

The Continuing Utility and Potential of Nb-based Superconducting composite wires

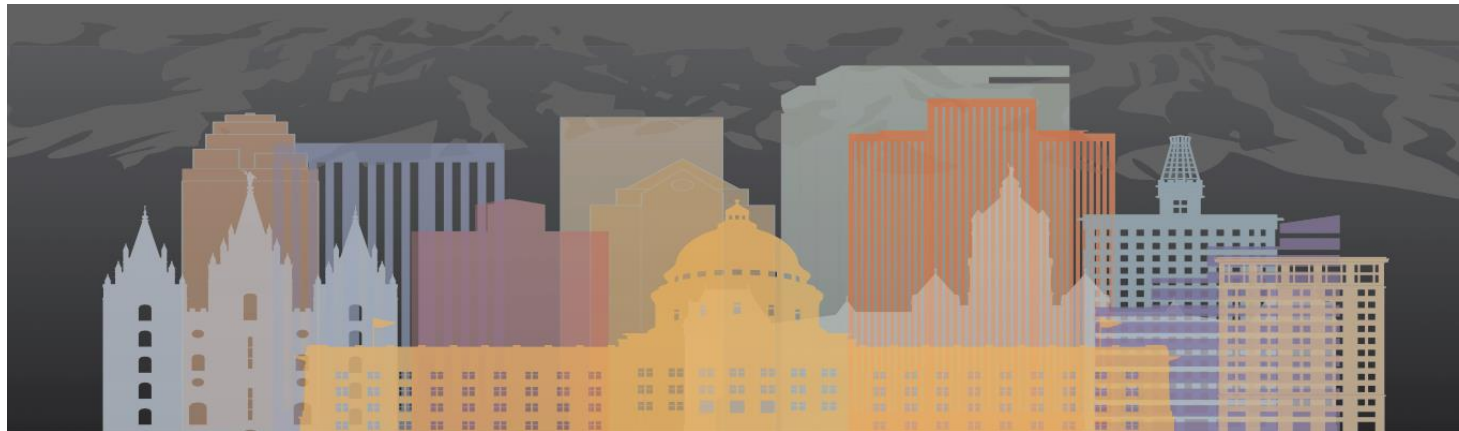
Subtitle: What have Nb-based SC done for you lately?

Mike Sumption,
(The Ohio State University)

..And Slides from (and thanks to!):
A Kikuchi
I Kresgin
C Senatore
C. Tarantini/M.Mandal

And some additional borrowings from “the literature”..

K. Schlenga
B Seeber



Sept 1-6, 2024, Salt Lake City

Are LTSC (Especially Nb-based) still relevant?

- Exciting developments continue for HTS conductors, including ReBCO, Bi:2212, MgB₂, and the pnictides
- However, Nb-based superconductors, including NbTi, Nb₃Sn, Nb₃Al, continue in their utility and potential
- NbTi conductors are important commercially (MRI and NMR), and various particle accelerators rely on them
- LTSCs will continue to be used wherever and whenever they can be, because they are cost effective, mature, and convenient (except for the cooling!)
- Nb₃Sn conductors continue to have potential for the next generation of accelerator magnets as the most cost effective and practical solution for achieving the needed performance
- Even if solely LTSC accelerator magnets are supplemented by HTS inserts, LTSC will be crucial aspects of the machine, keeping them viable both technically and cost-wise
- Recent advances in Nb₃Sn are quite exciting and performance continues to increase for this well known conductor
- New versions of Nb₃Sn as well as Nb₃Al may interesting applications in specialty magnets, insertion devices, and other roles
- LTSC conductor, especially those based on Nb, will continue to be of interest for machine and application development for some time to come.

NbTi

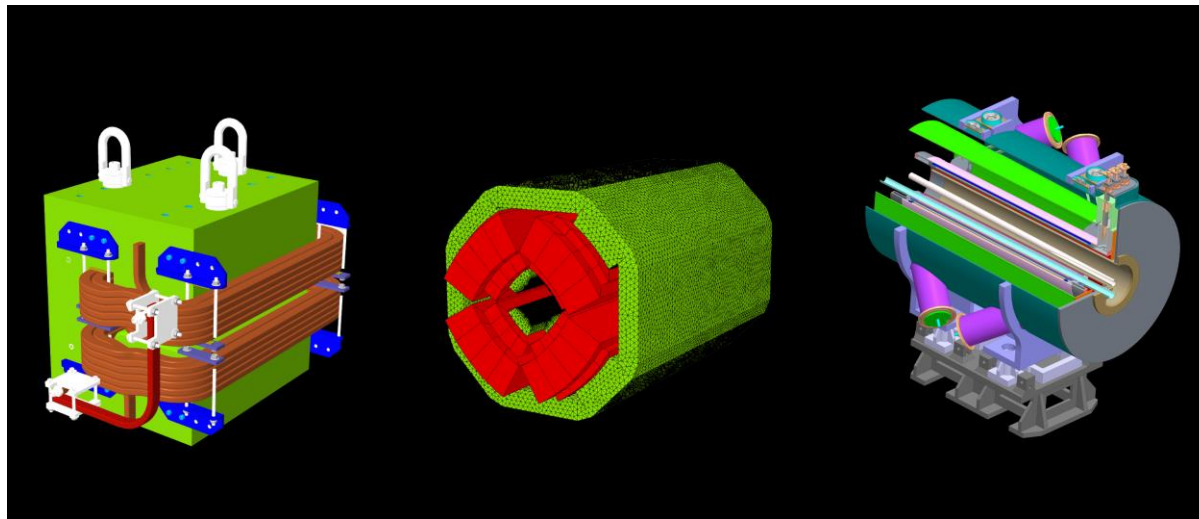
Where do we find it at this conference? In the *Magnet Sessions*

- MRI, sure, to be dominated by NbTi for the foreseeable future
- Electron Ion Collider
- Role in Muon collider?
- Proton therapy gantries
- Maglev (transportation transformation)
- Wind energy
- Quantum computing

Electron Ion Collider

Sure, existing accelerators with SC magnets are NbTi based, but even new ones (EIC) and some magnets of projected ones (Muon collider) rely on NbTi

NbTi based superconducting Magnets



Wind energy

LTSC appears to be commercially competitive from this (and other) analyses

TABLE III
COMPARISON OF THREE KINDS OF HTS TAPES

Items	Bi2223	Bi2212	YBCO
Critical Temp.	110 K	80 K	92 K
Practical working temp.	< 30 K	< 30 K	< 30 K
Cooling medium	Cold He gas, LNe or LH	Cold He gas, LNe or LH	Cold He gas, LNe or LH
Bc2 (4.2 K)	>100 T	>100 T	>100 T
Applied magnetic field	< 2 T @77 K < 20 T @4.2 K	20-50 T @4.2K	< 3 T @77 K > 25T@4.2K
Anisotropic	Strong	No	Strong
Max rated tensile stress	~ 270 MPa	> 250 MPa	> 550 MPa
Jc (A/mm ²)	~ 500 @(77 K, self field)	> 7000 @(4.2 K, self field)	3x10 ⁵ @(77 K, self field)
Jc (A/mm ²)	~ 150 @(77 K, self field) ~ 180 @(20 K, 5 T.L) > 300 @(20 K, 10 T//)	>1000 @(4.2 K, 0 T) 266 @(4.2 K, 45 T)	> 200 @(77 K, self field) > 400 @(20 K, 5 T.L) > 1000 @(20 K, 10 T//)
Price (2012)	40-50 \$/kAm @20 K, 120-150 \$/kAm@77 K	40-50 \$/kAm @20 K, 120-150 \$/kAm@77K	80-150\$/kAm @20 K, 300-500 \$/kAm@77 K
Dimensions	4.5mm*0.3mm	Custom	3-12mm *0.05-0.2mm
Technology maturity	High	High	High
Commercialization	Mass production	Minor production	Initial production

TABLE IV
COMPARISON OF THREE KINDS OF LTS WIRES

Items	NbTi	Nb ₃ Sn	MgB ₂
Critical Temp.	9.6 K	18 K	39 K
Practical working temperature	< 6 K	< 6 K	20-25 K
Cooling medium	LHe	LHe	LH or Conduction
Bc2 (4.2 K)	~13 T	~25 T	18 T
Applied magnetic field	< 10 T	< 23.5 T	< 18 T
Anisotropic	No	No	No
Max rated tensile stress	> 800 MPa	> 360 MPa	> 100 MPa
Jc (A/mm ²)	~ 3000 @ (4.2K, 5T)	~ 6000 @ (4.2K, 10T)	~ 1000 @ (4.2K, 10T)
Jc (A/mm ²)	< 1000 @ (4.2K, 5T)	< 1000 @ (4.2K, 10T)	~ 167 @ (4.2K, 10T)
Price (2012)	1-2 \$/kAm @4.2 K	~15 \$/kAm @4.2 K	~ 5 \$/kAm @20 K
Dimensions	Custom	Custom	Custom
Technology maturity	High	High	low
Commercialization	Mass production	Mass production	Initial production

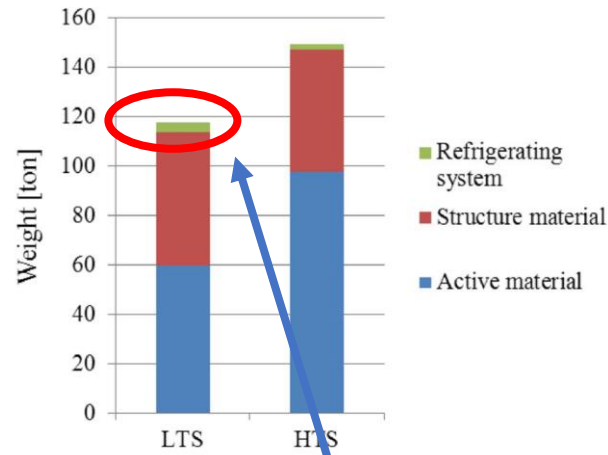


Fig. 9. Weight comparison of the designed LTS and HTS wind generators.

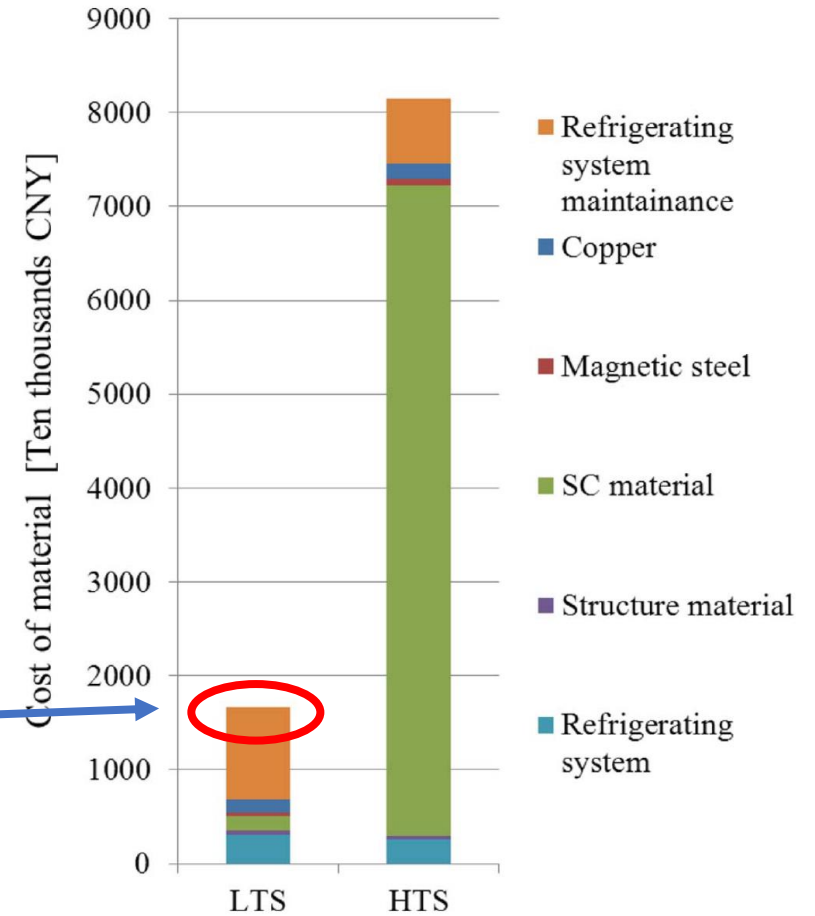


Fig. 11. Cost comparison of the designed LTS and HTS wind generators. (In a sequence from top to bottom, the six items of the legend indicate the subsections of the column diagrams successively.)

EEE TRANSACTIONS ON APPLIED SUPERCONDUCTIVITY, VOL. 25, NO. 3, JUNE 2015

5201806

Comparison Study of Superconducting Wind Generators With HTS and LTS Field Windings

Jin Wang, Member, IEEE, Ronghai Qu, Senior Member, IEEE, Yingzhen Liu, Jie He, Zhe Zhu, and Haiyang Fang

Quantum computing interconnects



Fig. 1. Eight-trace Maybell cable prototype manufactured using linearly actuated mechanical stage with laser welding. Two sheets of 1 mil thick NbTi foil are welded around PFA-coated NbTi wires with a continuous laser weld.

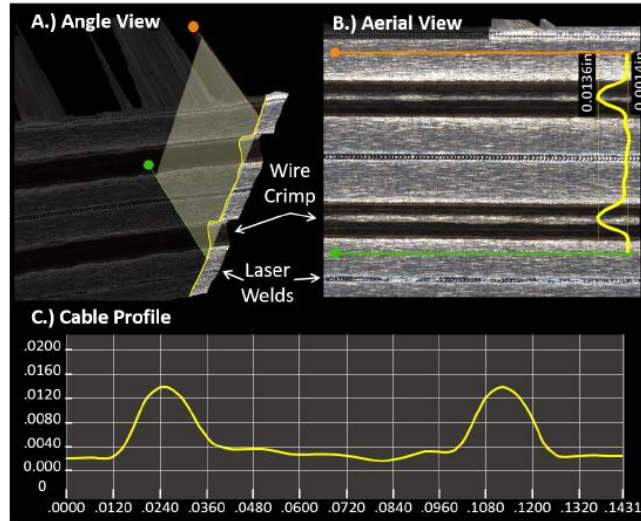
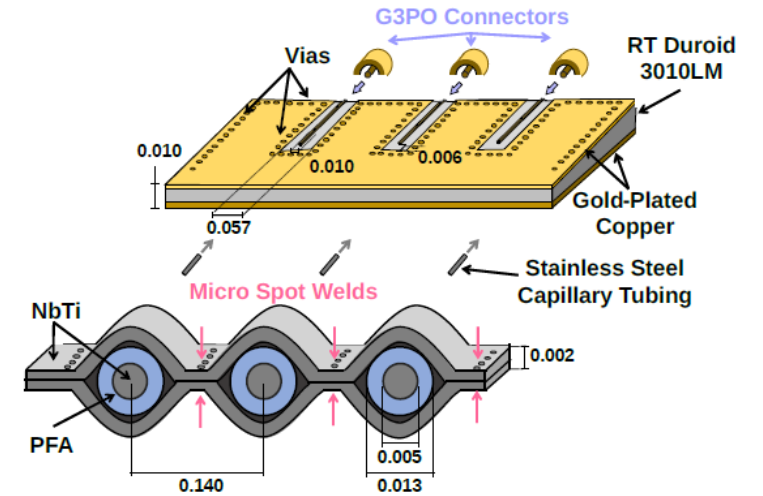


Fig. 2. Manufacturing data obtained from JT Automation during a prototype cable manufacturing run. A.) Angle view showing a single sheet of NbTi foil with two crimps made to house wires with continuous laser welds in-between. B.) Aerial view of the NbTi foil showing the same welds and crimps pictured to the left. C.) Cable profile measured in inches. In all views the cable profile is highlighted in yellow.



Improved Flexible Coaxial Ribbon Cable for High-Density Superconducting Arrays

Jennifer Pearl Smith *, Benjamin A. Mazin *, Alirio Boaventura[†], Kyle J. Thompson[†], Miguel Daal *

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Nb₃Sn

- Either sole magnets or background for HTS magnets for FCC
- Possible Role in Muon Collider magnets
- Proton therapy accelerator magnets (Mevion)
- Fusion ITER, DEMO, (now competing with ReBCO!)
- Undulators
- Energy Storage?

