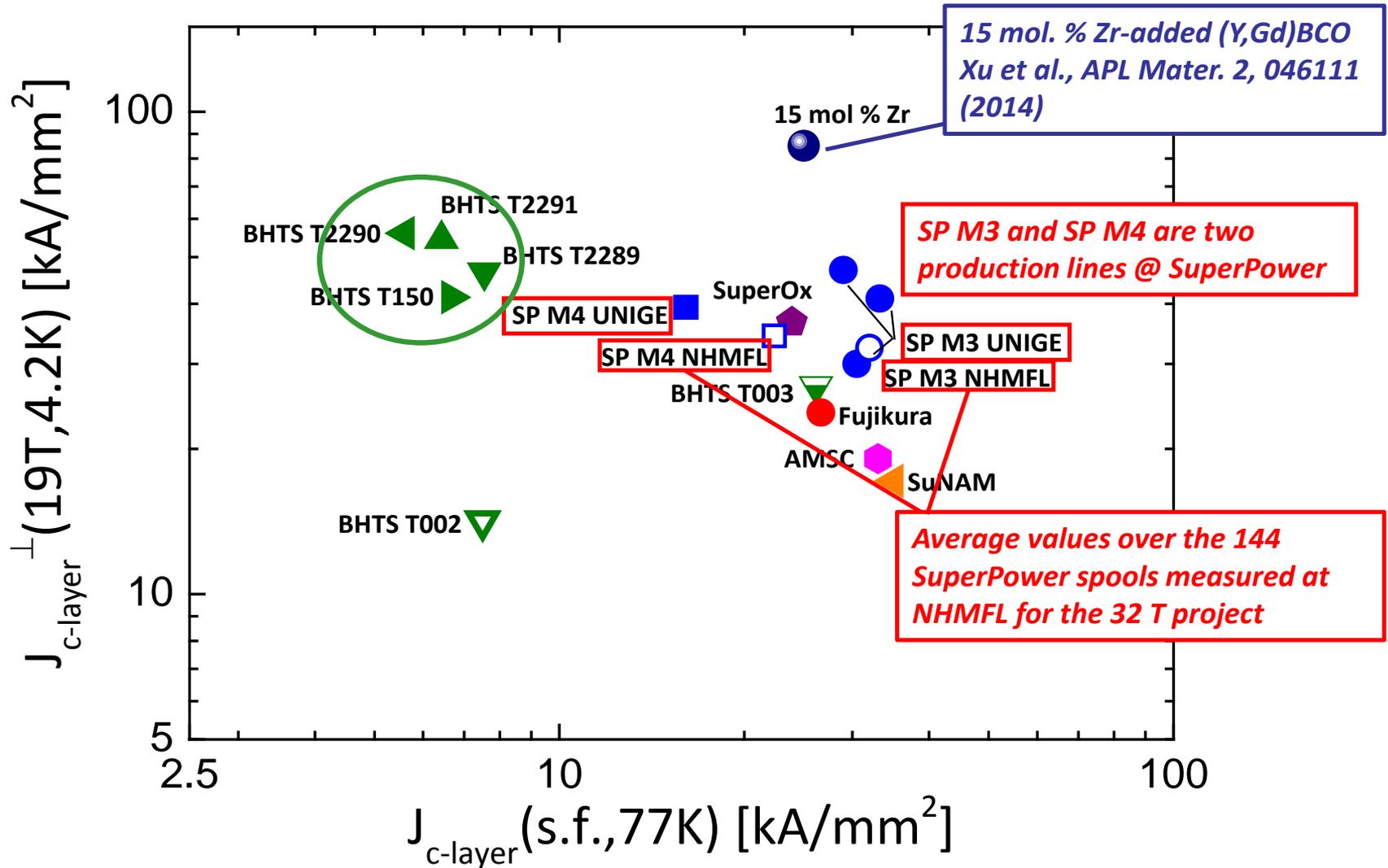


Overview of the industrial CCs



| |  |  |  |  |  |  |
|------------------------------|---|---|--|---|---|---|
| RABiTS | ✓ | | | | | |
| IBAD | | ✓ | ✓ | ✓ | ✓ | ✓ |
| physical deposition | | ✓ | ✓ | ✓ | ✓ | |
| chemical deposition | ✓ | | | | | ✓ |
| in situ process | | ✓ | ✓ | | ✓ | ✓ |
| ex situ process | ✓ | | | ✓ | | |
| substrate | NiW 75 μm | SS 100 μm | Hastelloy 75 μm | Hastelloy 60 μm | Hastelloy 60 μm | Hastelloy 50 μm |
| thermal stabilization | Laminated (2 sides) | Electroplated | Laminated (1 side) | Electroplated | Electroplated | Electroplated |

Performance overview: $J_c(s.f., 77K)$ vs. $J_c^\perp(19T, 4.2K)$





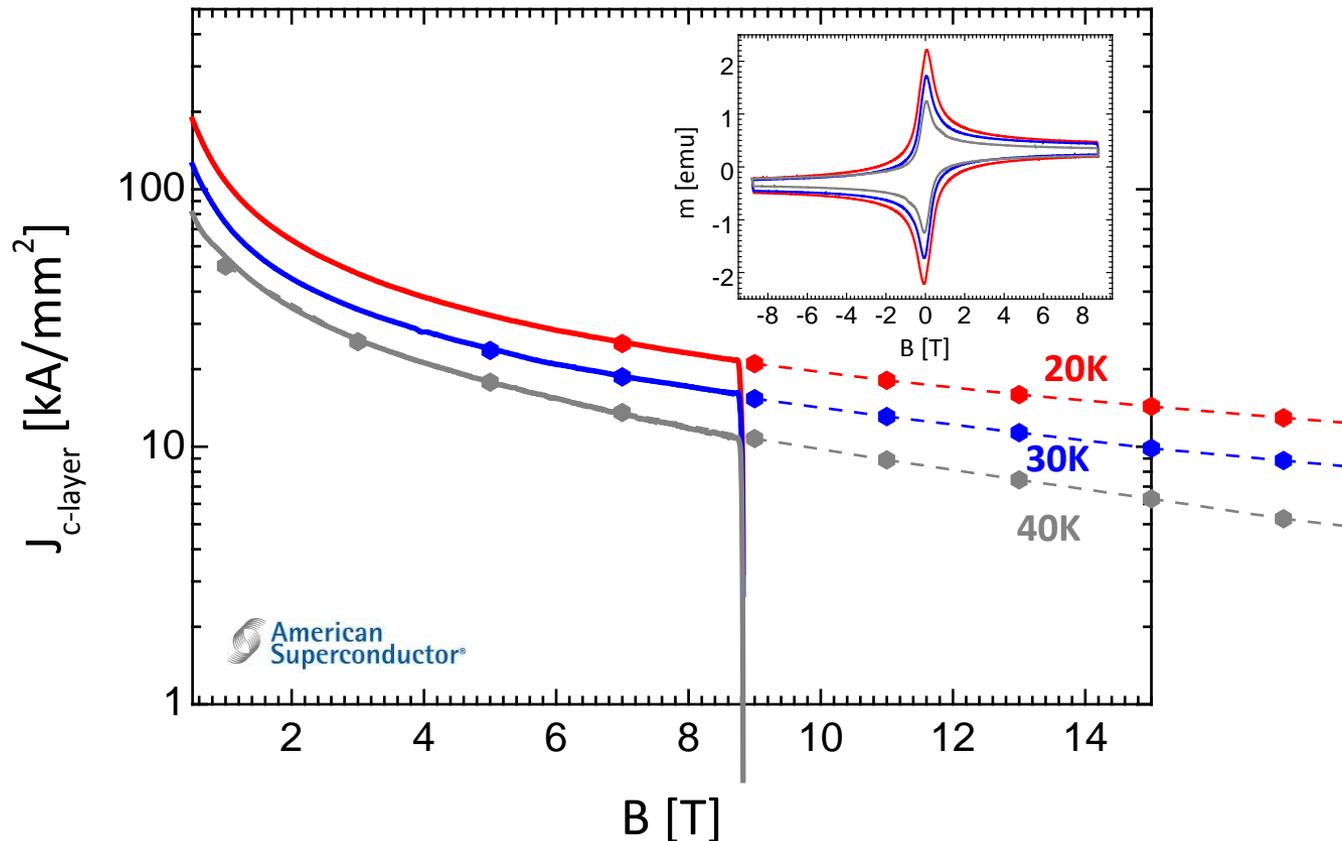
Practical characterization of REBCO CCs

Applications @ low temperature / high fields

- *J_c depends strongly on the orientation of the tape wrt the magnetic field*
- *B_{c2} at low temperature is ~ 100 T*
- *The operating temperature margin is 30 – 40 K*
 - *Thermo-physical properties, $c(T,B)$ & $\kappa(T,B)$, are essential*
- *The response of the tape to mechanical loads depends on its architecture (electromechanical properties)*