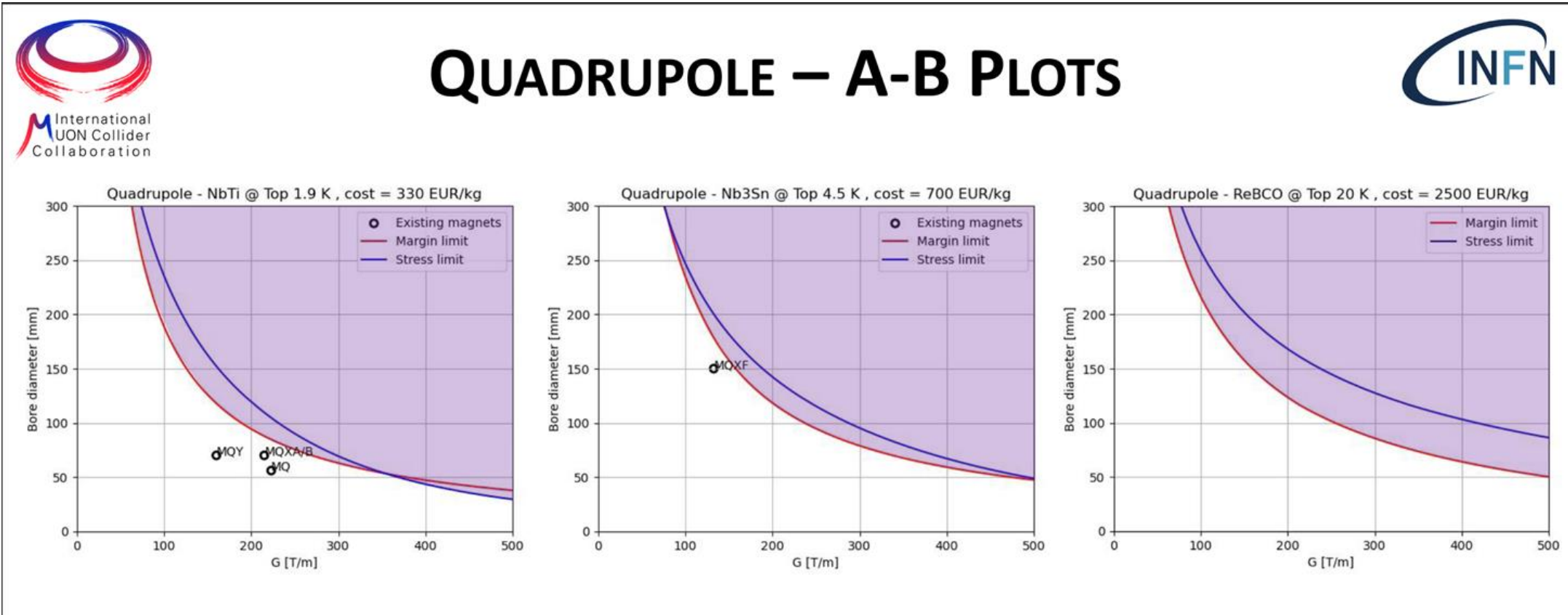
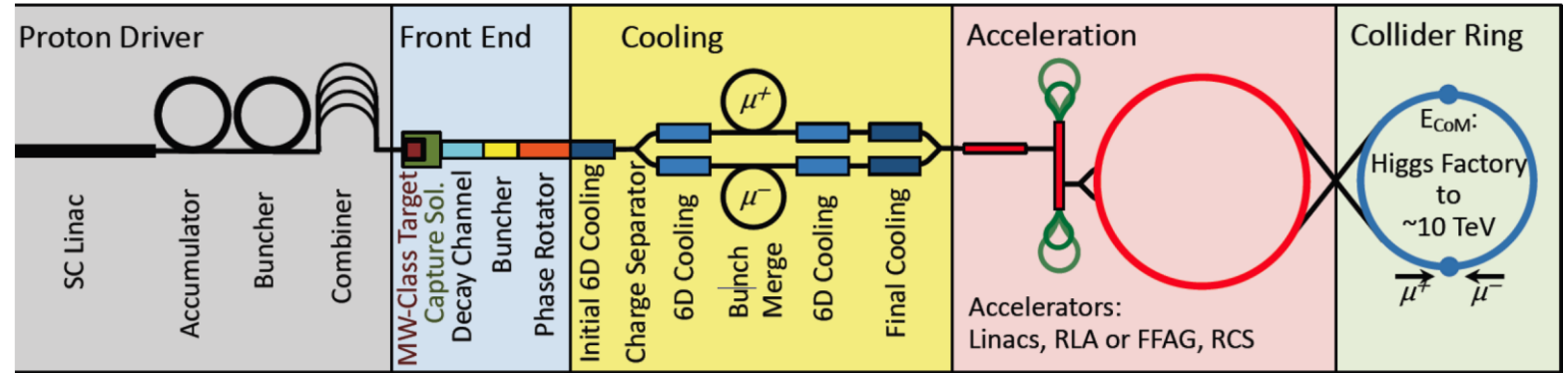
Nb₃Sn and NbTi potential for some muon collider magnets

Performance limits of accelerator dipole and quadrupole for a Muon Collider

D. Novelli^{1,2}, L. Alfonso², A. Bersani², B. Caiffi², S. Farinon², S. Mariotto³, T. Salmi⁴, L. Bottura⁵, ...

¹Sapienza University of Rome, ²INFN - Genoa, ³INFN and University of Milan, ⁴Tampere University, ⁵CERN

15 December 2023 WP7 - Task 4

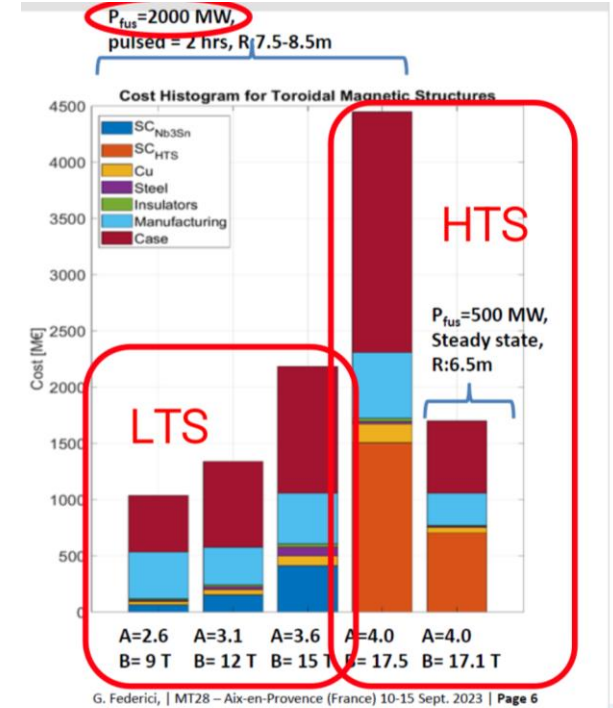
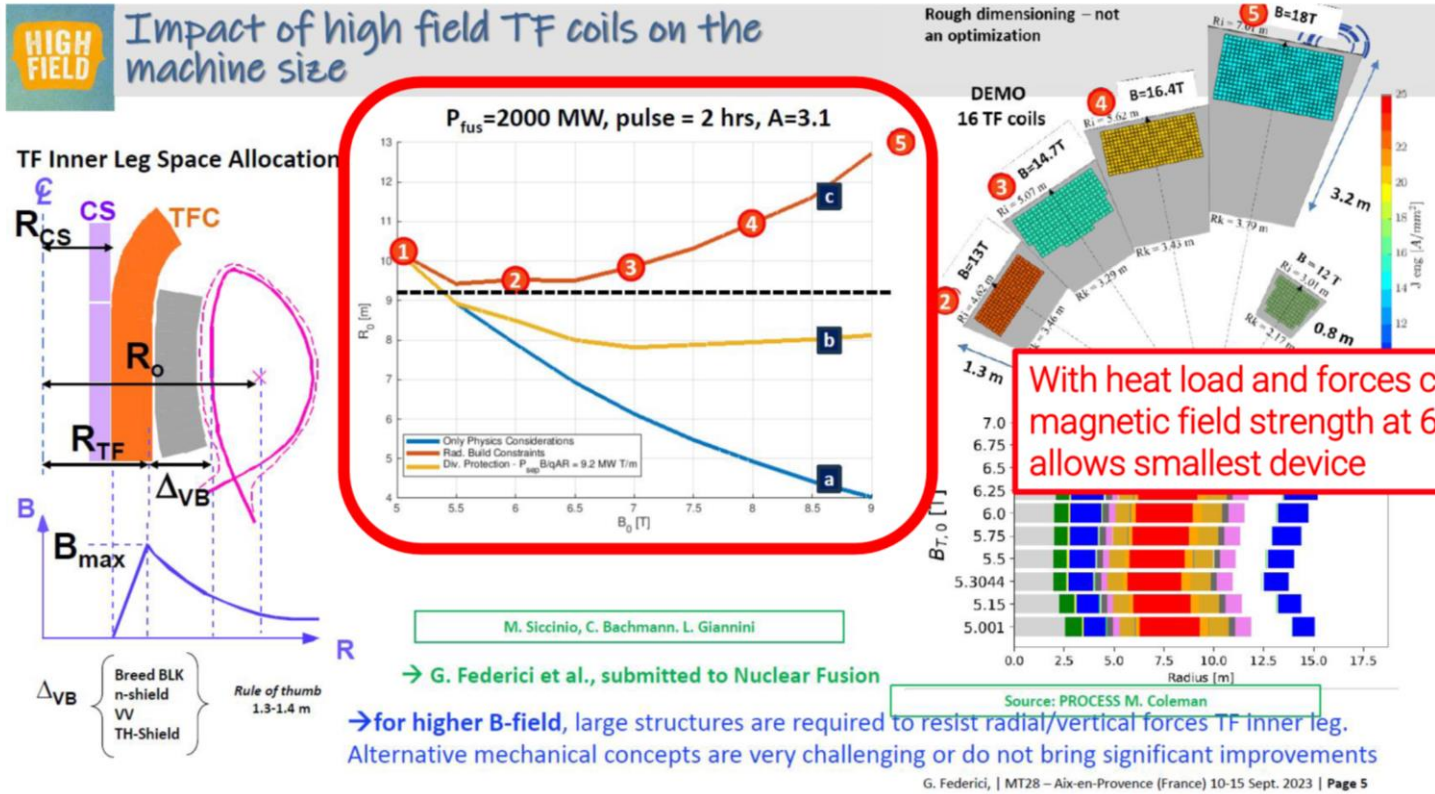


Fusion

Relationship between magnetic field and tokamak size—a system engineering perspective and implications to fusion development

G. Federici^{1,2*}, M. Siccinio^{1,3}, C. Bachmann¹, L. Giannini¹, C. Luongo¹ and M. Lungaroni¹

Higher field is better? --- or is there an optimum?



Not exactly Nb-Based: Chevrels?

Prospects of an alternative superconductor technology for fusion reactors

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B. Seeber^{a1}

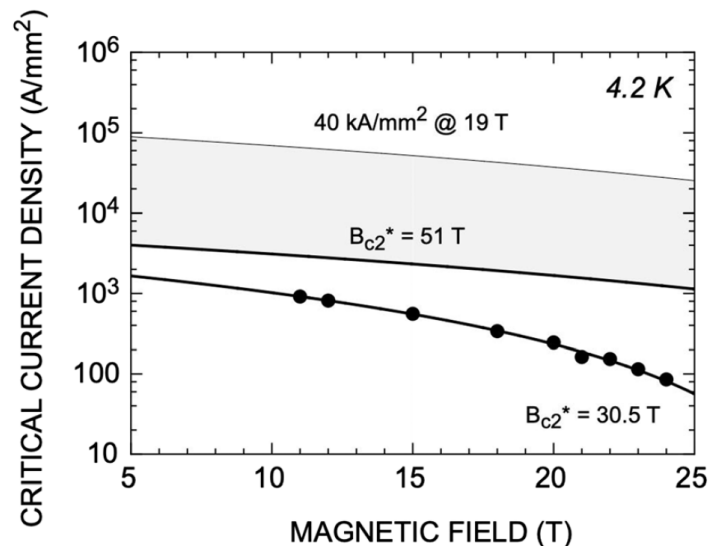


FIG. 6. Critical current density in the superconducting section of a monofilamentary TMC conductor vs magnetic field.⁴⁰ The effective upper critical field, estimated by applying a scaling law for the pinning force⁴¹ and extrapolation to zero, is 30.5 T (4.2 K). Increasing the effective upper critical field to 51 T, which means transparent grain boundary behavior, improves substantially the critical current density. The upper limit corresponds to the benchmark critical current density of 40 kA/mm² at 19 T/4.2 K.

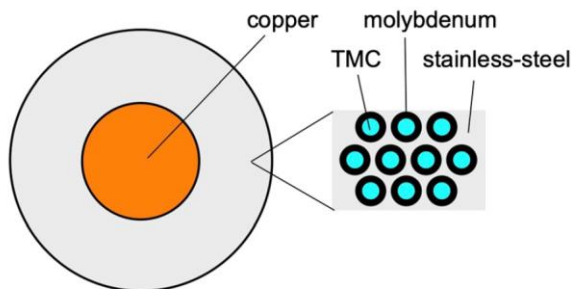


FIG. 2. Schematic layout (not in scale) of a multifilamentary TMC conductor. TMC filaments with a molybdenum diffusion barrier are imbedded in a stainless-steel matrix and stabilization is assured by the copper core.

TABLE III. Constituents of a 0.82 mm TMC wire with 1920 filaments (OD = 10 μm) and a stabilizer/superconductor fraction of 1.

Constituents	Volume (%)	Density (g/cm ³)	Weight (%)
TMC superconductor (PMS)	28.6	6.15	22.5
Mo barrier (stabilizer)	14.3	10.3	18.6
Stainless-steel matrix	42.8	7.8	42.7
Copper (stabilizer)	14.3	8.9	16.2

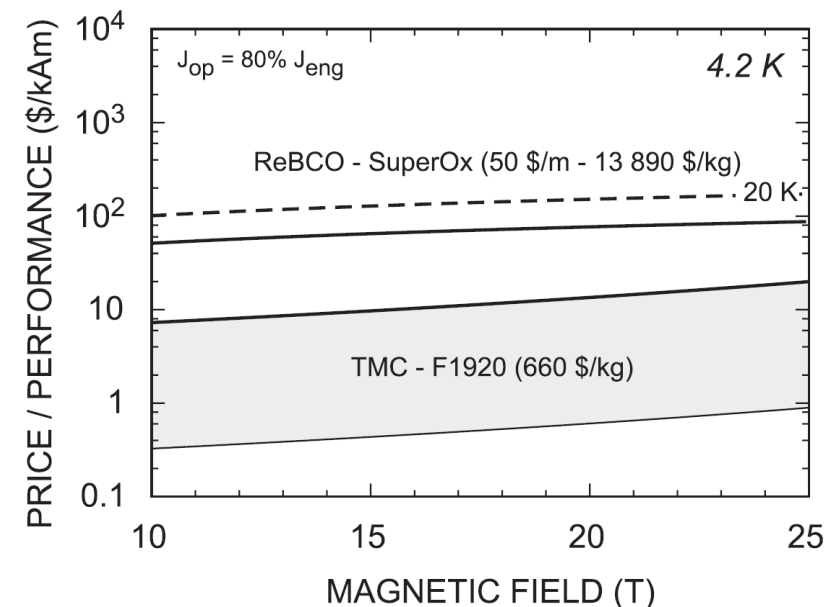
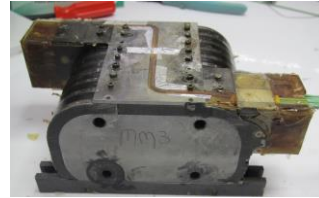


FIG. 4. \$/kAm index at 4.2 K vs magnetic field for a TMC multifilamentary wire F1920 is shown with an operating current density of 80% of the engineering current density and a conductor price of 660 \$/kg (production scaling factor P = 10). The upper line is the expected behavior for transparent grain boundaries and the lower line corresponds to the upper bound estimate for the critical current density (40 kA/mm² at 19 T/4.2 K). For comparison, a 4 mm ReBCO tape, manufactured by SuperOx, with a conductor price of 50 \$/m (13 890 \$/kg) is depicted.

Nb₃Sn undulator for the Advanced Photon source (APS)

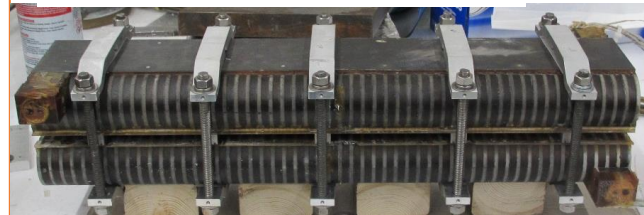
Slides Courtesy Ibrahim Kesgin

- A 3-year project supported by the DOE.
- Collaboration among three US National Labs:
 - ANL (lead institution),
 - FNAL (heat treatment & help with the magnet design),
 - LBNL (protection system).
- Project breakdown:
 - R&D Phase: Build and test short prototypes and scaled to a 0.5-meter lengths.
 - Construct a full-scale magnet (1.1 meters long).
 - Modify an existing cryostat to accommodate the Nb₃Sn undulator magnets.
 - Undulator assembly, testing, magnetic characterizations and installation on the APS.



84 mm

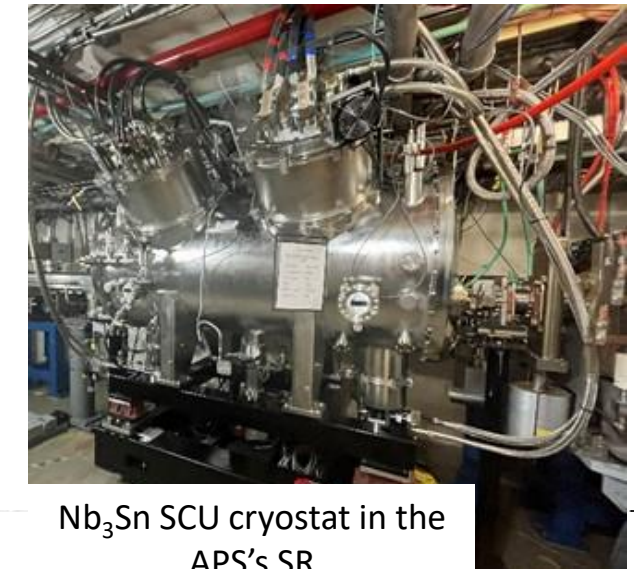
~0.5 m long Nb₃Sn magnets



Cold mass assembly with the 1.1 m long Nb₃Sn magnets



Undulator specifications	Nb ₃ Sn	NbTi
Undulator Field, T	1.17	0.97
K value	2	1.6
Design current, A (~70 and ~80% of the I _c) at 4.2 K	820	450
Period length, mm	18	18
Magnetic gap, mm	9.5	9.5
Magnetic length, m	1.1	1.1
Vacuum gap, mm	7.2	7.2

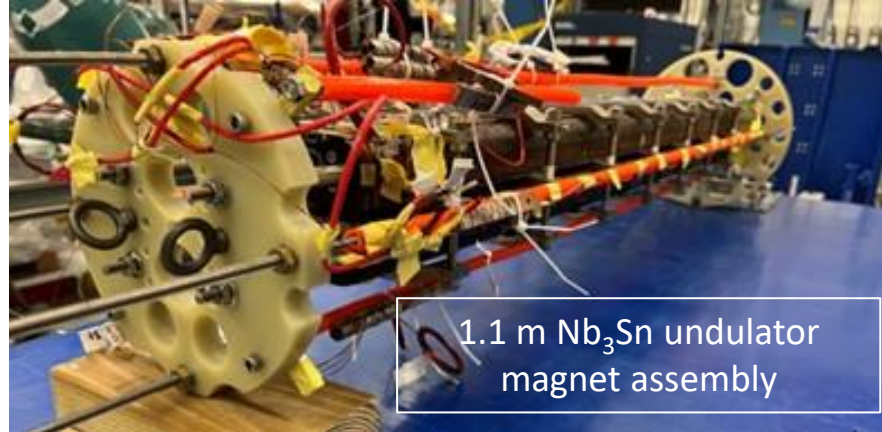


Nb₃Sn SCU cryostat in the APS's SR

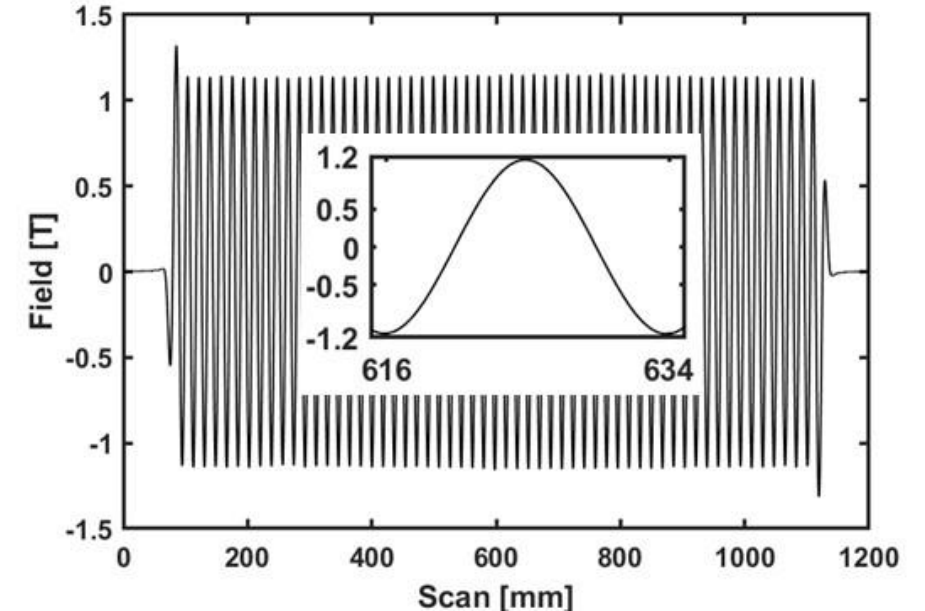
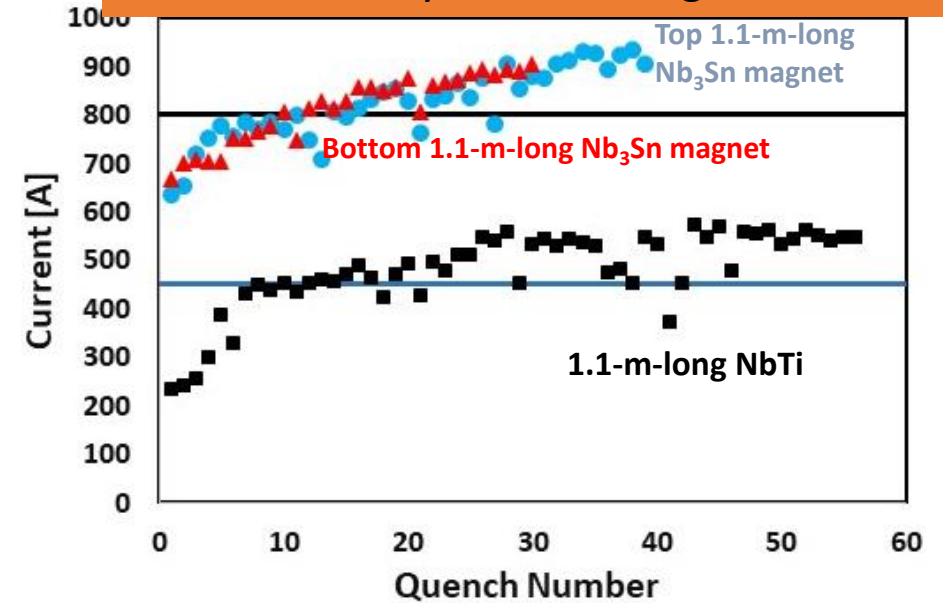
Nb₃Sn SCU replaced NbTi SCU in APS's Sector 1 and successfully delivered x-ray beams as the first Nb₃Sn-based SCU. Operated flawlessly until the start of the APS upgrade on April 17th, '23.

Undulator quench training and field measurements

Slides Courtesy Ibrahim Kesgin



- 1.1m SCU magnets assembled in undulator configuration with diagnostic elements and quench trained
- Undulator achieved design field without requiring additional training during the second cooldown
- **Phase error of <6 degrees achieved up to the maximum operating current**



Work supported by the U.S. Department of Energy, Office of Science, under Contract No. DE-AC02-06CH11357
Through Accelerator & Detector Research Program

Vertical test set-up

Nb₃Sn in FCC or FCC-like accelerator magnets

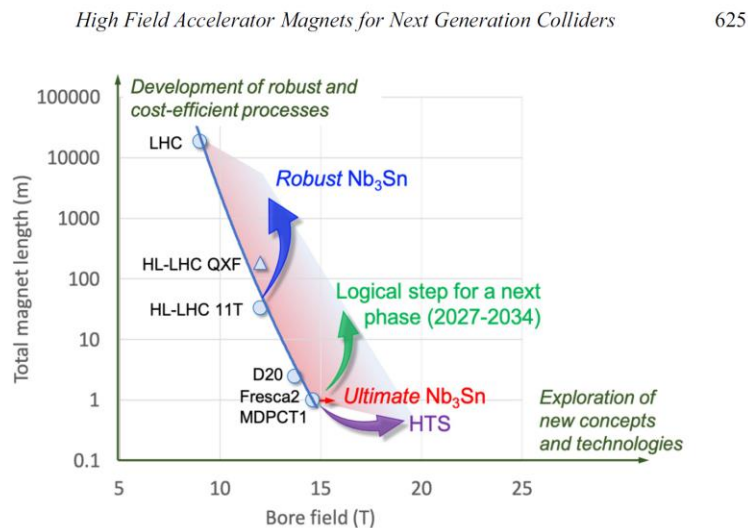


Fig. 3. Graphical representation of the objective of the HFM R&D program in this phase, 2021-2027. Both fronts of maximum field (red for Nb₃Sn, purple for HTS) and large-scale production (blue) are intended to be advanced at the same time. Also represented, in green, a possible evolution for the longer term, 2027-2034.

High Field Accelerator Magnets for Next Generation Colliders – Motivation, Goals, Challenges and R&D Drivers

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https://doi.org/10.1142/9789811278952_0031

FERMILAB-TM-2807-TD

CONCEPTUAL DESIGN OF A 20 T DIPOLE BASED ON HYBRID REBCO/Nb₃Sn COS-THETA COIL*

A. V. Zlobin[†], Fermilab, Batavia, IL 60510, USA

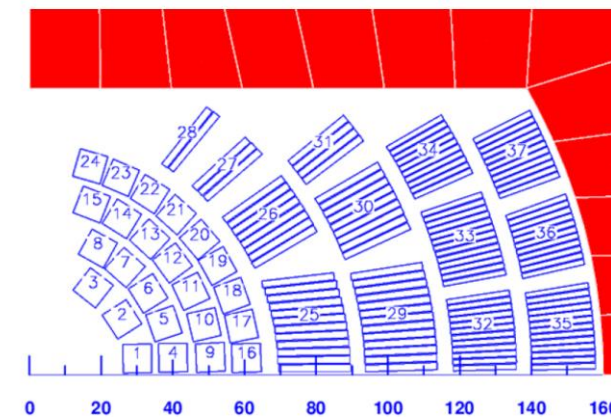
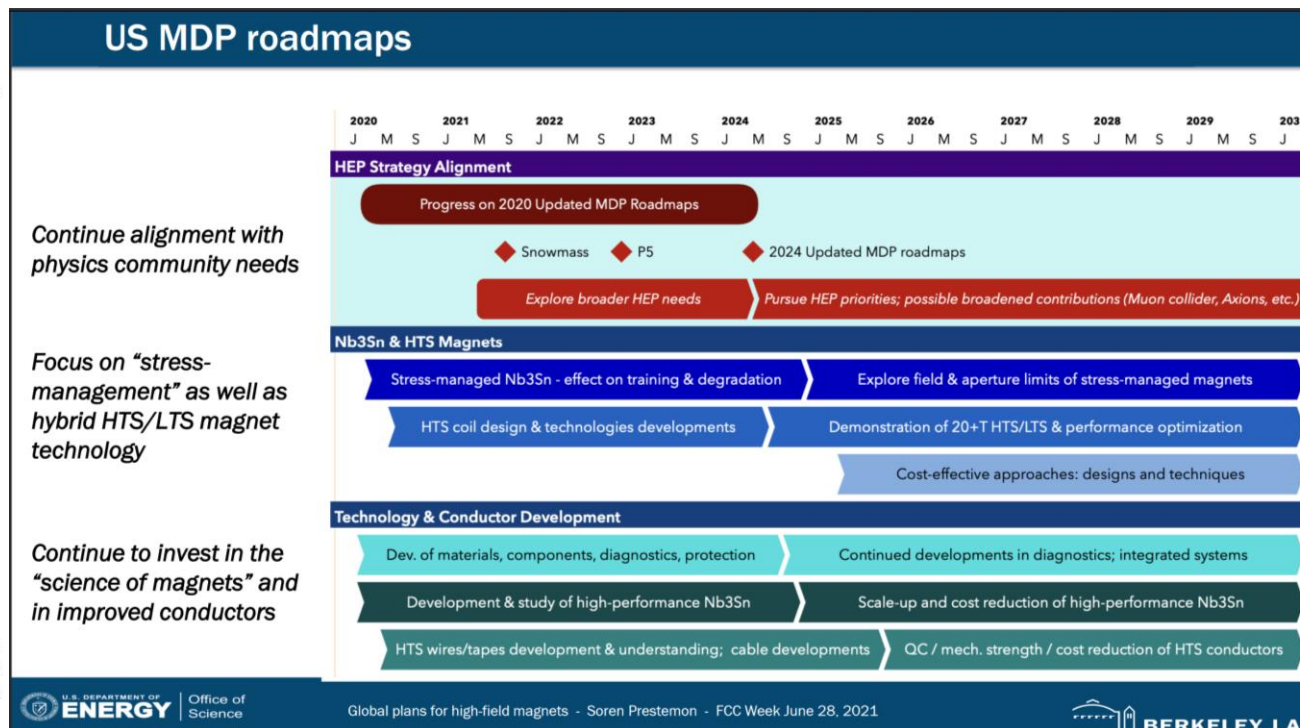


Figure 3: Cross-section of one quadrant of the 20 T hybrid REBCO/Nb₃Sn dipole coil inside the iron yoke.

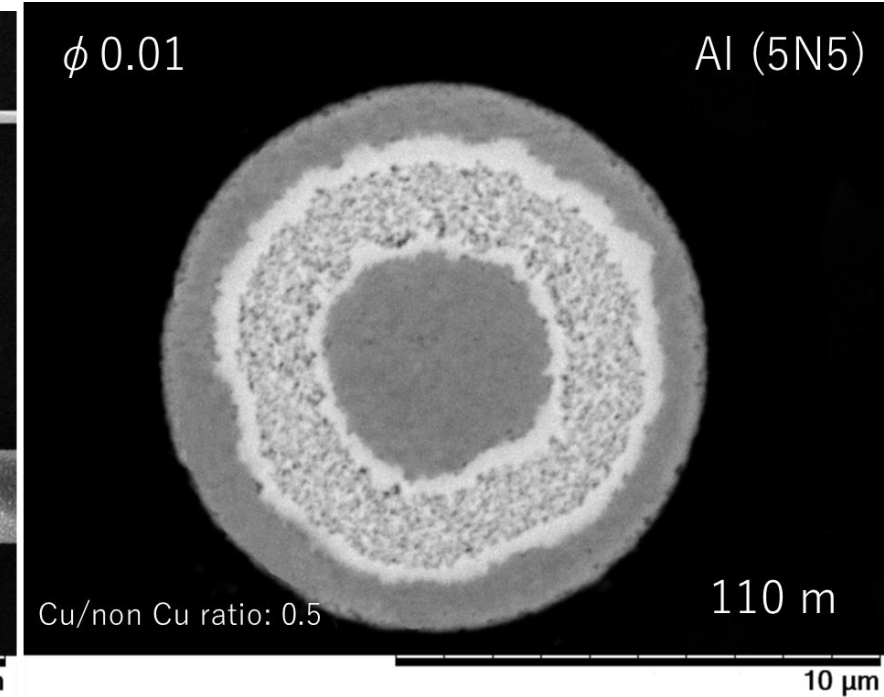
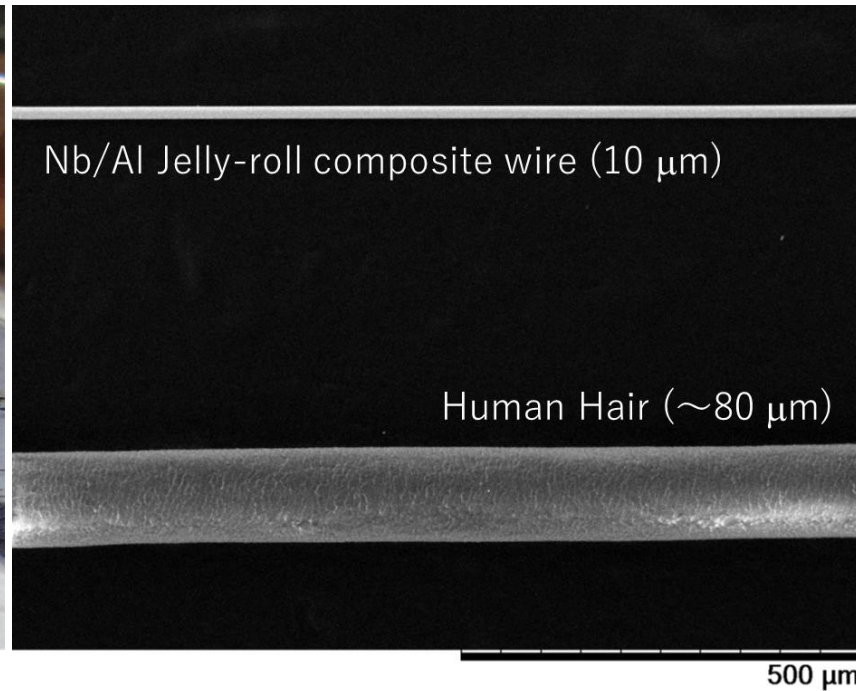
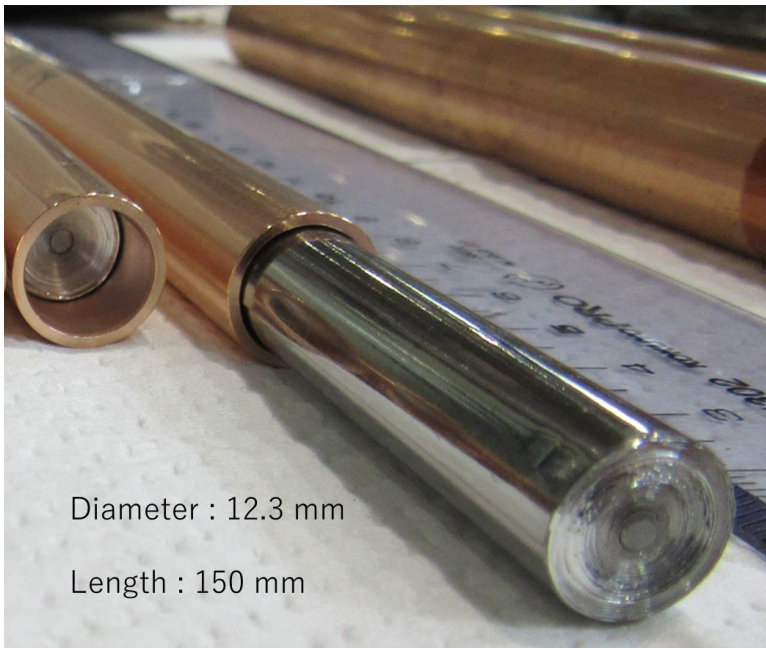
Table 3: Magnet Parameters

Parameter	REBCO/ Nb ₃ Sn	Bi2212/ Nb ₃ Sn
Nominal current I_{nom} , kA	14.90	13.45
Nominal bore field B_o , T	20.0	20.0
Coil nominal field B_{nom} , T	20.34	20.04
Magnet $TF=B_o/I_{nom}$ at I_{nom} , T/kA	1.342	1.487
Magnet margin at 1.9 K, %	10.9	13.2
Total HTS coil area, mm ²	601	972
Total Nb ₃ Sn coil area, mm ²	3854	3110
Total coil area, mm ²	4455	4082

Novel Developments in Nb₃Sn and Nb₃Al

- Very fine wires and cables (NIMS and commercial collaborators) of Nb₃Sn and Nb₃Al (NIMS)
- Progress in APC conductors
- Possible Progress in Nb₃Sn *Bc2*

10 microns Nb_3Al Jelly-Rolled Mono-Core Wire

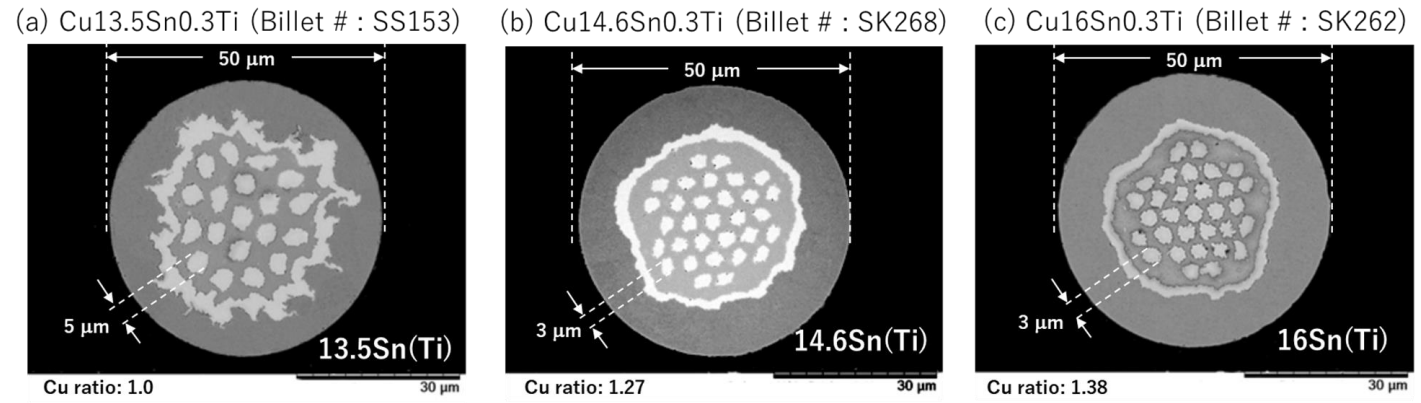


The thinnest Nb_3Al superconducting wire in the world!