Transport and magnetic measurements of $J_c(B, T, \theta)$

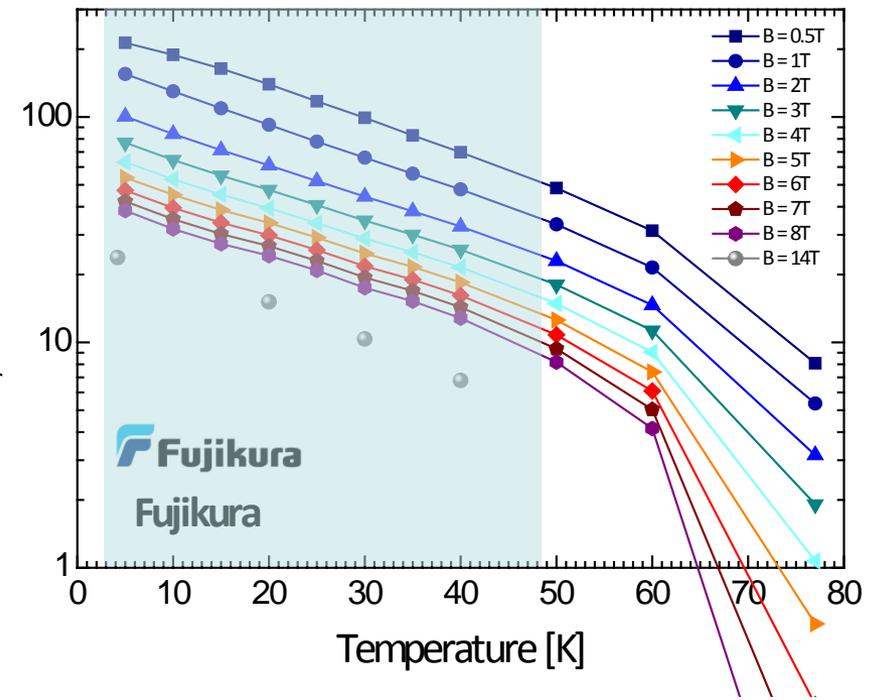
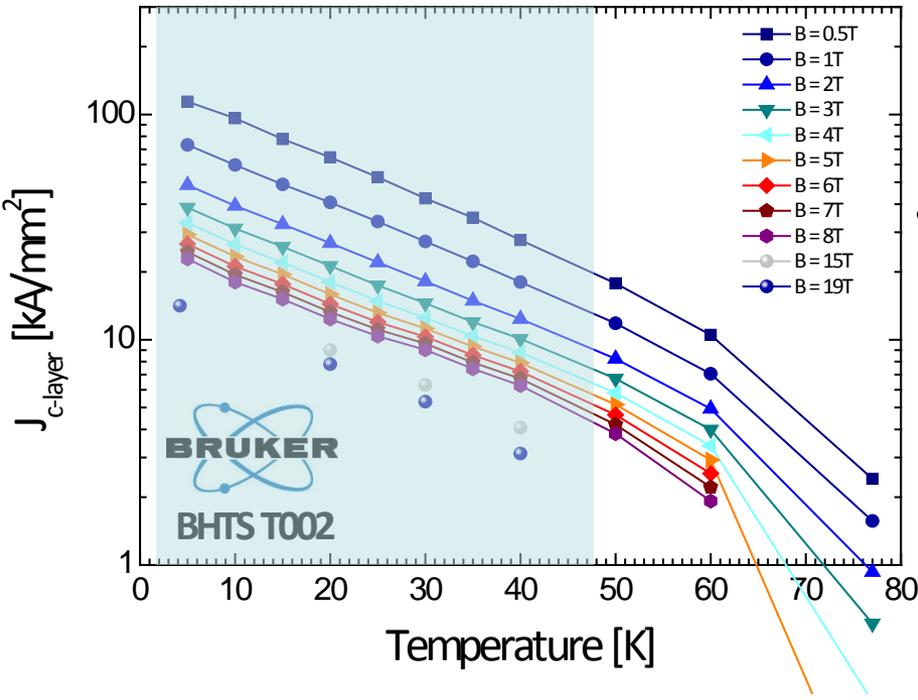


Only a limited portion of the critical surface is practically accessible from transport measurements

Magnetization measurements are the tool to explore a larger region of the critical surface

Temperature dependence of J_c

$\theta = 0^\circ - B//c$

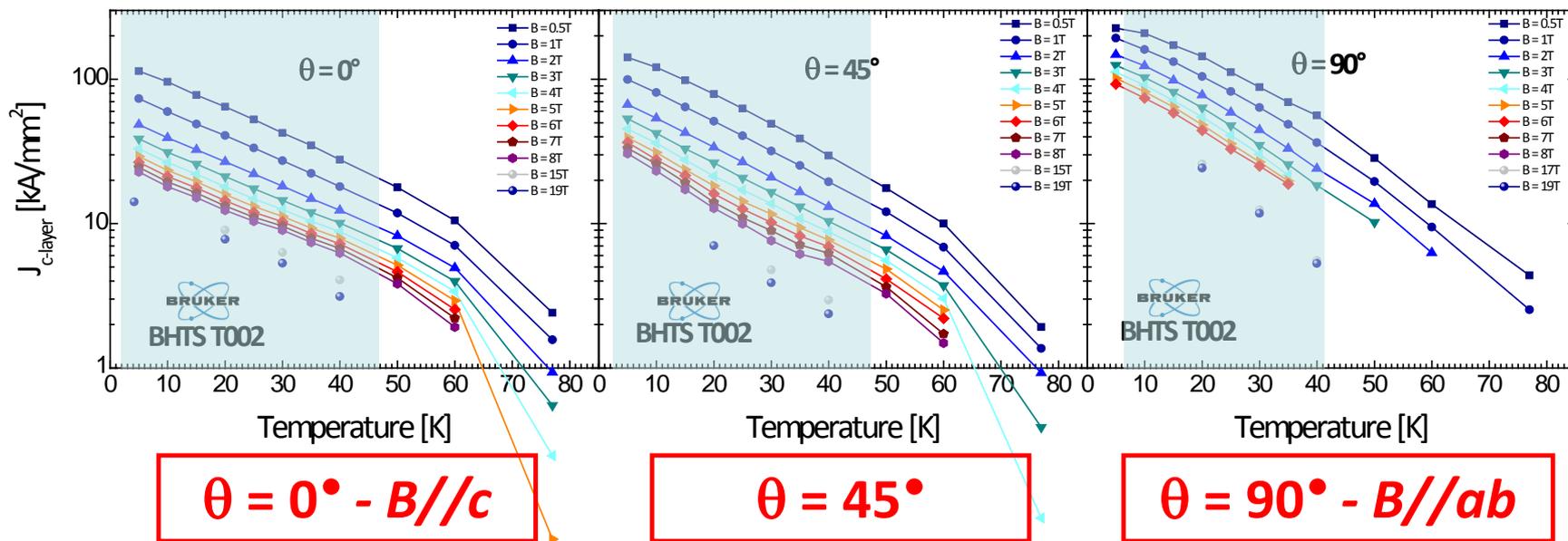


Temperature scaling relation

$$J_c(B, T) = J_c(B, T = 0) e^{-\frac{T}{T^*}} \Rightarrow \frac{J_c(B, T_1)}{J_c(B, T_2)} = e^{-\frac{T_1 - T_2}{T^*}}$$