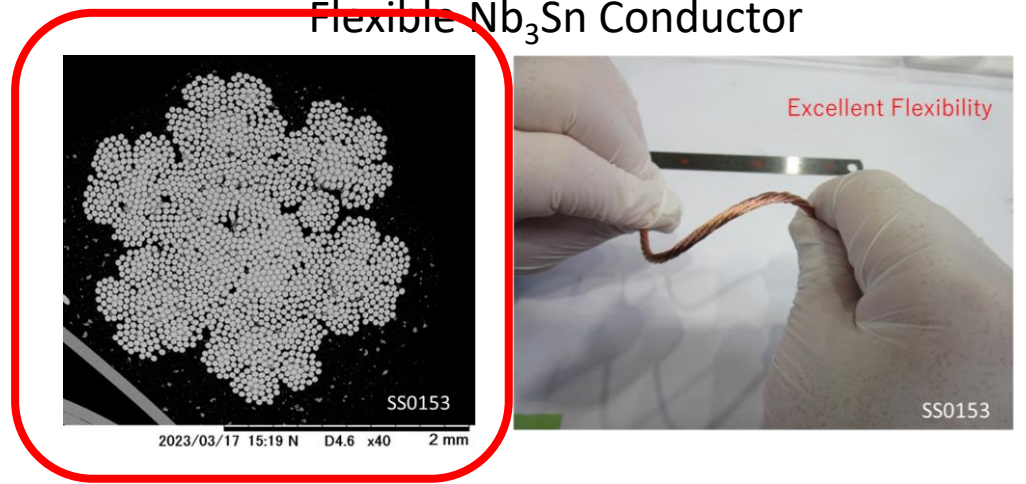
50 microns Bronze-Processed Nb₃Sn Multifilamentary Wires

Development at NIMS (Courtesy of A. Kikuchi)

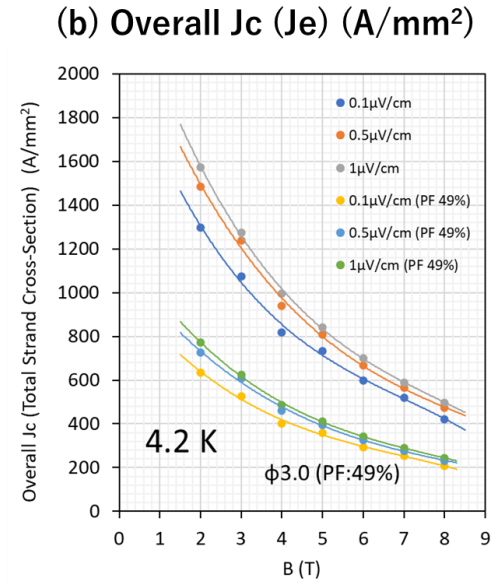
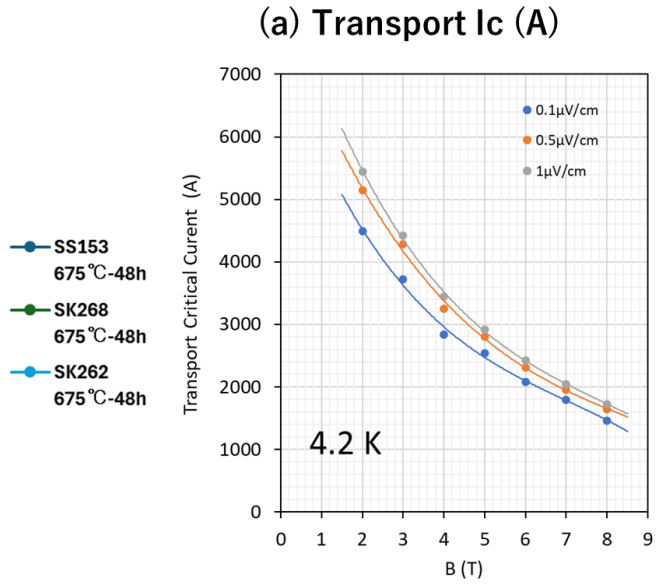
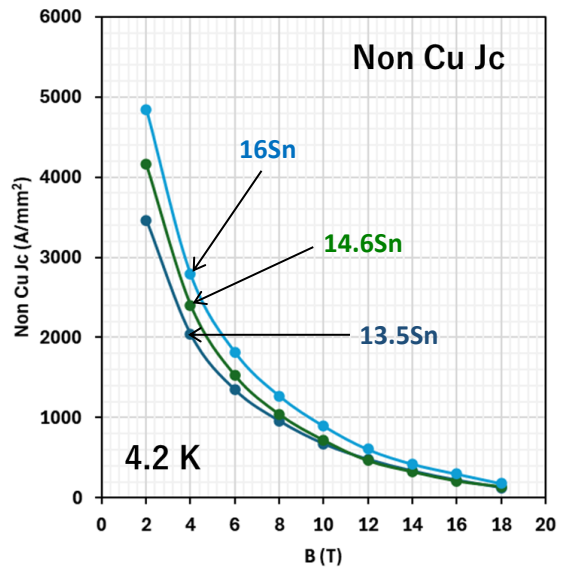
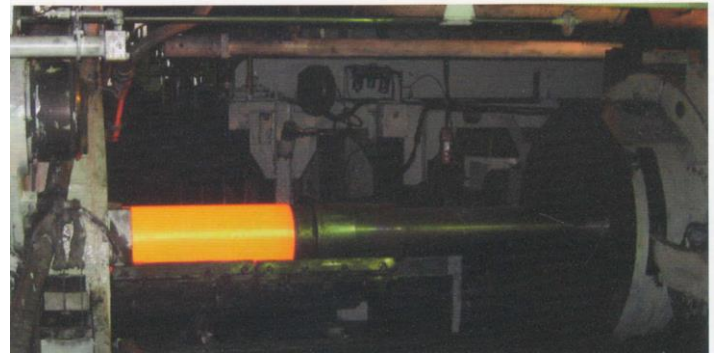
Mass-Production Scale
50 microns Nb₃Sn Ultrafine Wires



Demonstration of Large Current Capacity
Flexible Nb₃Sn Conductor

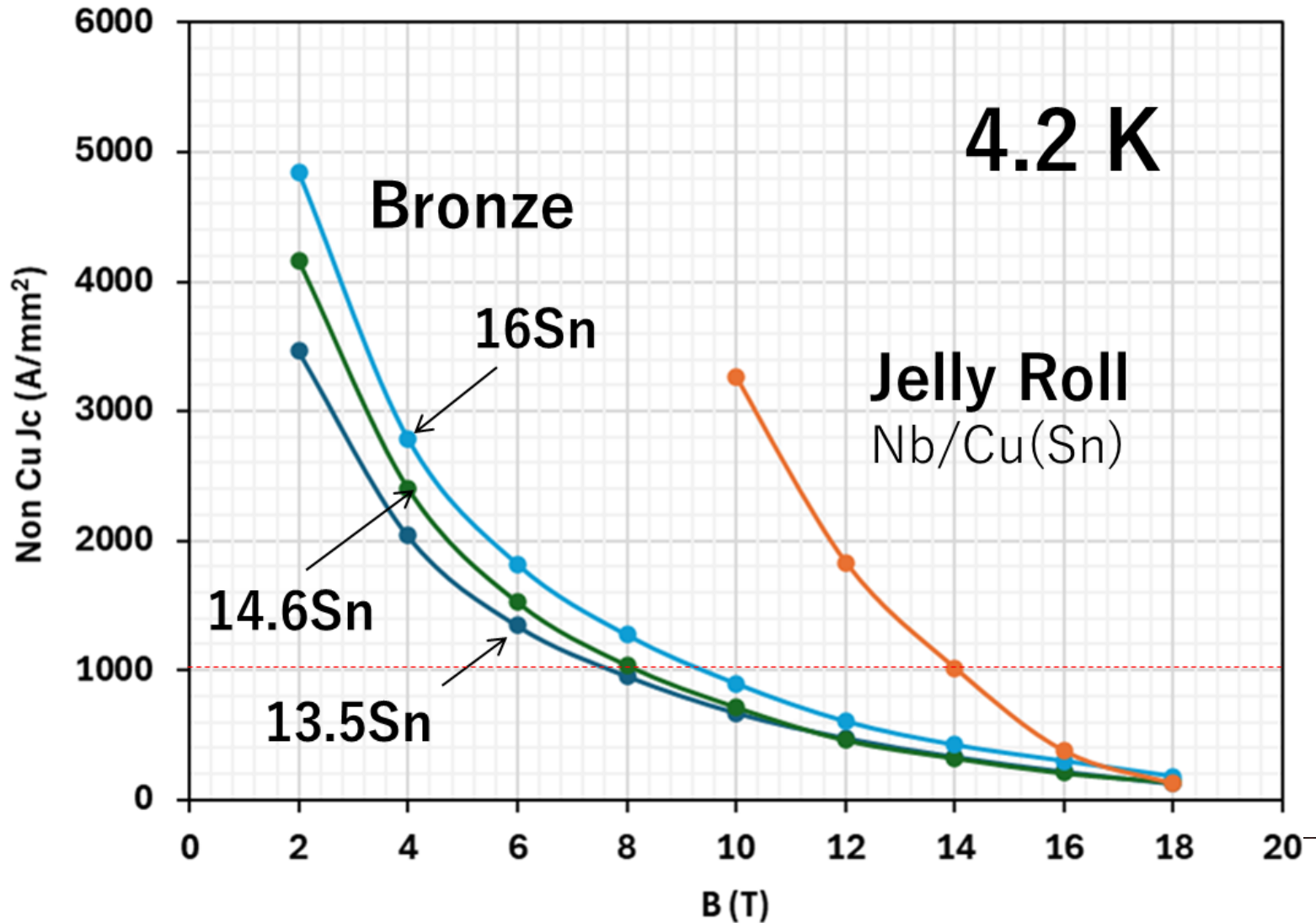
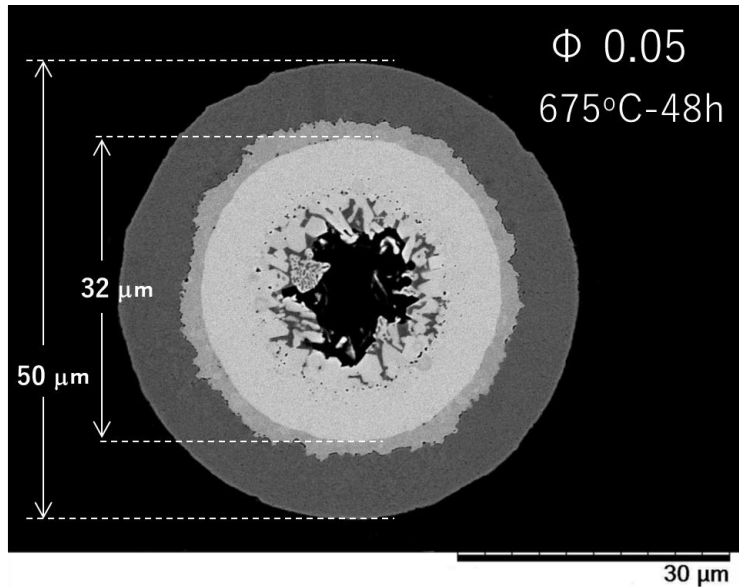
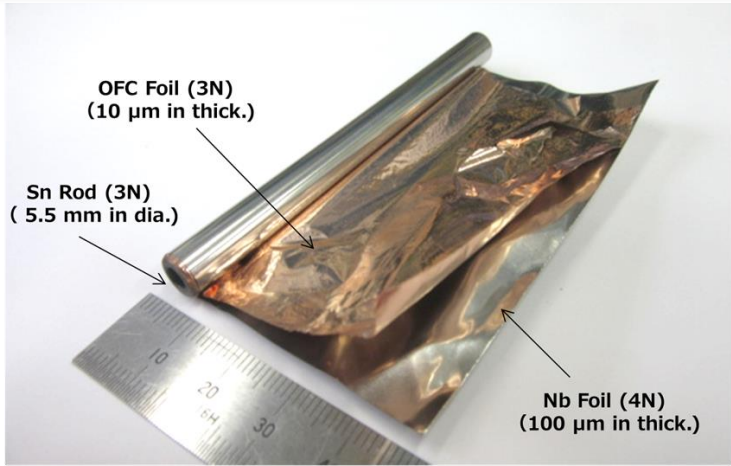


8 inches Billet



50 microns Jelly-Rolled Nb₃Sn Mono-Core Wire

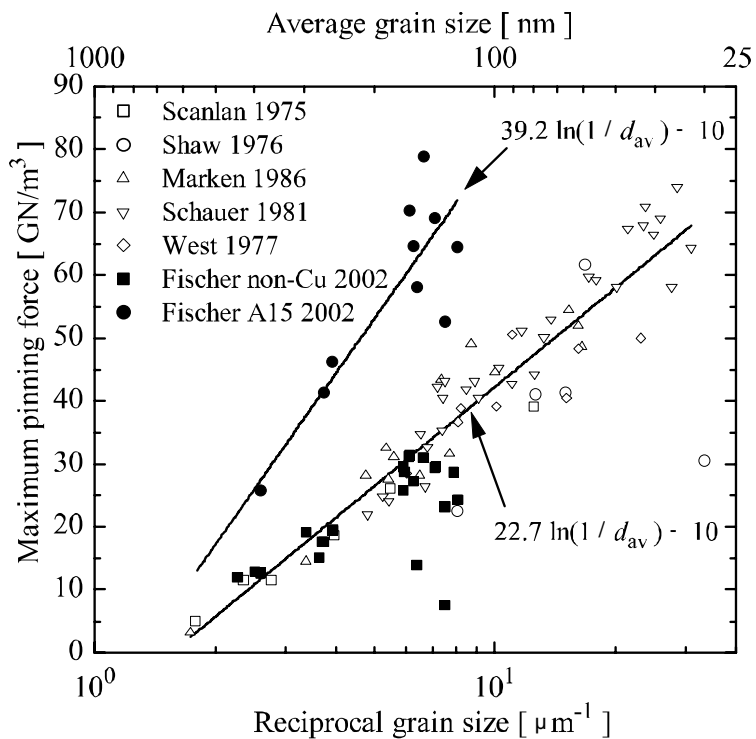
Development at NIMS (Courtesy of A. Kikuchi)



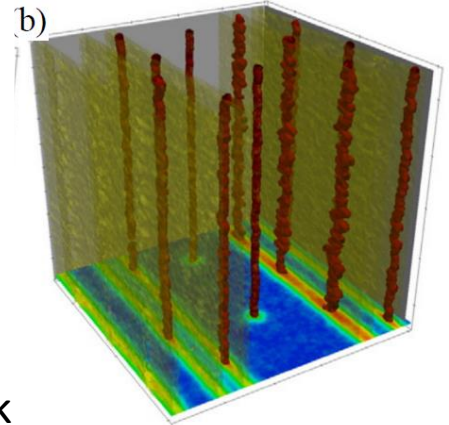
Nb₃Sn Challenges and Opportunities

- New frontiers in performance!
- Increase J_c , J_e
- Increase B_{c2}
- Increase Stability as J_{c2} and B_{c2} go up
- High quality, long length, commercial manufacture
- Development of commercial products for continuity

Well, What are the flux Pinning sites in Nb₃Sn? - Grain Boundaries!- Can we get more of them?

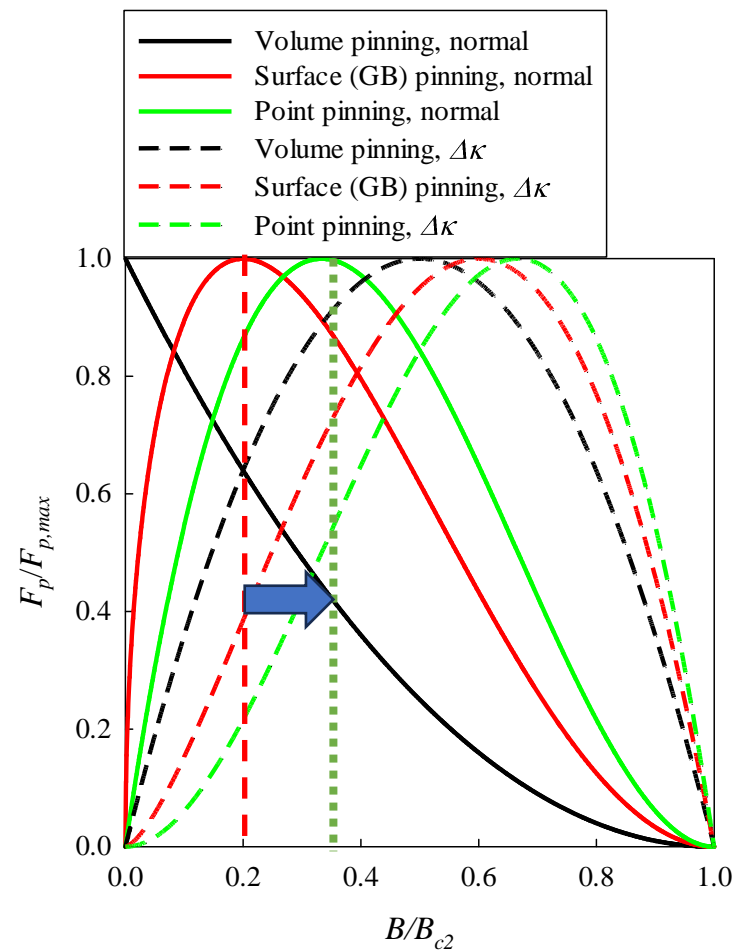
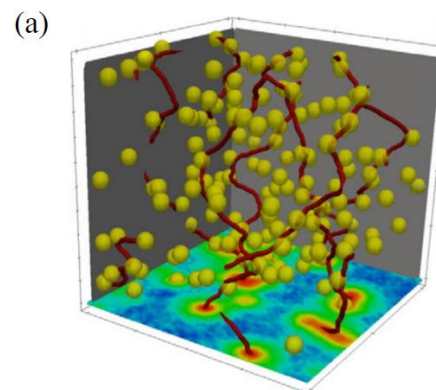


We could add more Surface pins (refine GBs)



Kwok

Or, could we add Point pins?



Dew Hughes

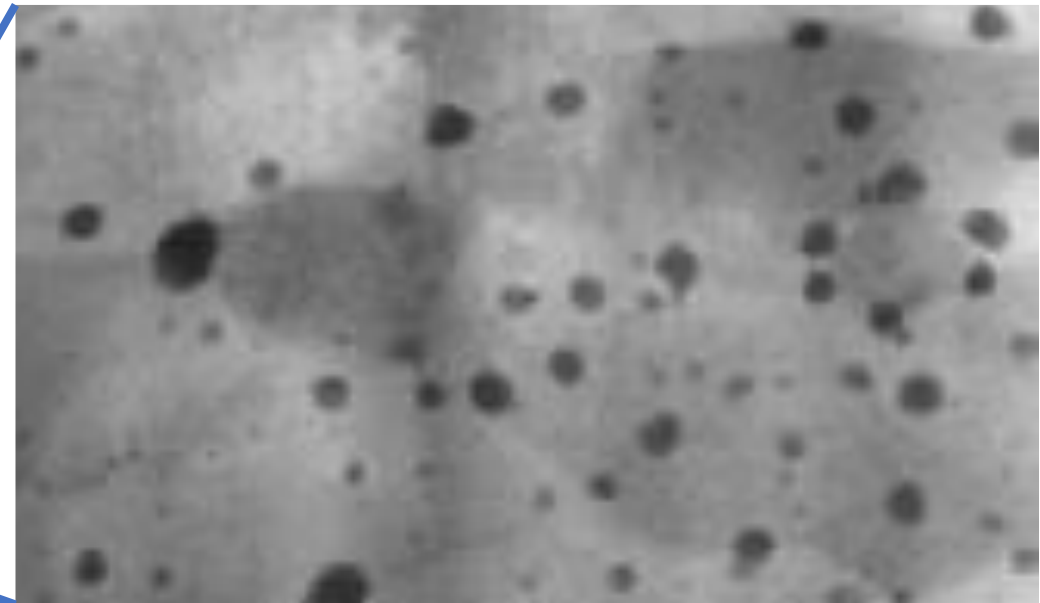
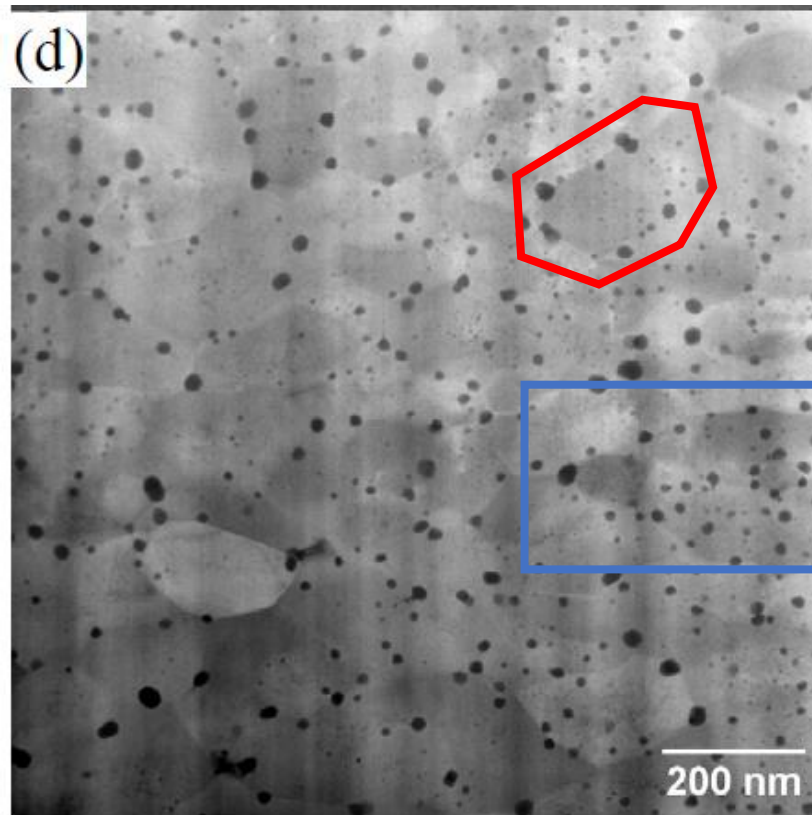
- F_{pmax} (4.2 K) vs inverse grain size for Nb₃Sn.
- Compilation by Fischer.
- Pinning force scales as 1/GB size

But, not only GB refinement (via Zener Pinning) - also Direct Fluxon pinning

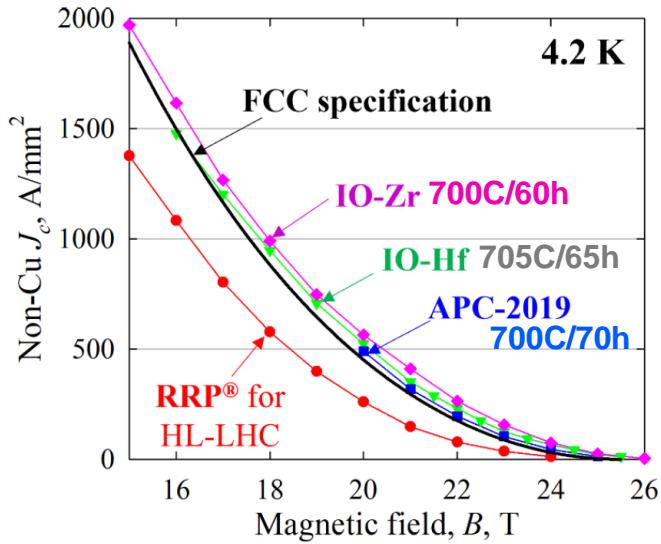
FNAL-HTR-OSU

GBs show precipitates (slows their growth and thus “refines” them)

Pins inside grains -- directly pin flux also

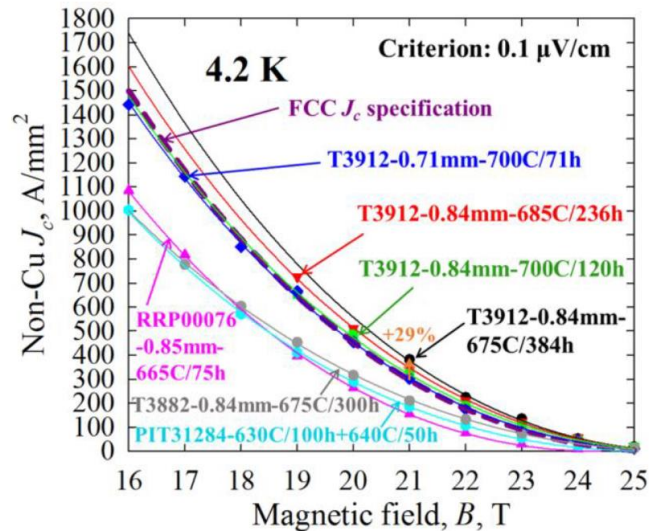


FG/CG ratios of APC Nb₃Sn conductors based on Nb-Ta-Hf/Zr



In previous works:

- Most APC Nb₃Sn conductors which surpassed the level of FCC specification were reacted at ~ 700 °C due to high FG/CG ratio and small grain-size.
- The APC Nb₃Sn conductor reacted at 675 °C attained the highest non-Cu J_c s due to even smaller grain size, but low stability



X Xu et al 2023 *Supercond. Sci. Technol.* 36 035012

X Xu et al 2019 arXiv:1903.08121

Sample	H.T. (°C x h)	FG/CG
APC-1.0%Hf	675 x 400	1.81
	685 x 248	1.91
	705 x 85	2.37
APC-1.0%Zr	675 x 270	1.63
	685 x 125	2.19
	700 x 62	2.61
PIT-standard	630 x 100 + 640 x 50	3.08

- For achieving high non-Cu J_c s, the APC wire reacted at 675 °C needs to have very aggressive recipe due to low FG/CG ratio, inducing low stability.
- If we increase FG/CG ratio at heating temperature ≤ 675 °C, we can use more conservative recipe for APC wire.
- It is expected that APC wires reacted at low heating temperature simultaneously achieve high non-Cu J_c and stability

(2-4) Solubility drop → concentration spike at interface

2. **Solubility Difference:** Scarce literature on Nb₃Sn solubility suggests:

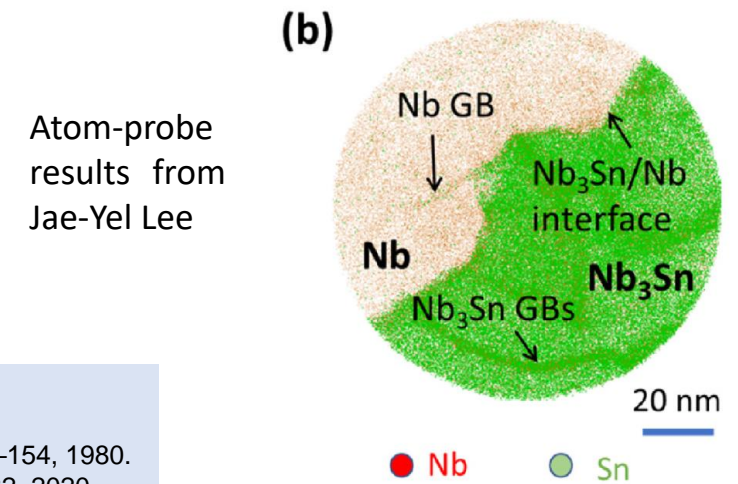
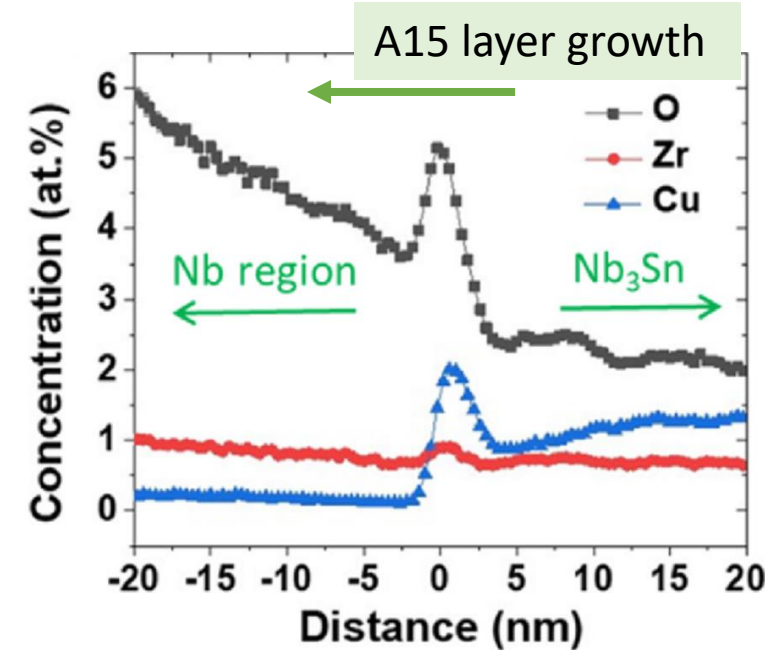
- Zr solubility in Nb₃Sn ~ 1-4.3% [1, 2]
- O solubility in Nb₃Sn ~ 0.4-0.5% [2, 3]

3. **Pile up at moving interface:**

Atom-probe tomography [4] shows that as Nb₃Sn forms, Zr & O pushed ahead of Nb₃Sn/Nb interface

4. **Excess Zr+O drives nucleation:**

Concentration spike drives nucleation at the interface



[1] D. Sharma, D. Kalyan, S. K. Makineni, and S. Santra, *Journal of Alloys and Compounds*, vol. 935, p. 168140, 2023.
[2] I. V. Efimov, B. P. Mikhailov, and E. A. Moroz, *Izvestiia Akademii nauk SSSR. Metall.*, pp. 168–172, 1979.
[3] D. B. Smathers and D. C. Larbalestier, in *Filamentary A15 Superconductors*, M. Suenaga and A. F. Clark, Eds. Boston, MA: Springer US, pp. 143–154, 1980.
[4] Atom-probe results from Jae-Yel Lee, published in X. Xu, M. D. Sumption, J. Lee, J. Rochester, and X. Peng, *J. Alloys Compounds*, Art. no. 156182, 2020.

Starting size of precipitate dictated by thermodynamics

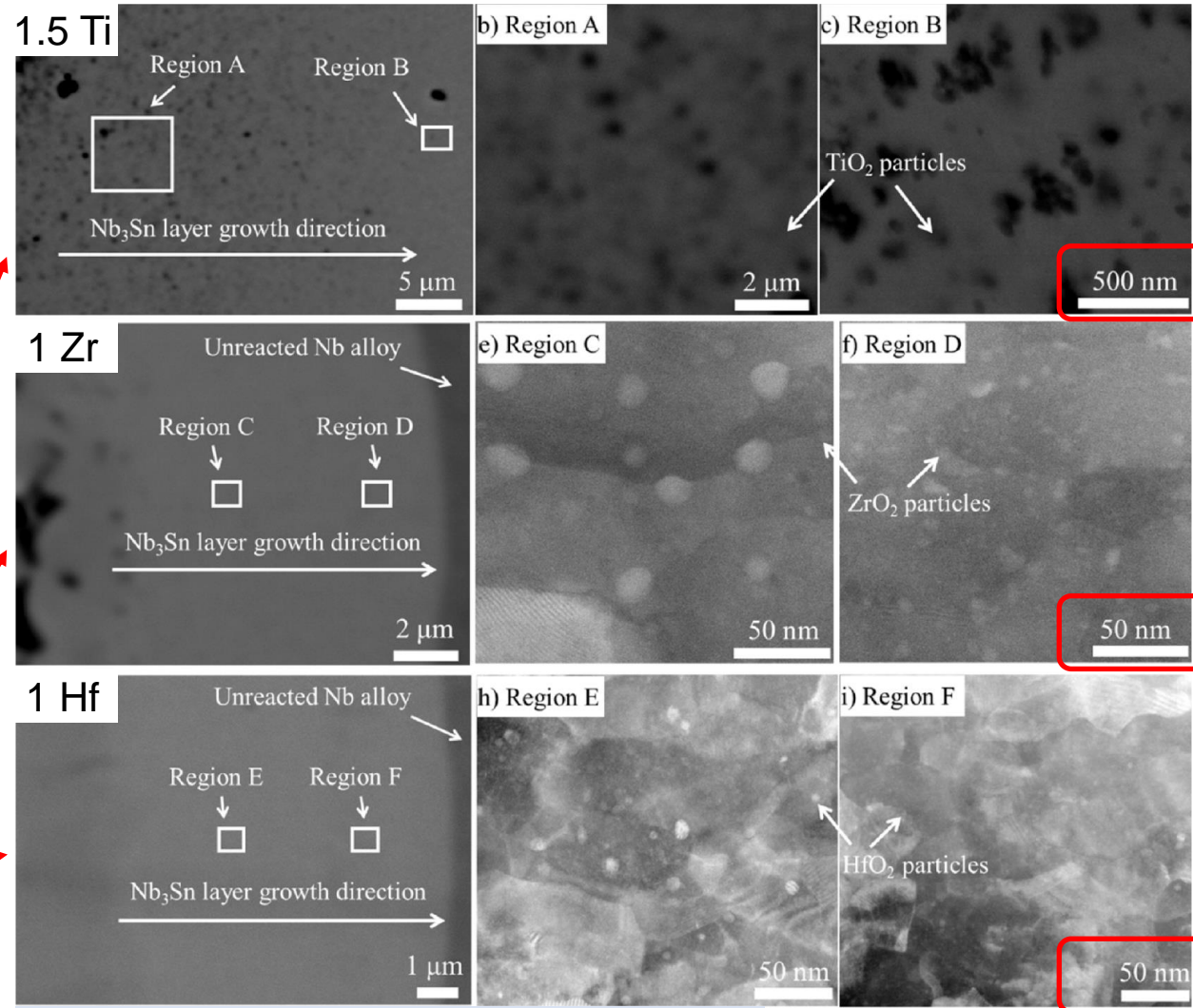
- Applies not just to ZrO_2 but also HfO_2 (and TiO_2)
- Different oxides have different Gibbs energies (and precipitate sizes)
- Larger reduction in Gibbs energy \rightarrow smaller particles can nucleate

$$\Delta G = \frac{4}{3}\pi r^3(\Delta g_v - \Delta g_s) + 4\pi r^2\gamma$$

	Ti	Zr	Hf
d, est, nm		6	1.4
d, meas, nm	50	10	5

Ti – Large
Zr – Medium
Hf – Small

Why large disagreement? – one reason Growth!