Temperature dependence of J_c : 3 orientations

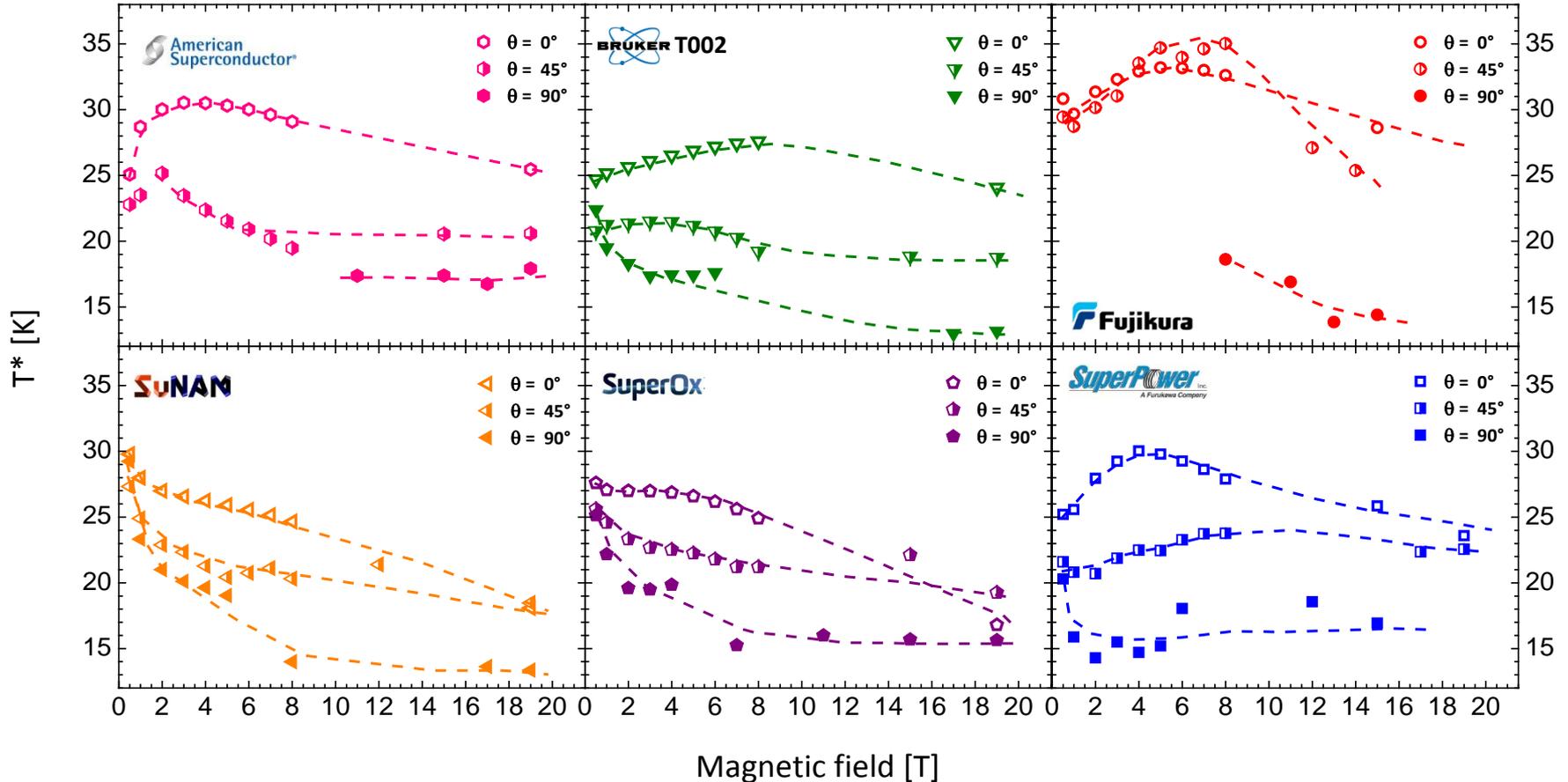


The temperature scaling relation $J_c(B, T) = J_c(B, T = 0) e^{-\frac{T}{T^*}}$ holds also at 45° and 90° for T up to 40 K

T^* ranges between 15 K and 35 K – it depends on field and orientation



Temperature scaling parameter T^*



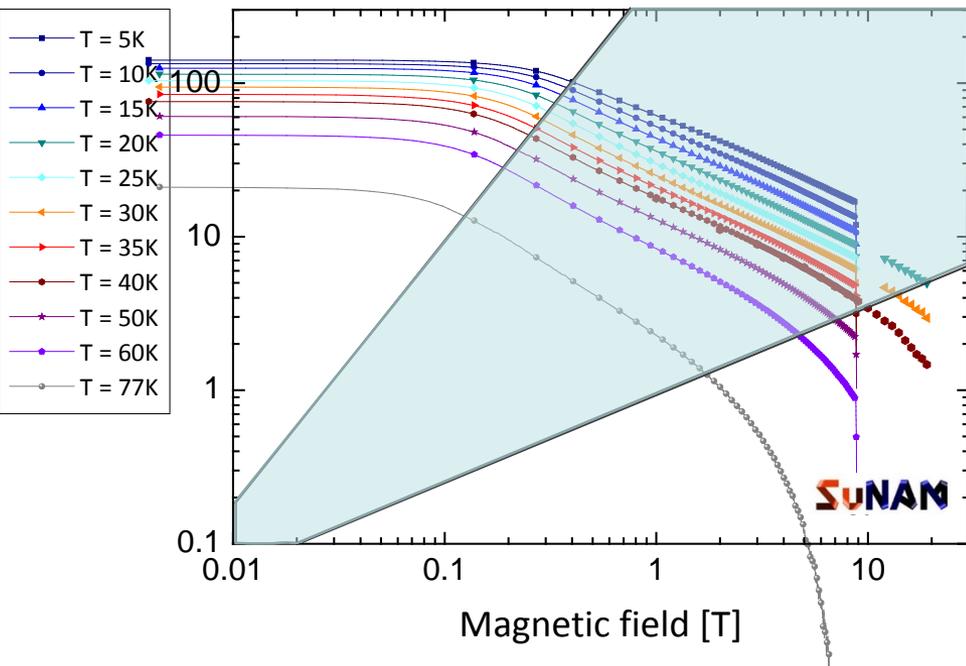
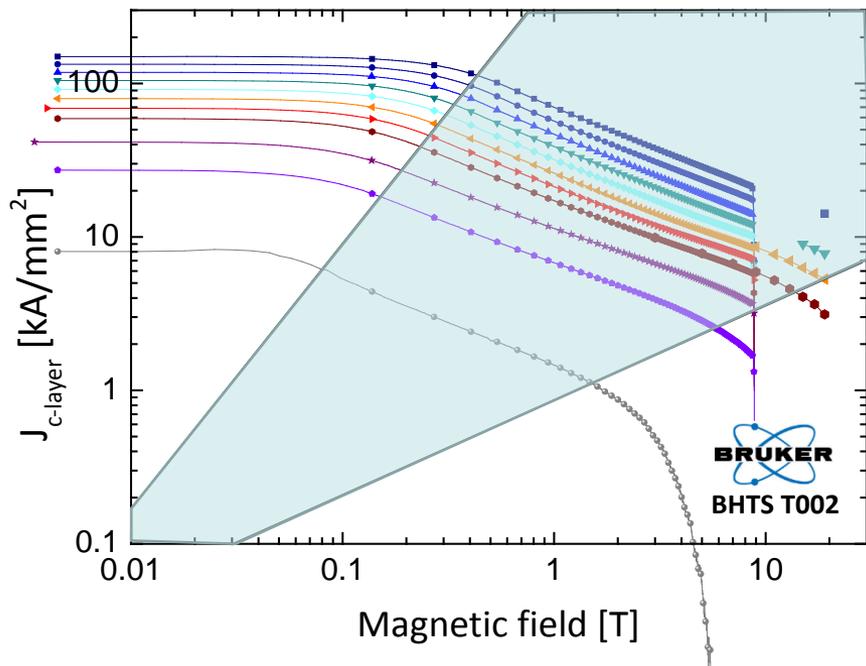
T^* ranges between 15K and 35K – it depends on field and orientation