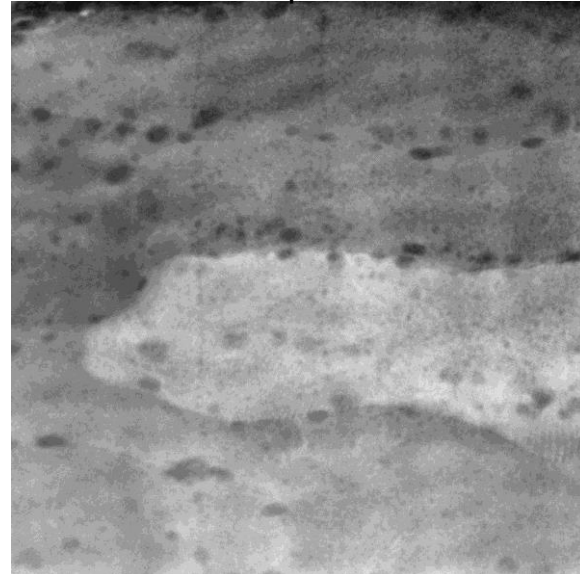
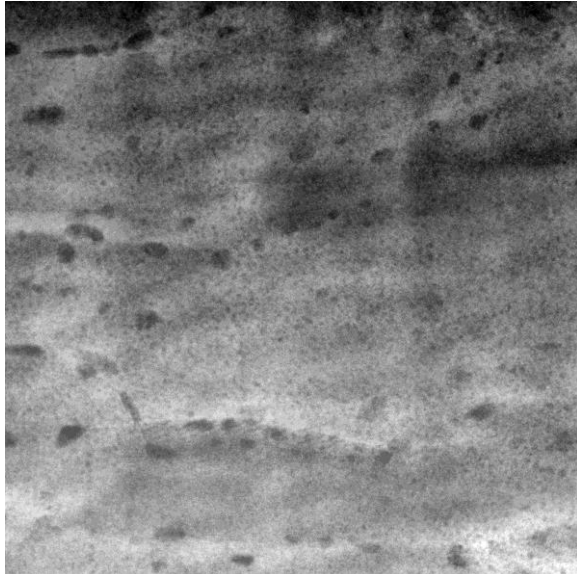
X. Xu et al., *J. Alloys Compounds*, vol. 857, Art. no. 158270, 2021.

(5) Particle Growth Over Time

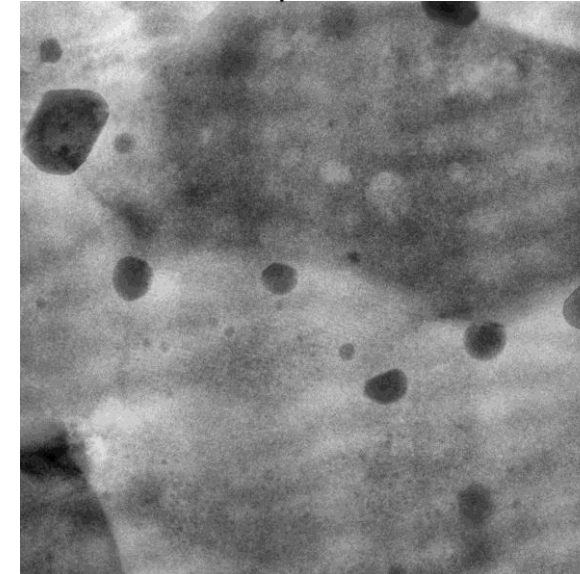
- Fine dispersion of particles near interface (1-2 nm, fewer up to ~10 nm)
- Coarsen into fewer, larger particles (up to ~30 nm) towards core, or for “longer times”
- Wide particle size distribution – cannot approximate as one size

Near Nb/Nb₃Sn interface
(Newly formed)

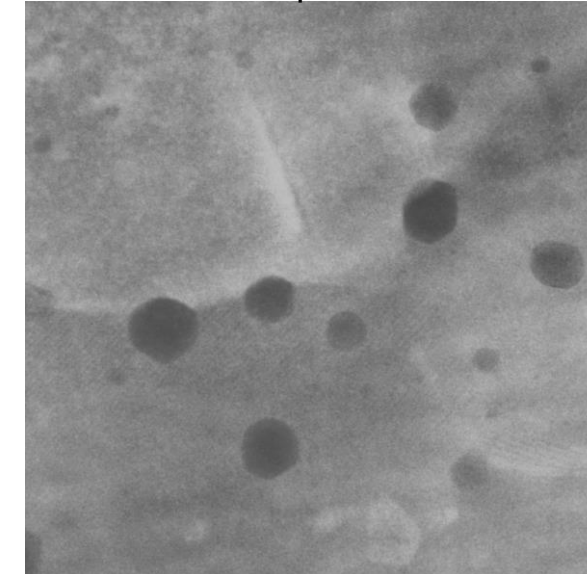
Distance from interface: 0.5 μm



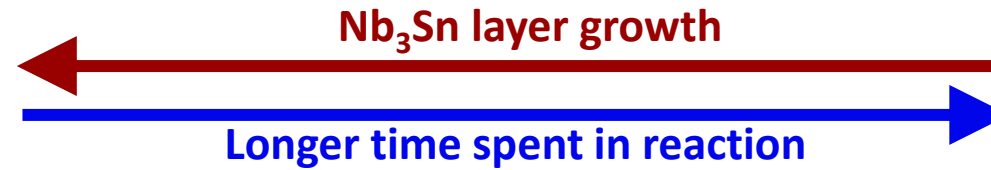
1 μm



4 μm



6 μm



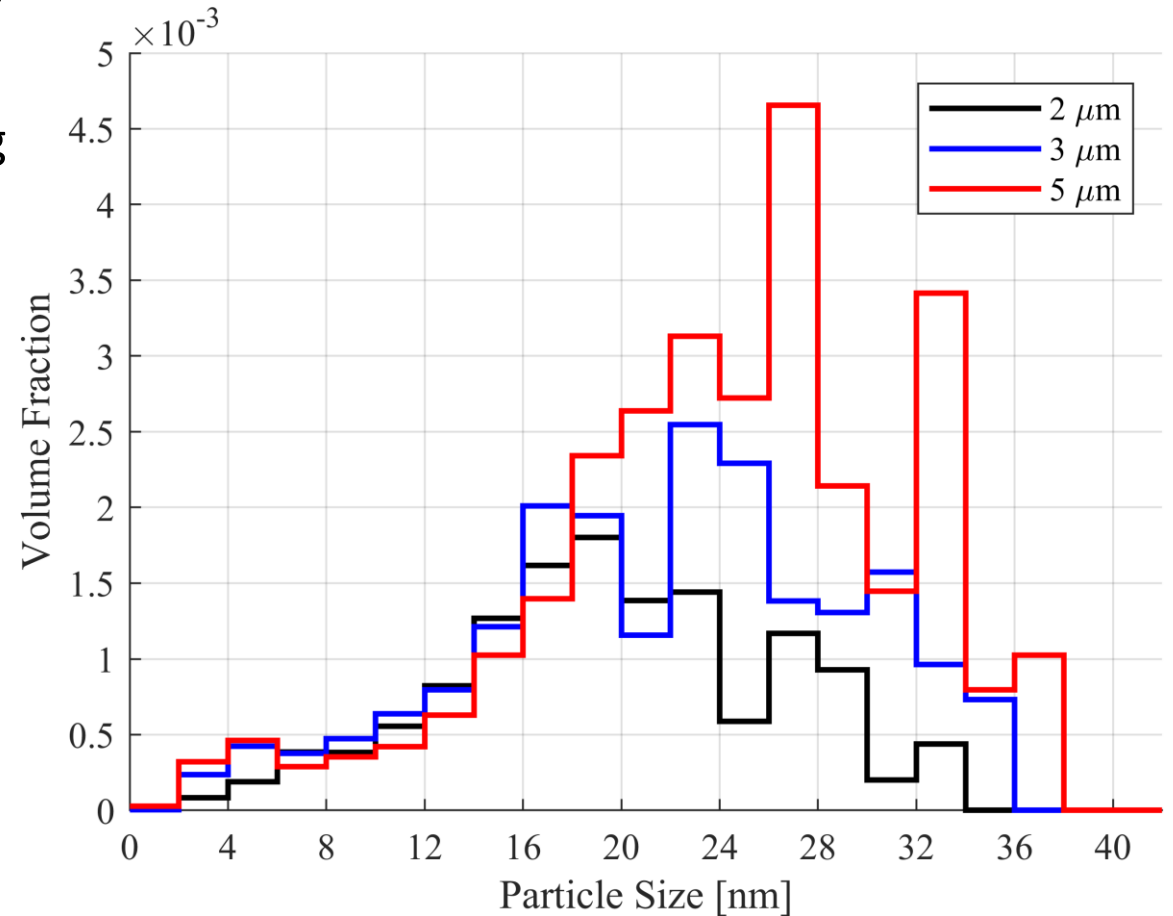
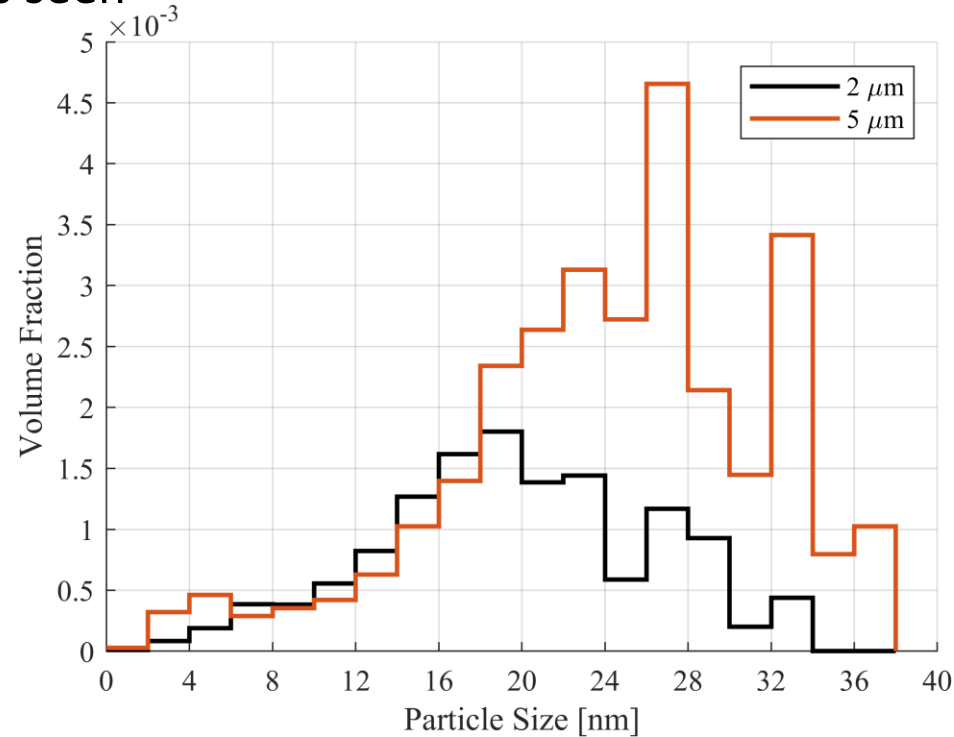
Near core (first formed)

HAADF-STEM images (200 nm x 200 nm) of Zr APC wire, 720°C/32h
processed in ImageJ with Gaussian blur and “Enhance Local Contrast” function

Particle Growth Over Time

- Zr APC, 740 °C/16h
- The volume-fraction histogram shows the change in size distribution from 2 μm from the Nb/Nb₃Sn interface to 5 μm from the interface
- At distances further from interface, particle coarsening is seen

- Distances measured from the reaction interfaces
- Larger distances describe regions that have had longer for particles to coarsen



Number Density of APC at 2 μm from Nb/A15 interface

Notice

- Log-normal distribution
- Bimodal distribution

... perhaps larger precipitates are at GBs -- uncertain

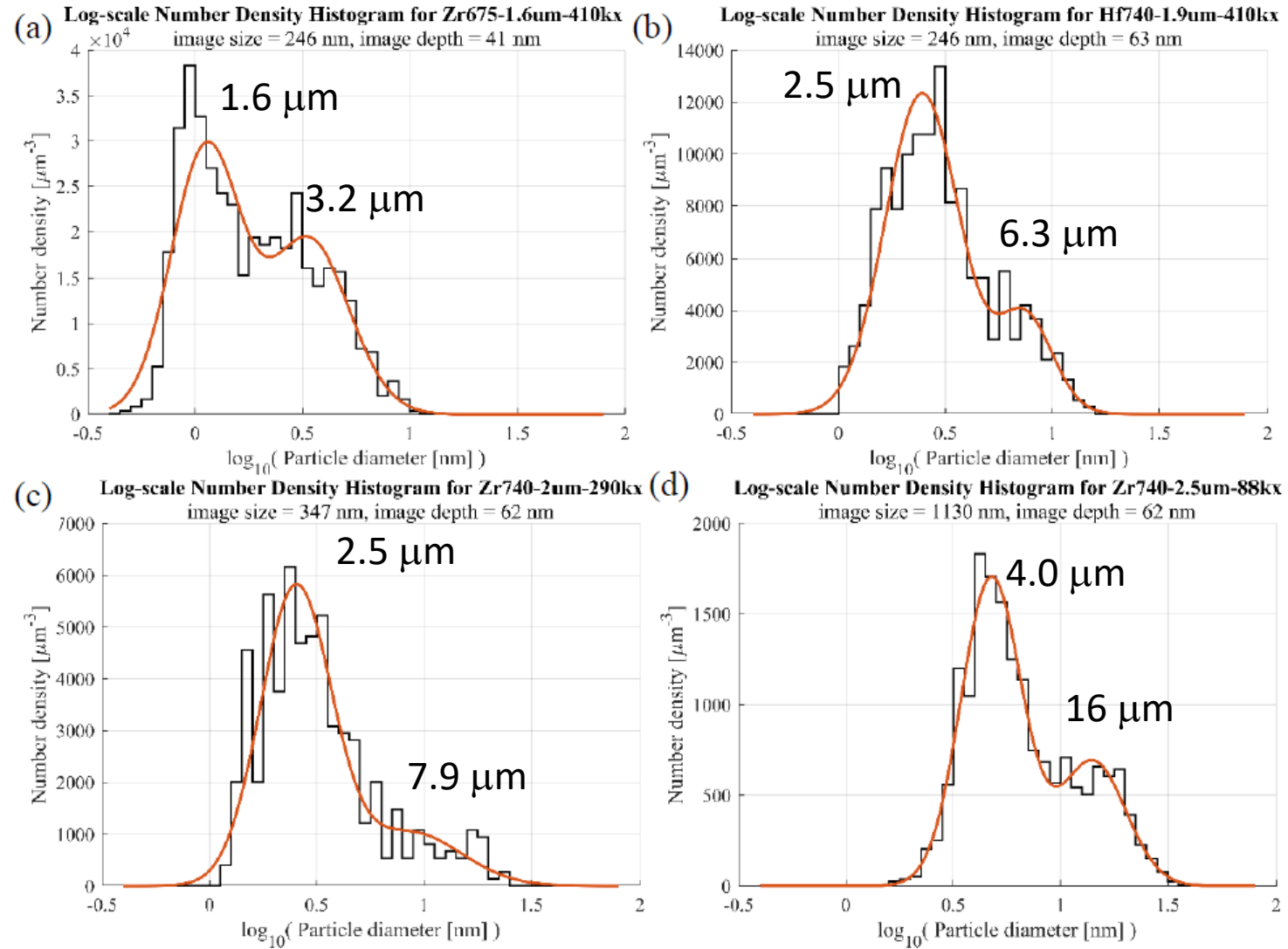
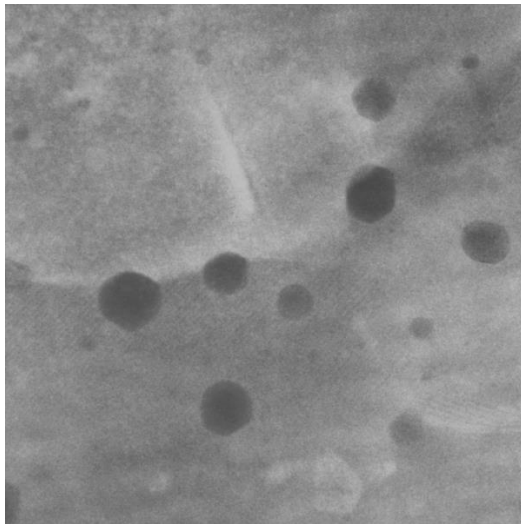


Figure 5.8. Selected particle size distributions from near 2 μm from the Nb/Nb₃Sn interface plotted on a logarithmic axis, from (a) Zr675, (b) Hf740, (c) Zr740 taken at high magnification, and (d) Zr740 taken at low magnification. Curve fit is of a Gaussian mixture model which fits two normal distributions to the data.

Growth of precipitates through the layer (with time)

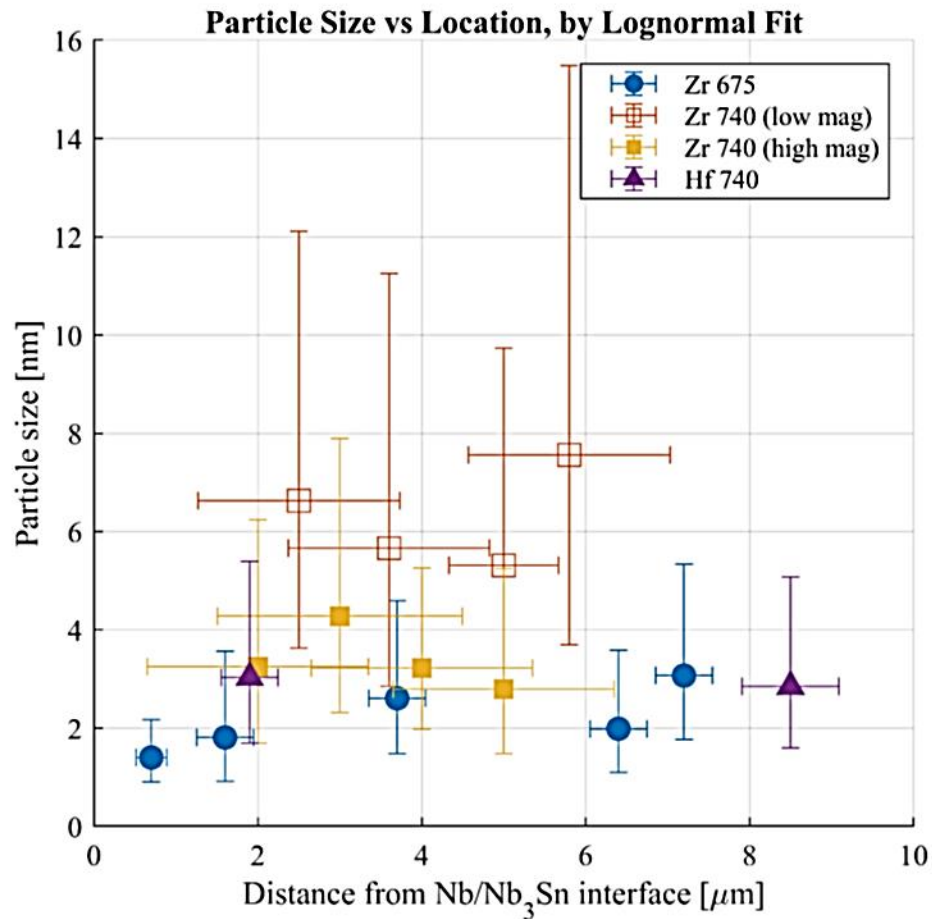


Figure 5.9. Particle size vs distance from the Nb/Nb₃Sn interface based on the lognormal distribution. Points represent the parameter μ and vertical error bars represent the parameter σ (the mean and standard deviation of the logarithms of particle size, respectively). The horizontal error bars represent the sum of the image width and the uncertainty in image location.

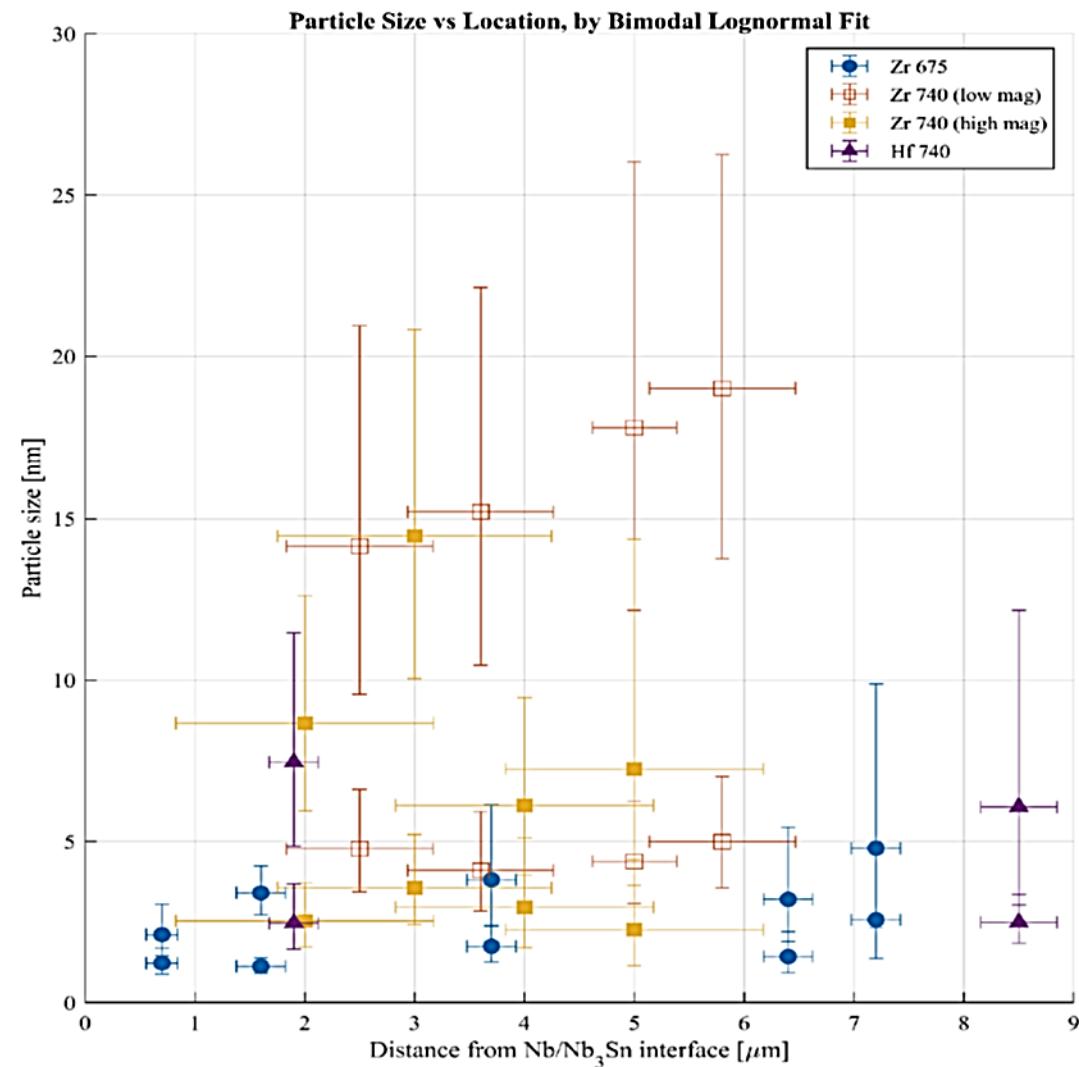
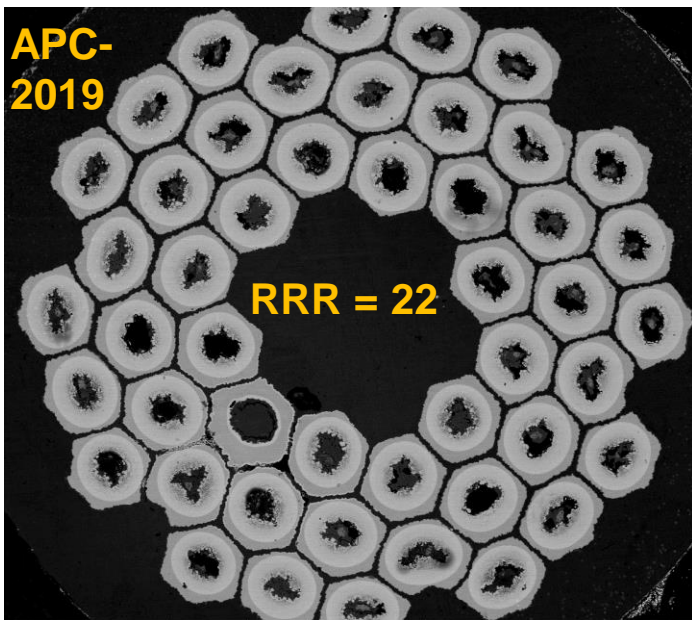


Figure 5.10. Particle size vs distance from the Nb/Nb₃Sn interface based on the bimodal lognormal distribution. Points represent the parameter μ and vertical error bars represent the parameter σ (the mean and standard deviation of the logarithms of particle size from both peaks in the bimodal fit, respectively). The horizontal error bars represent the sum of the image width and the uncertainty in image location.

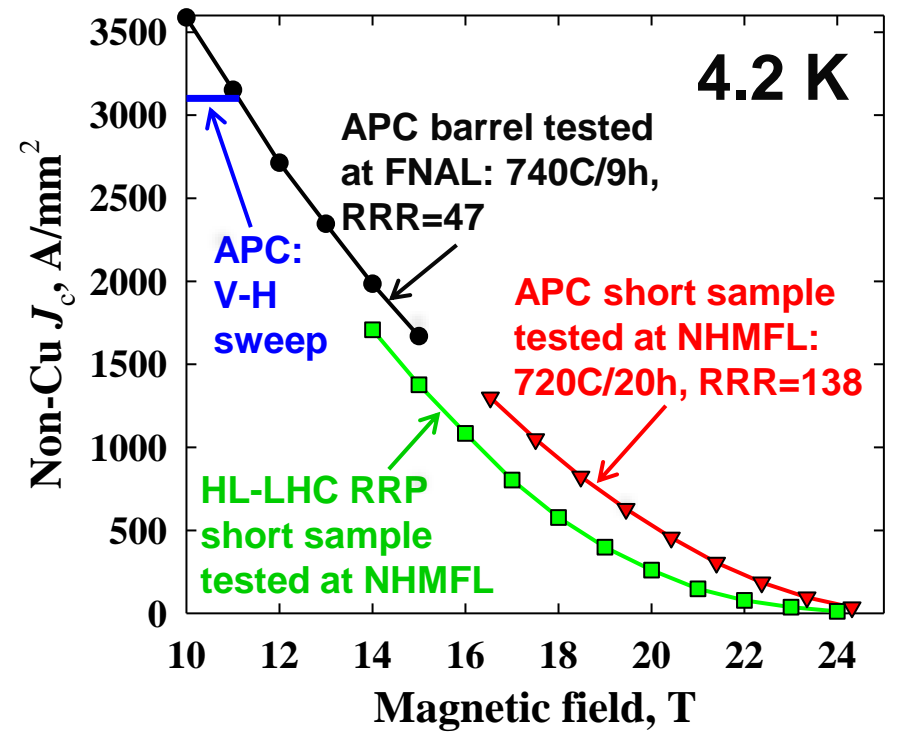
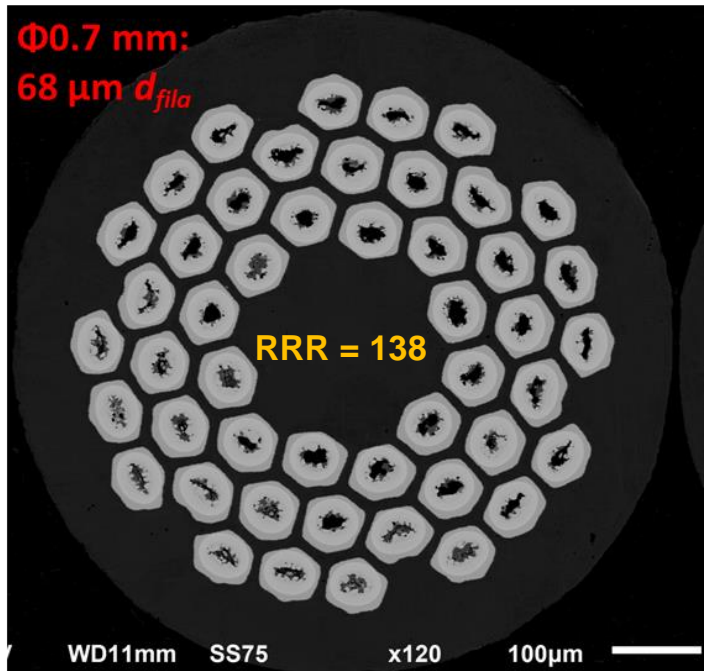
Solving the wire quality and instability issue

- What has been done:
 - Optimize wire design. The 2019 wires had very aggressive design, causing poor wire quality.
 - Use Nb alloy tubes with higher quality. Previous tubes had quality issue. New ATI tubes are better.

2019 wire: aggressive recipe + old Nb alloy tube w/ low quality:



Recent wire, using ATI Nb-Ta-Hf:



APC wires made using Nb-Ta-Hf seem to have lower $F_{p,max}$ and thus J_c than those using Nb-Ta-Zr.

- Stability can be further improved by (1) optimizing heat treatment to increase RRR, (2) reducing filament size.
- Some instability was due to testing in the short sample form

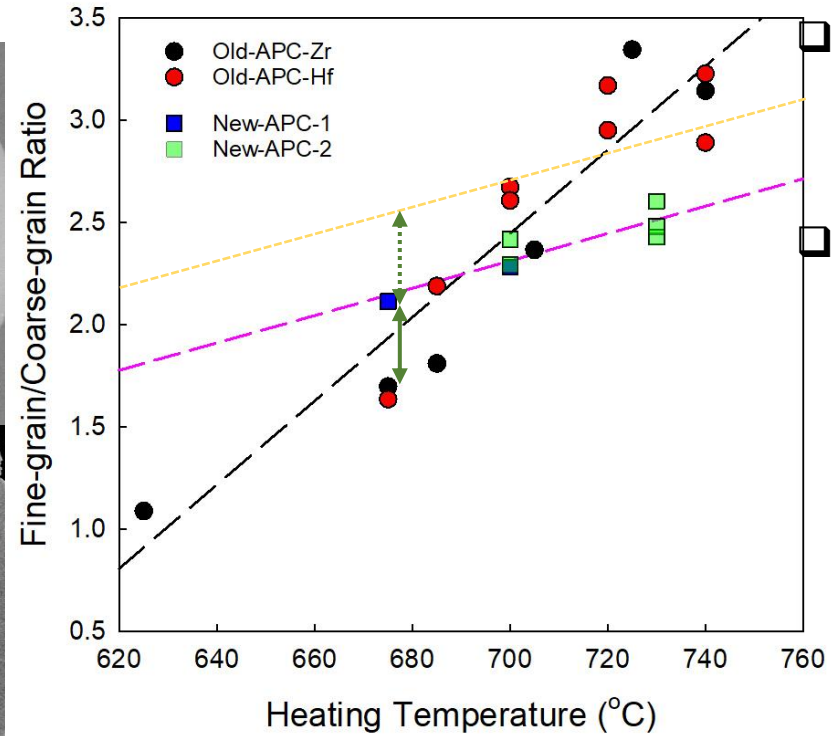
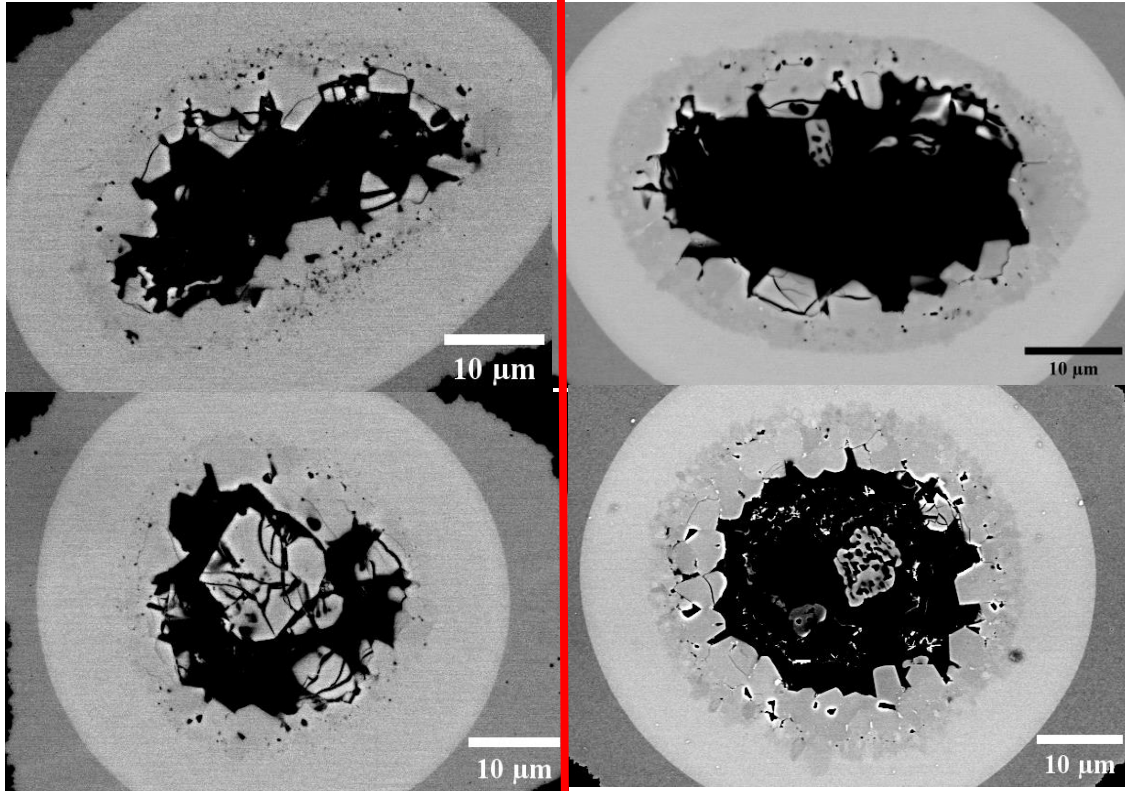


New APC Nb₃Sn conductors with Optimized Recipe

FNAL-HTR-OSU

New-APC-1, 675 °C
(T4313, T4348, T4350)

Old-APC, 675 °C
(T4141, T4113)



New APCs have higher FG/CG ratio than old APCs at 675 °C

Compared to old APCs, FG/CG ratio of new APCs decreases with decreasing heating temperature with a slower rate. In this case, new APCs have potential to attain higher FG/CG ratio than old APCs at low heating temperature

❖ In new APC reacted at 675 °C, disconnected CG regions were formed in some filaments. However, well-connected CG regions still exist in other filaments.