Lower T^* values \Rightarrow faster decrease of I_c with increasing T



Field dependence of J_c

$\theta = 0^\circ - B//c$

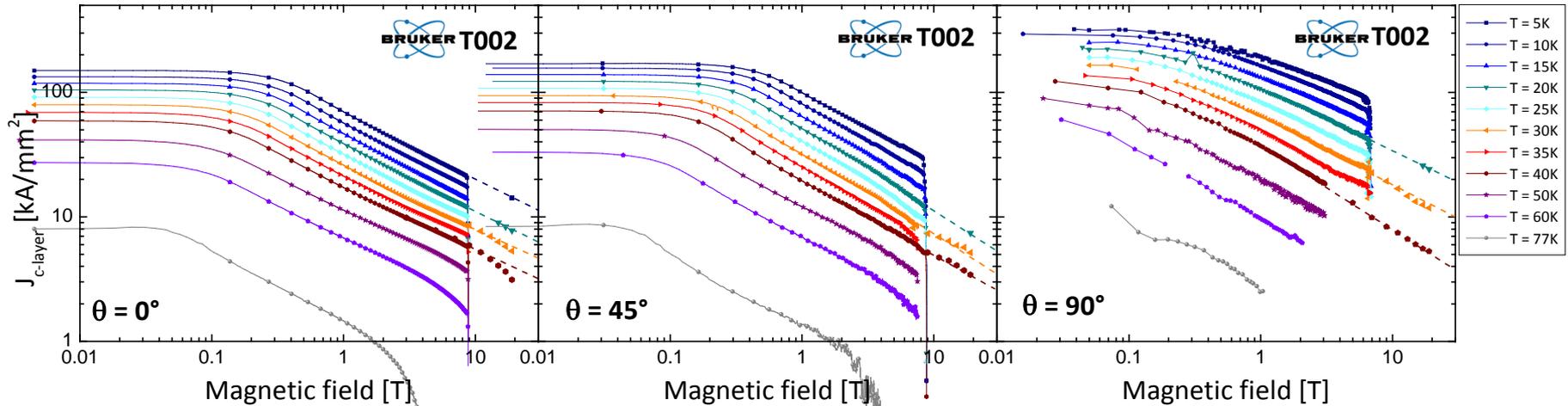


Field scaling law $J_c(B, T) = J_c(B = 0, T) B^{-\alpha}$

α is almost constant below 40 K, the value varies between 0.5 and 0.8



Field dependence of J_c : 3 orientations



$\theta = 0^\circ - B//c$

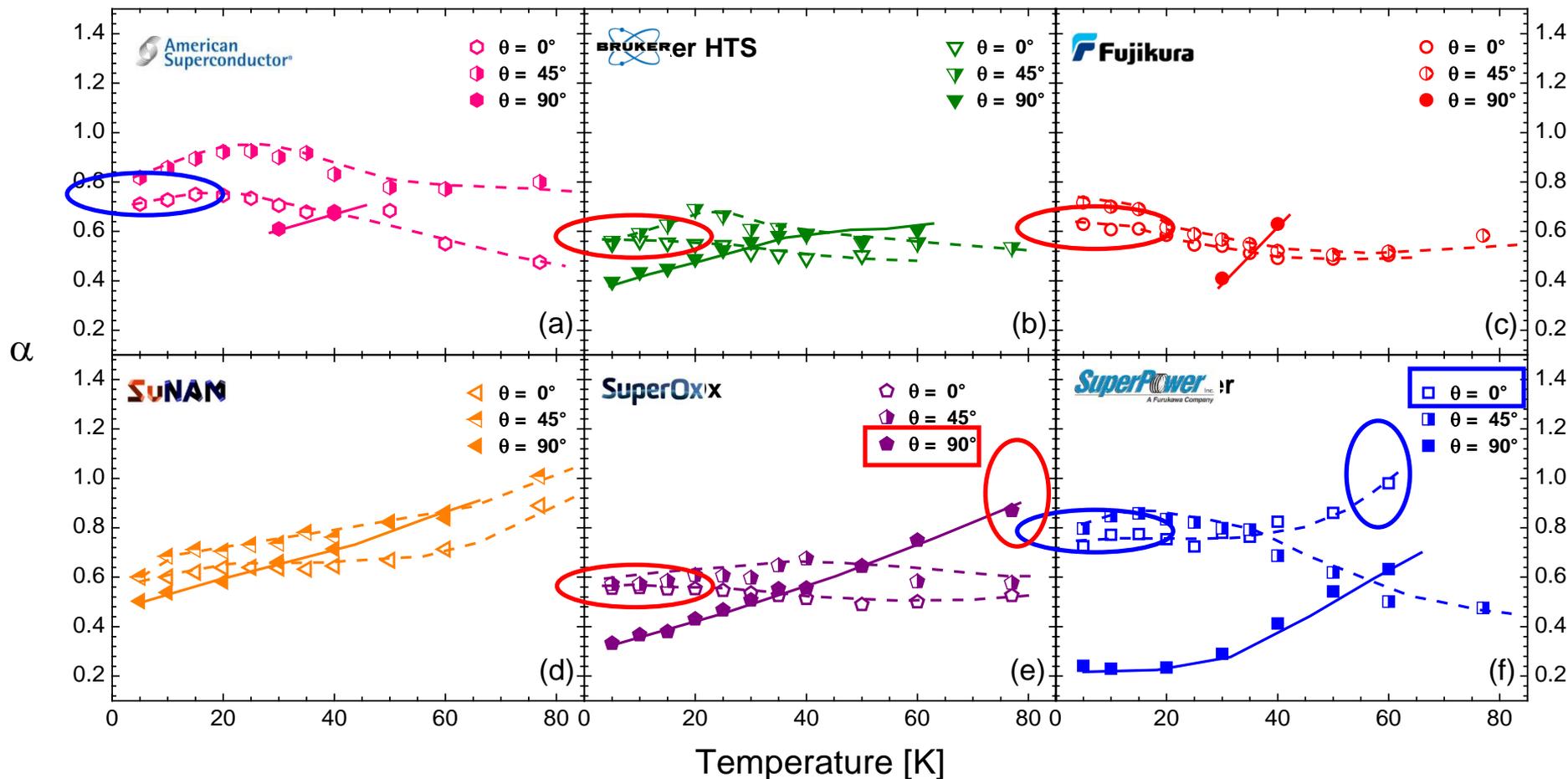
$\theta = 45^\circ$

$\theta = 90^\circ - B//ab$

Field scaling relation

$$J_c(B, T) = J_c(B=0, T) B^{-\alpha}$$

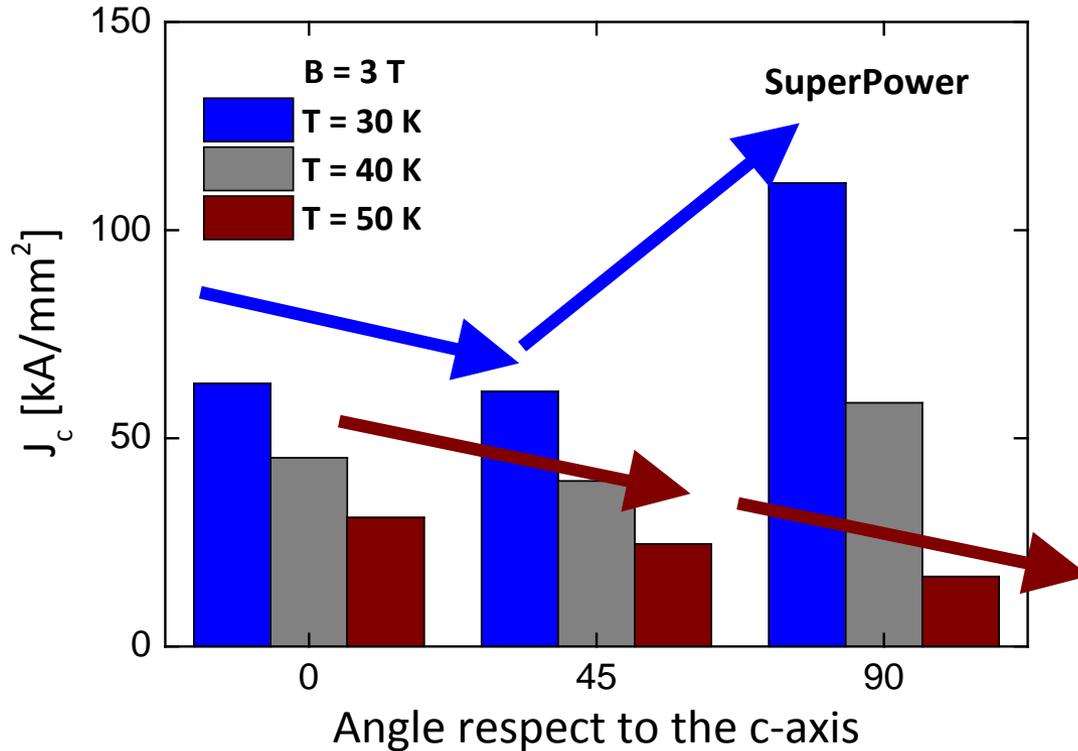
Field scaling parameter α



Higher α values \Rightarrow faster decrease of I_c with increasing B



$J_c(T)$ angular dependence: SuperPower with AP



Effects of artificial pinning on the J_c anisotropy

$$T < 30 \text{ K} \Rightarrow J_c(0^\circ) < J_c(45^\circ) < J_c(90^\circ)$$

$$30 \text{ K} < T < 40 \text{ K} \Rightarrow J_c(0^\circ) > J_c(45^\circ) \text{ and } J_c(0^\circ) < J_c(90^\circ)$$

$$T > 40 \text{ K} \Rightarrow J_c(0^\circ) > J_c(45^\circ) > J_c(90^\circ)$$

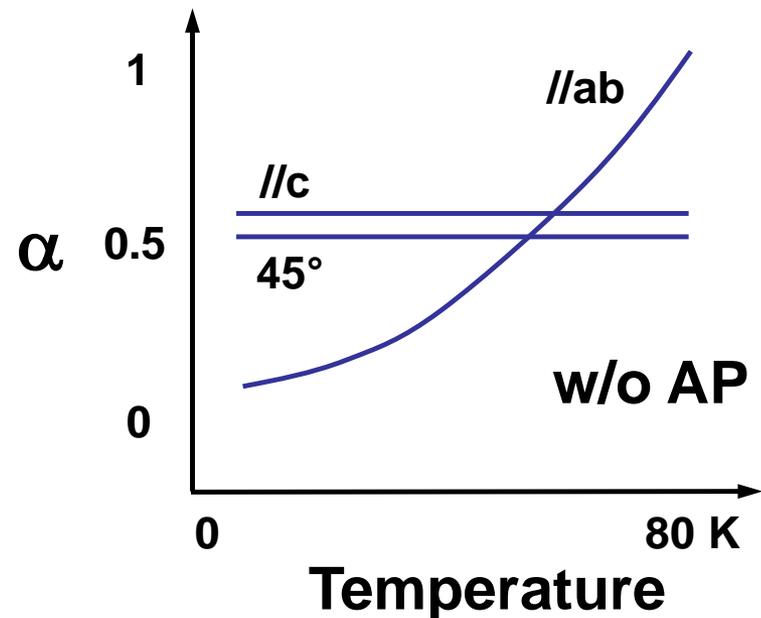
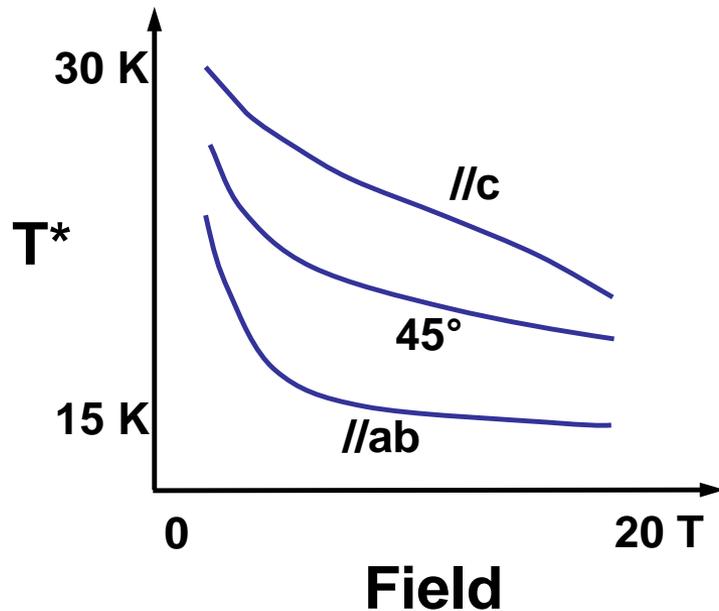


Temperature and field scaling of J_c

For temperatures below ~ 50 K, critical surface $J_c(B, T)$ in the form

$$J_c(B, T) = J_c(B=0, T=0) B^{-\alpha} e^{-\frac{T}{T^*}}$$

Scaling relation verified for $\theta = 0^\circ, 45^\circ$ and 90° , but T^* and α depend on θ



Lower T^* values \Rightarrow faster decrease of I_c with increasing T

Higher α values \Rightarrow faster decrease of I_c with increasing B

Critical current depends on

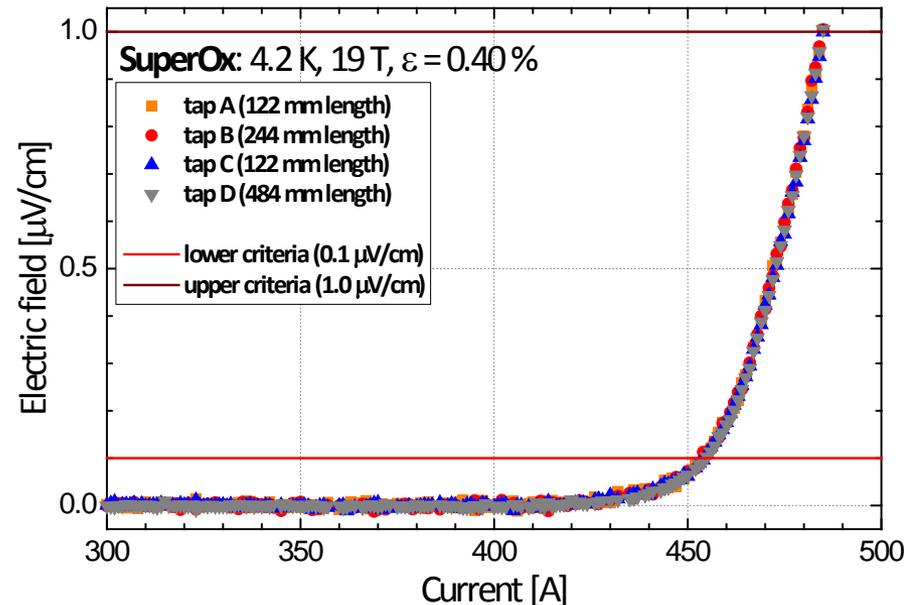
- *temperature*
- *field intensity*
- *field orientation*
- *mechanical loads*



I_c vs. axial strain: measurement method

Walters spring (WASP)

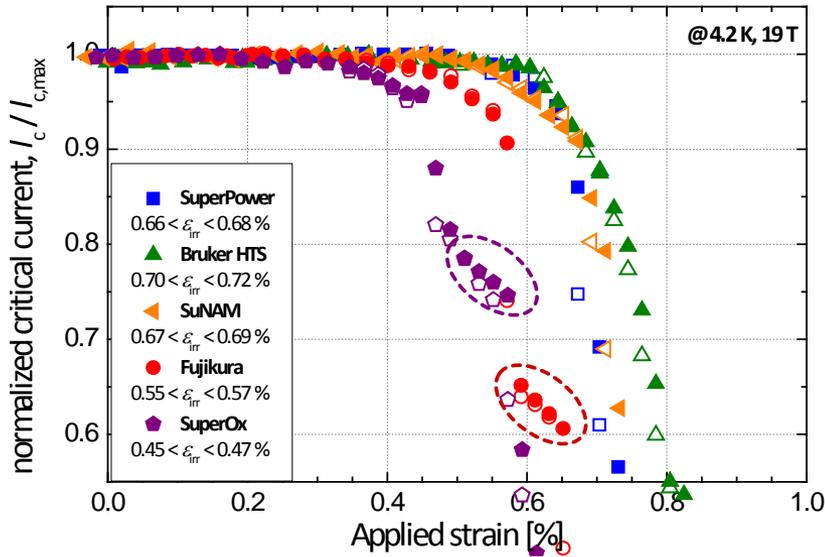
- Sample is soldered to Ti-alloy spring
- Turning the spring strains the sample
 - calibrated with strain gauges glued to the sample
 - sample is pre-strained upon cooldown due to thermal expansion mismatch
 - pre-strain is determined & subtracted
- 1m-long sample
 - precise
 - low noise
 - low I_c criteria
 - get n values



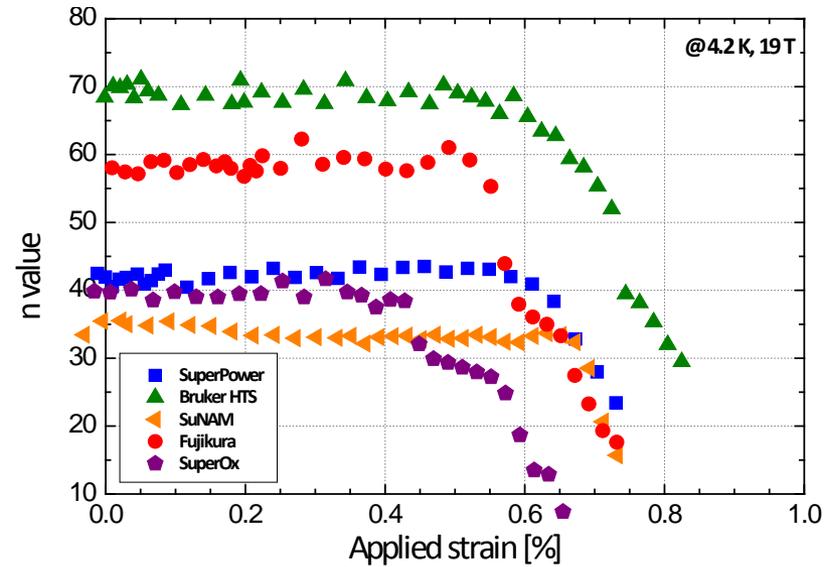


Dependence of I_c on axial strain @ 4.2 K, 19 T

I_c vs. applied strain



n value vs. applied strain

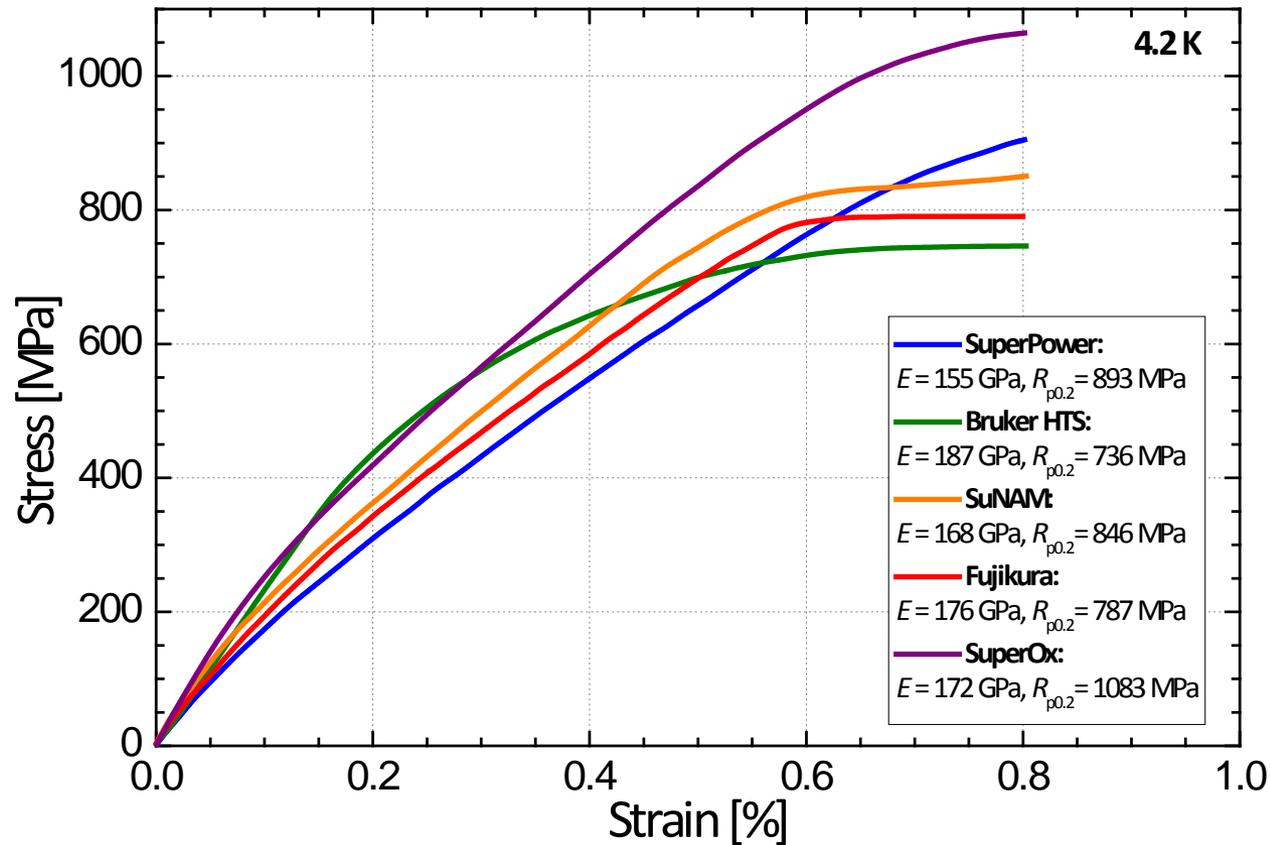


Fujikura & SuperOx: delamination \rightarrow steps \rightarrow lower ϵ_{irr}





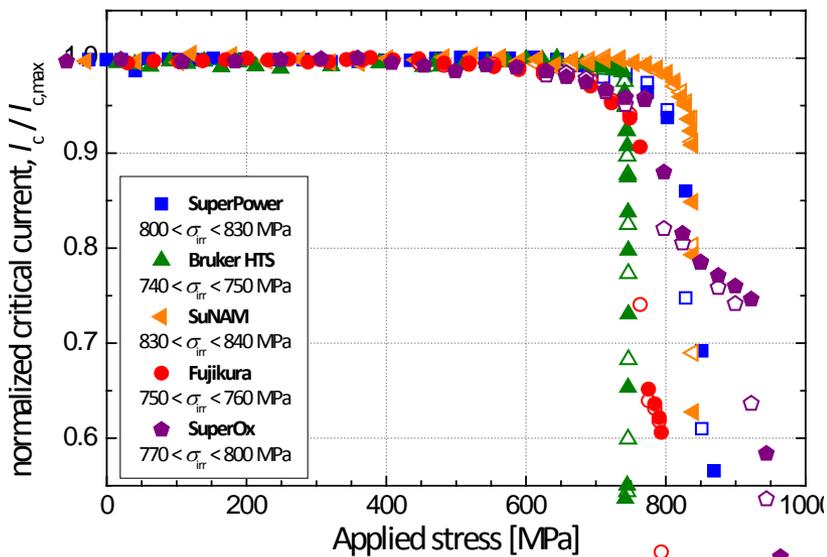
Stress vs. strain measurements @ 4.2 K



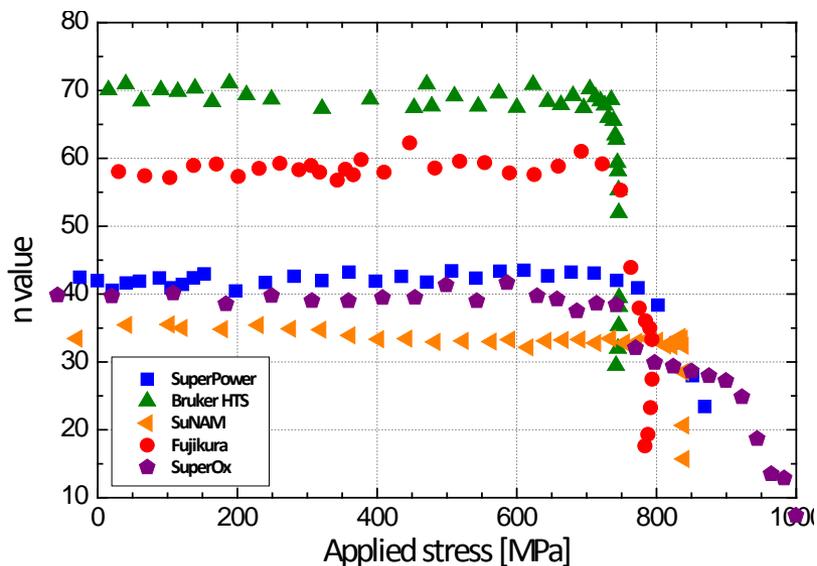


Dependence of I_c on axial stress @ 4.2 K, 19 T

I_c vs. applied stress

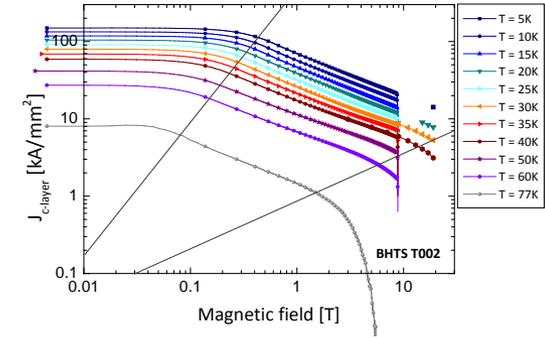


n value vs. applied stress

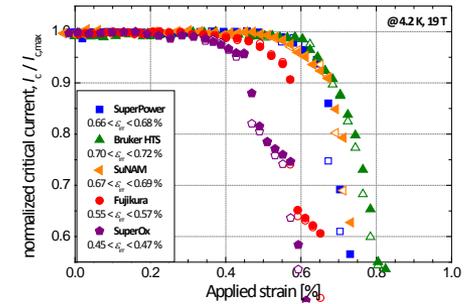


- All samples have a very similar behaviour
- Very low stress effect \rightarrow curves are flat in rev. region
- Irreversible limits σ_{irr} in 740 – 840 MPa range

Electromagnetic properties ✓



Electromechanical properties ✓



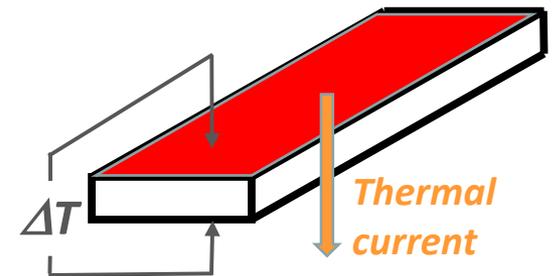
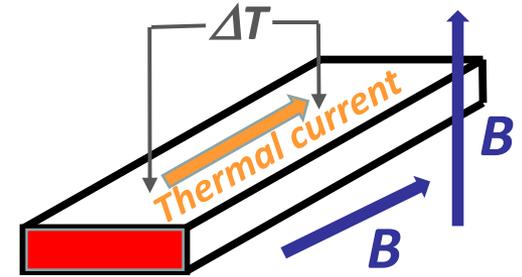
Thermo-physical properties → →



Thermal conductivity of REBCO CCs

Thermal conductivity is an essential parameter for QUENCH studies

- **Longitudinal thermal conductivity in magnetic fields up to $B=19$ T**
 B perpendicular & parallel to **thermal current**
- **Transverse thermal conductivity**



M. Bonura and CS, SuST 28 (2015) 025001

M. Bonura and CS, TASC 25 (2015) 6601304



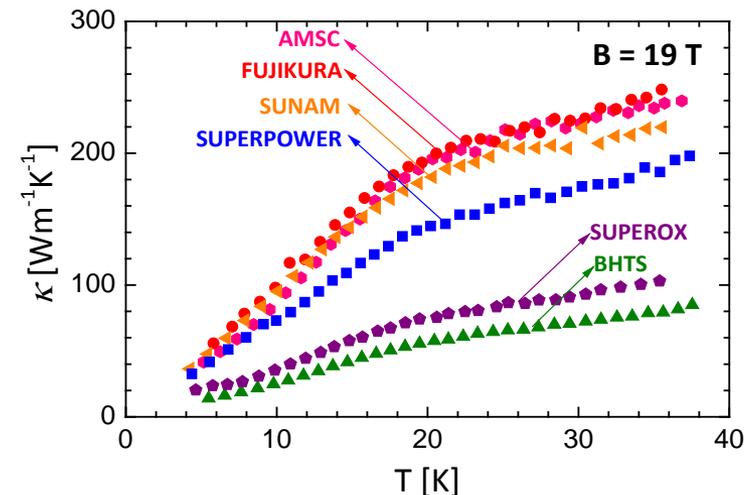
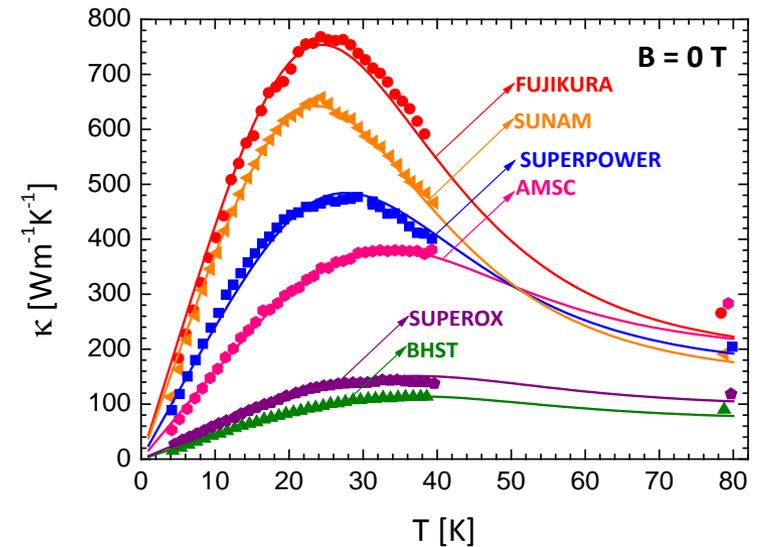
Longitudinal thermal conductivity

$$\kappa_{exp} = \sum_i \kappa_i \frac{S_i}{S_{tot}} \approx \kappa_{Cu} \frac{S_{Cu}}{S_{tot}} \quad \text{and} \quad \kappa_{Cu} = f(RRR_{Cu})$$

| Manufacturer | RRR_{Cu} [fit] | RRR_{Cu} [$\rho(T)$] | S_{Cu}/S_{tot} |
|--------------|---------------------|-----------------------------|------------------|
| AMSC | 20 | 19 | 0.51 |
| BHST | 14 | 17 | 0.20 |
| FUJIKURA | 62 | 59 | 0.44 |
| SUNAM | 69 | 61 | 0.34 |
| SUPEROX | 13 | 14 | 0.27 |
| SUPERPOWER | 39 | 42 | 0.40 |

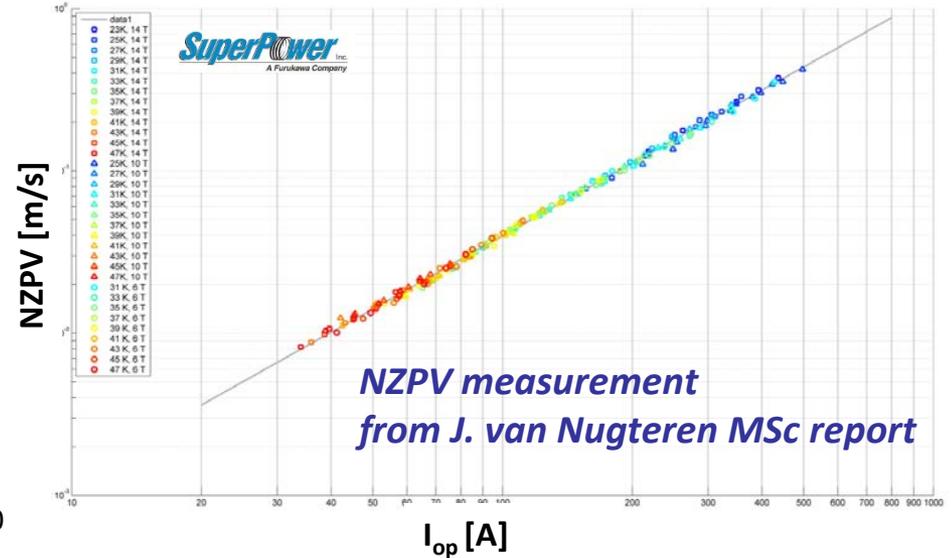
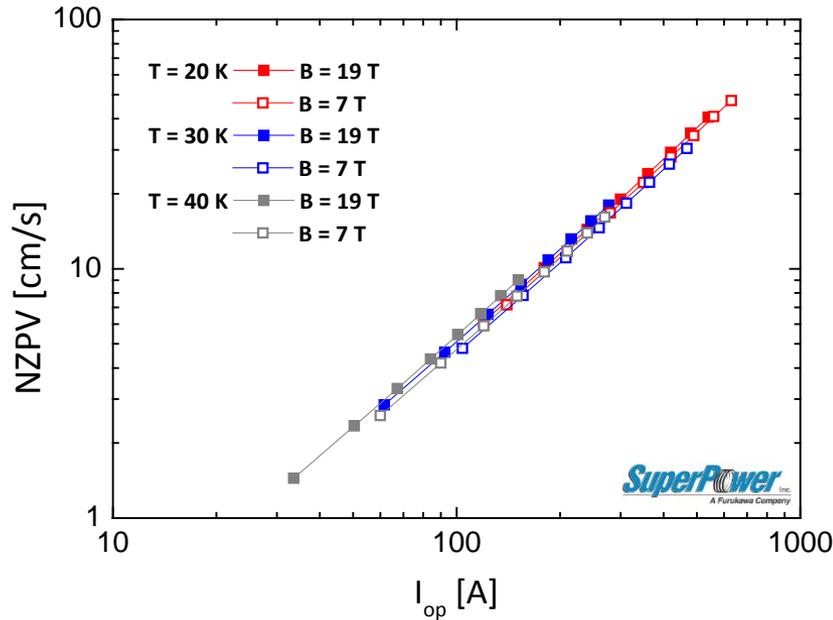
$\kappa(T, B=0T)$ can be estimated ($\pm 15\%$) from RRR_{Cu} and S_{Cu}/S_{tot}

$Cu/non-Cu$ ratio and RRR_{Cu} determine the in-field variation of κ





Normal zone propagation velocity



$$NZPV_L \approx \frac{I_{op}}{S_{tot}} \sqrt{\frac{\kappa(T_S)\rho(T_S)}{\int_{T_{op}}^{T_S} c_S(T_S)dT \left[c_n(T_S) - \frac{1}{\kappa(T_S)} \frac{d\kappa}{dT} \Big|_{T=T_S} \int_{T_{op}}^{T_S} c_S(T_S)dT \right]}}$$

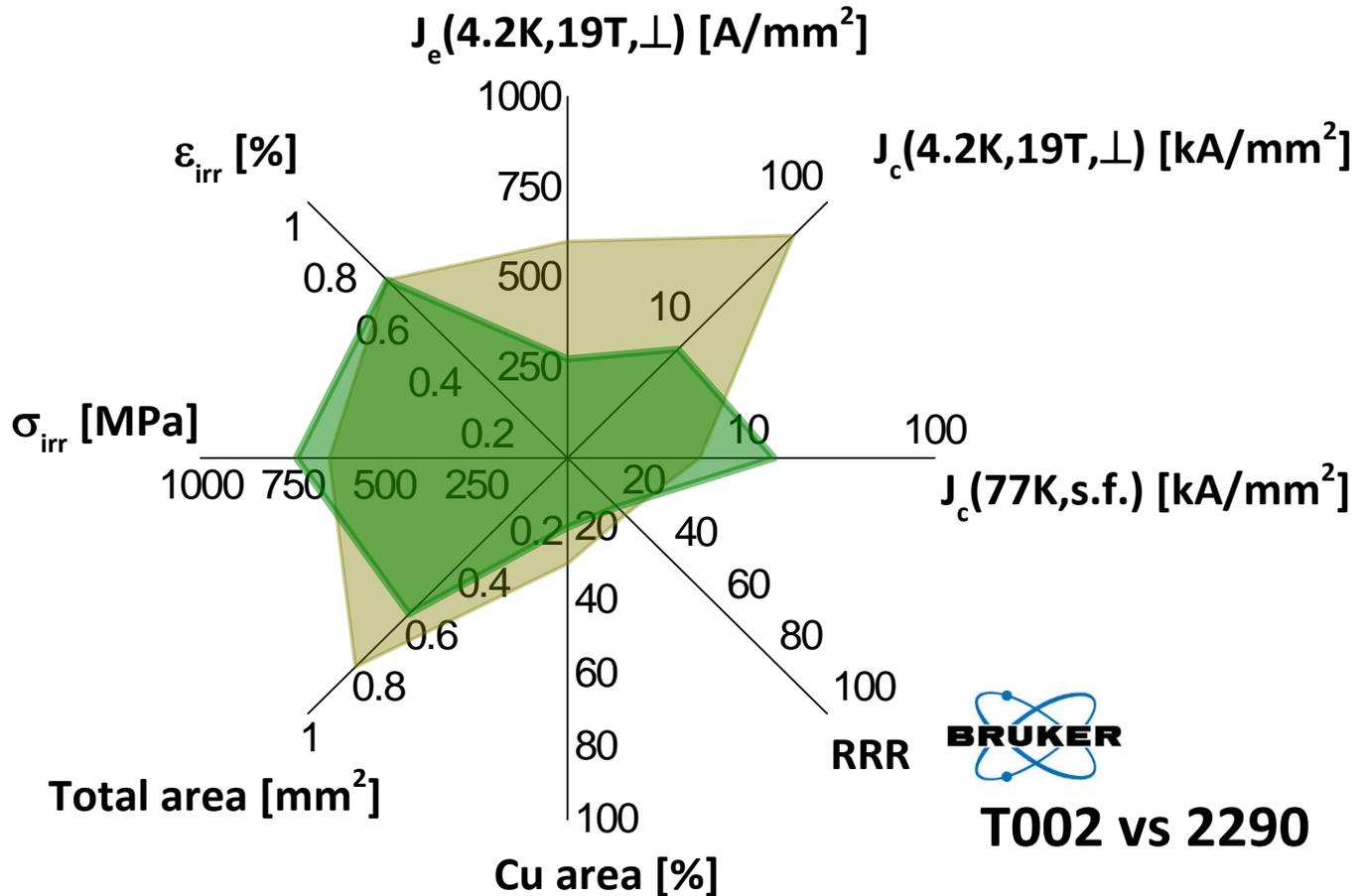
where $T_S = T_{CS} + \frac{T_C - T_{CS}}{2}$

is determined by the $J_c(T)$ dependence

From the experimental κ , ρ , c , $J_c(T)$, NZPV is found to depend only on I_{op} following a power law

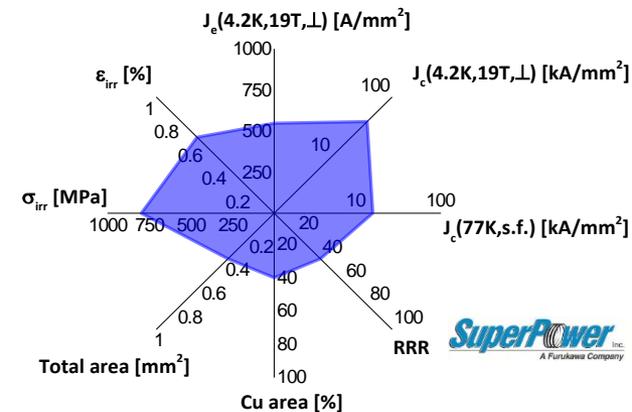
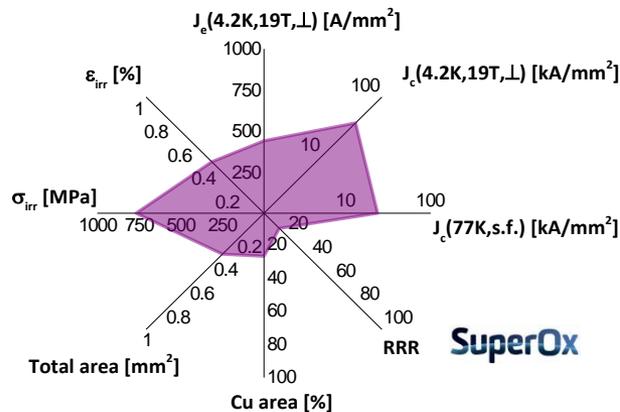
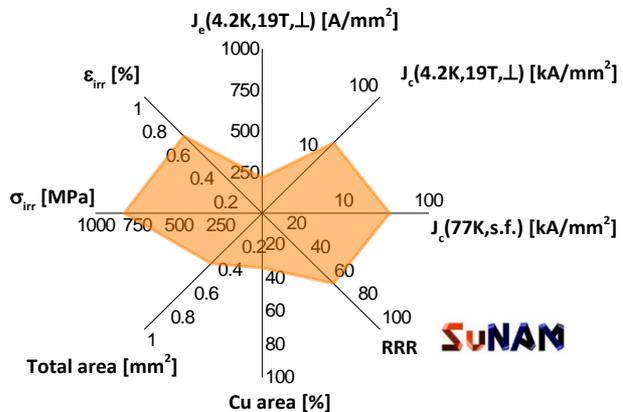
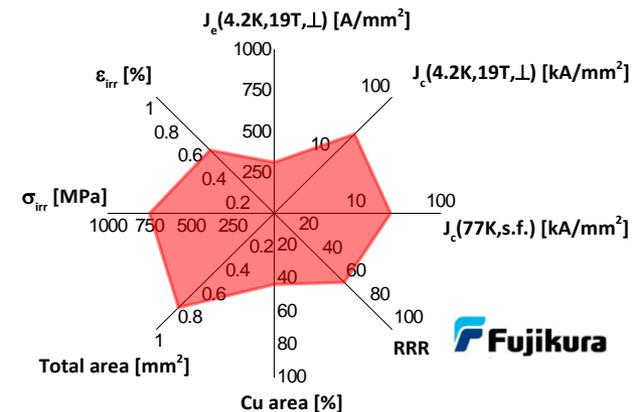
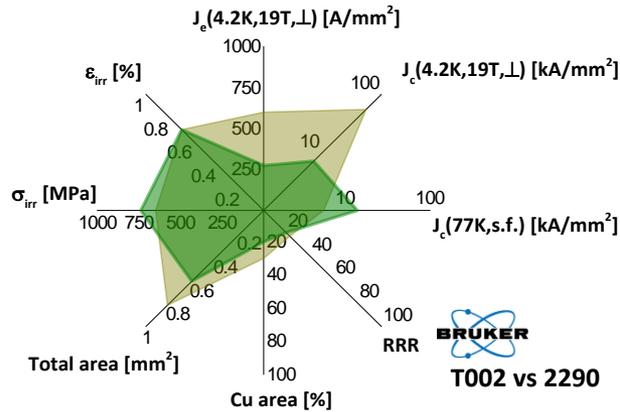
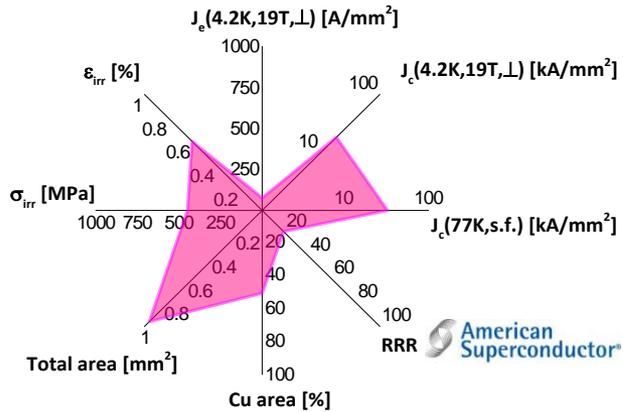


Summary - Main parameters at a glance





Summary - Main parameters at a glance



Conclusions

- Explored the $J_c(B, T, \theta, \sigma)$ surface for CCs from **6 manufacturers**
- **Scaling of $J_c(B, T)$** with an exponential T dependence and a power-law B dependence
- Reconstruction of the critical surface possible with a minimum number of measurements
- Irreversible limit σ_{irr} under **axial** loads in **740 – 840 MPa** range for all manufacturers
- Direct measurements of **in-field thermal conductivity** for quench propagation studies and **calculation of the NZPV**