By further optimizing recipes of APC Nb₃Sn conductors:
It is expected that even higher FG/CG ratio can be achieved at low heating temperature.

Enhanced Nb₃Sn with Hf induced Grain refinement

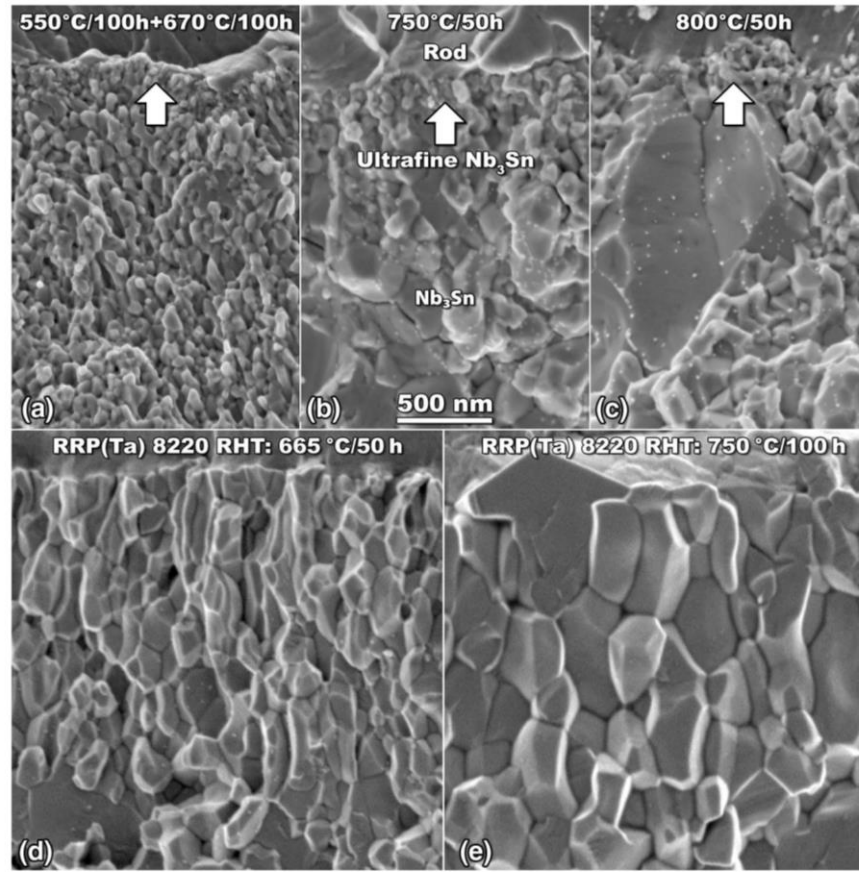
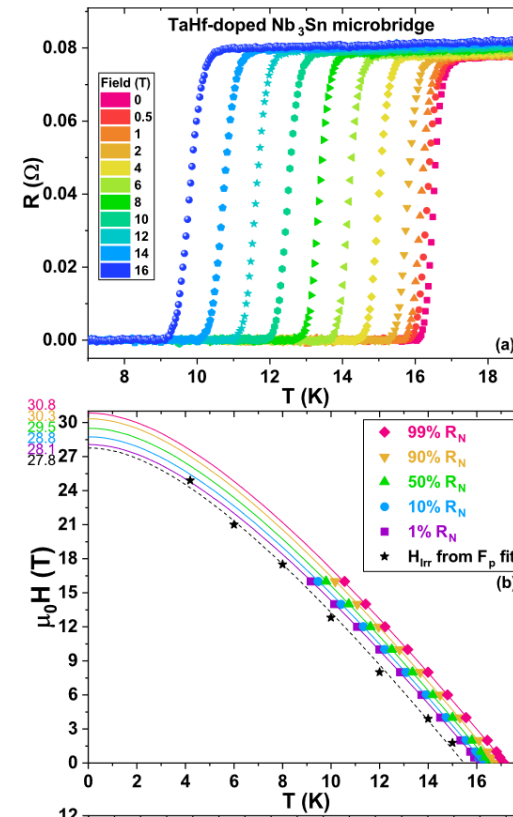


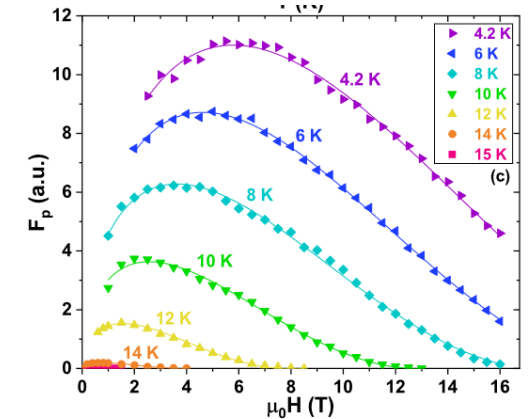
Figure 3. SEM characterization of Ta-Hf-doped Nb₃Sn compared with standard Ta-doped Nb₃Sn. Fractographs of Nb₃Sn grains after heat treatments at different temperature for Ta-Hf-doped samples made with home-made Nb₄Ta₁Hf special alloy (a-c) and for Ta-doped RRP wire made with industrial Nb₄Ta (d,e).



scientific reports

OPEN **Origin of the enhanced Nb₃Sn performance by combined Hf and Ta doping**

Chiara Tarantini^{1,2,3}, Fumitake Kametani^{1,2}, Shreyas Balachandran¹, Steve M. Heald³, Laura Wheatley⁴, Chris R. M. Grovenor⁴, Michael P. Moody⁴, Yi-Feng Su^{1,5}, Peter J. Lee¹ & David C. Larbalestier^{1,2}



Basic Understanding of B_{c2} in doped Nb_3Sn

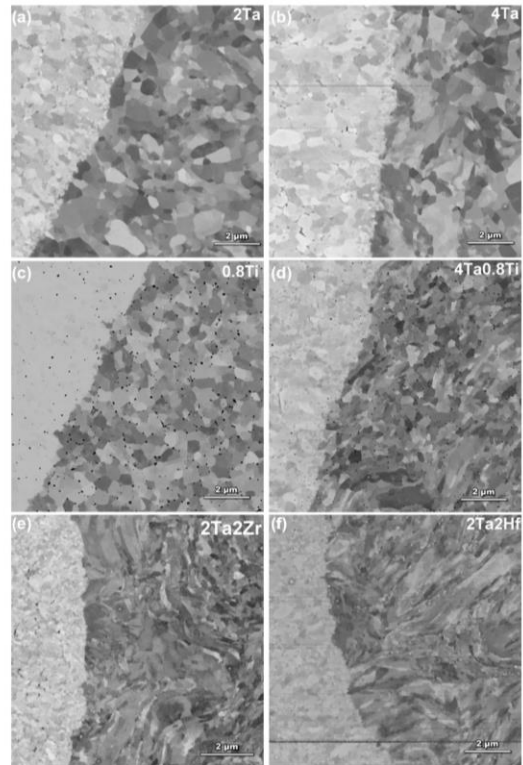


FIG. 5. Representative FESEM-BSE images of the Nb-alloy core/ Nb_3Sn interface after the monofilaments were reacted at $550^\circ\text{C}/50\text{ h} + 750^\circ\text{C}/50\text{ h}$. The darker Nb-alloy cores are on the right and the lighter A15 diffusion layers are on the left of the interface (sample IDs are indicated in the top right corner of each image). Electron channeling contrast in the corresponding images reveals recrystallized microstructures in the unreacted Nb_xTa_x ($x = 2, 4$), $Nb_{0.8}Ti$, and $Nb_4Ta_{0.8}Ti$ alloys. In contrast, the Nb_2Ta_2Hf and Nb_2Ta_2Zr alloys retain a deformed, cold-worked grain structure.

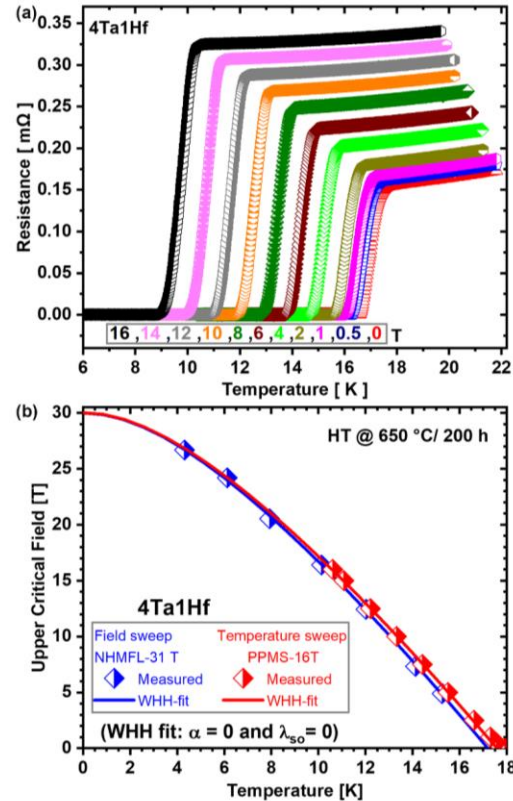


FIG. 6. (a) The traces of resistance against temperature using temperature sweeps at constant field from 0 to 16 T in our 16 T PPMS for Nb_4Ta_1Hf reacted at $550^\circ\text{C}/50\text{ h} + 650^\circ\text{C}/200\text{ h}$. (b) At the bottom we show the experimental $H_{c2}(T)$ values and their WHH fits in PPMS 16 T and NHMFL 31 T.

with the paramagnetic limitation parameter (α) and a spin-

Influence of Nb alloying on Nb recrystallization and the upper critical field of Nb_3Sn

Nawaraj Paudel¹, Chiara Tarantini¹, Shreyas Balachandran^{1*}, William L. Starch, Peter J. Lee¹, and David C. Larbalestier^{1†}
¹Applied Superconductivity Center, National High Magnetic Laboratory, Florida State University, Tallahassee, Florida 32310, USA

(Received 16 May 2024; accepted 15 July 2024; published 1 August 2024)

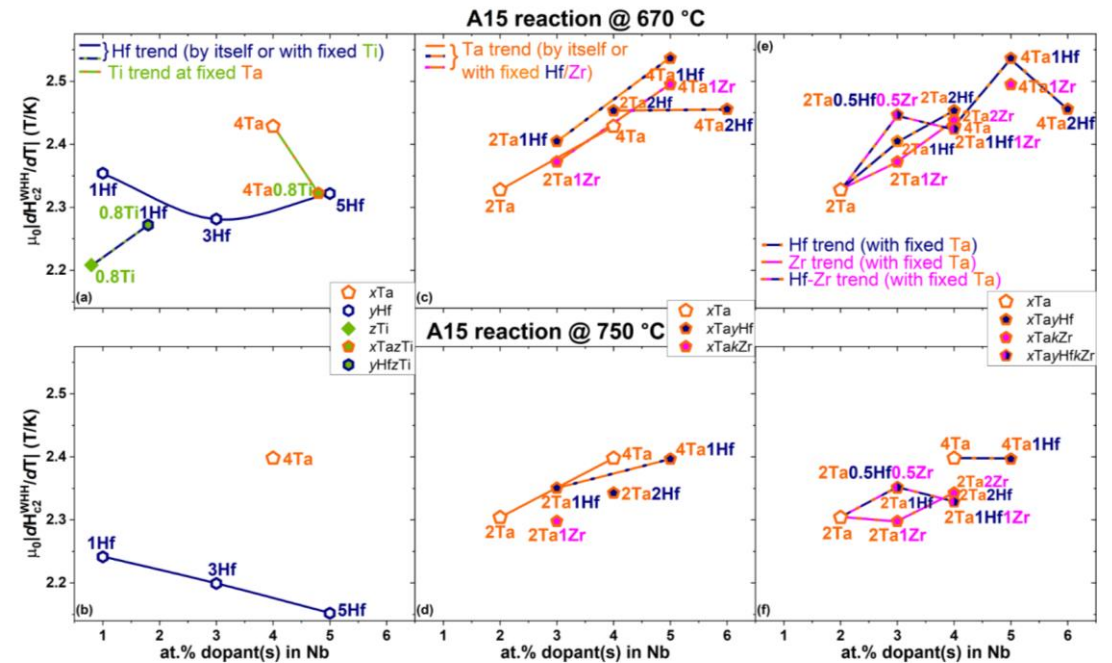


FIG. 8. H_{c2} slope evaluated by the WHH fit for alloyed A15 samples reacted at $550^\circ\text{C}/100\text{ h} + 670^\circ\text{C}/100\text{ h}$ (top row) and at $550^\circ\text{C}/50\text{ h} + 750^\circ\text{C}/50\text{ h}$ (bottom row) as a function of the amount of dopant(s). The same alloy sets as used for the (a)-(b), (c)-(d), and (d)-(e) columns in Fig. 7 are used for the column sets here. As explained in the text, the labels refer to the atomic percentage of dopant(s) in the unreacted Nb alloys.

Gianmarco BOVONE, Francesco LONARDO, Florin BUTA, Carmine SENATORE



Department of Quantum Matter Physics, University of Geneva, Switzerland
 Department of Nuclear and Particle Physics, University of Geneva, Switzerland

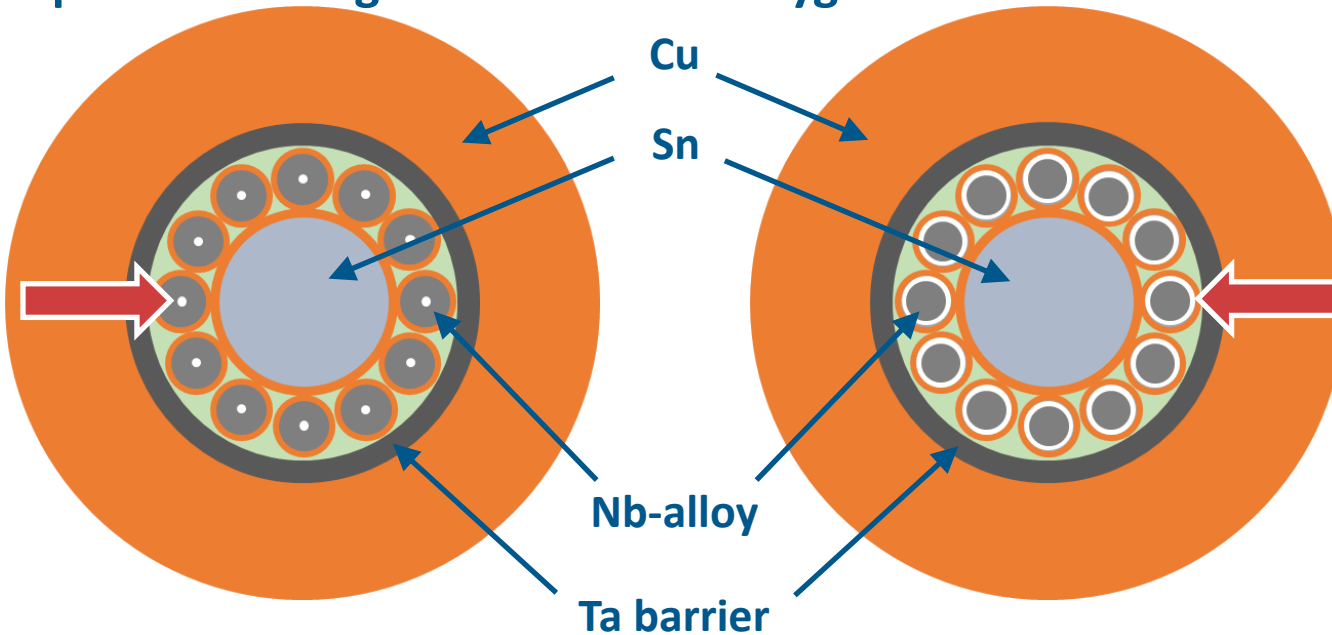
Internal Oxidation of test-bed
Internal Sn subelements

Simon HOPKINS, Thierry BOUTBOUL



CERN, Switzerland

Two possible configurations for the oxygen source



SnO₂ Core

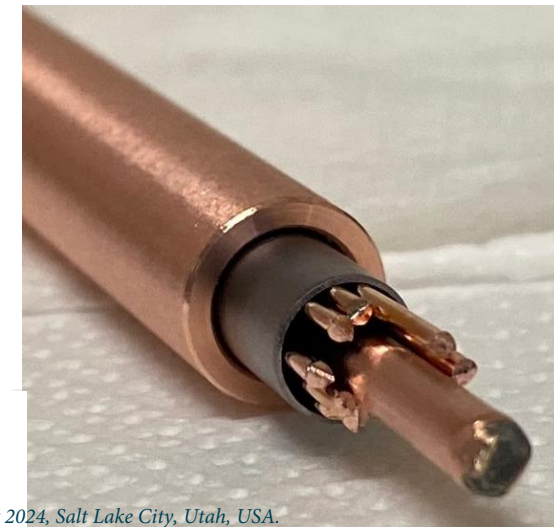
SnO₂ powder inside the Nb-alloy filaments

SnO₂ Annular

SnO₂ powder between the Nb-alloy filaments and the Cu tube

Nb-alloy	Oxide configuration
Nb-7.5wt%Ta (REF.)	None
Nb-7.5wt%Ta-1wt%Zr	None
	SnO ₂ Core
Nb-7.5wt%Ta-2wt%Hf	None
	SnO ₂ Core
	SnO ₂ Annular

Two commercial ternary alloy were tested with **1wt%Zr** and **2wt%Hf**



G. Bovone *et al.*, Supercond. Sci. Tech. **36** (2023) 095018
 DOI: [10.1088/1361-6668/aced25](https://doi.org/10.1088/1361-6668/aced25)

Internal Oxidation of test-bed Internal Sn subelements

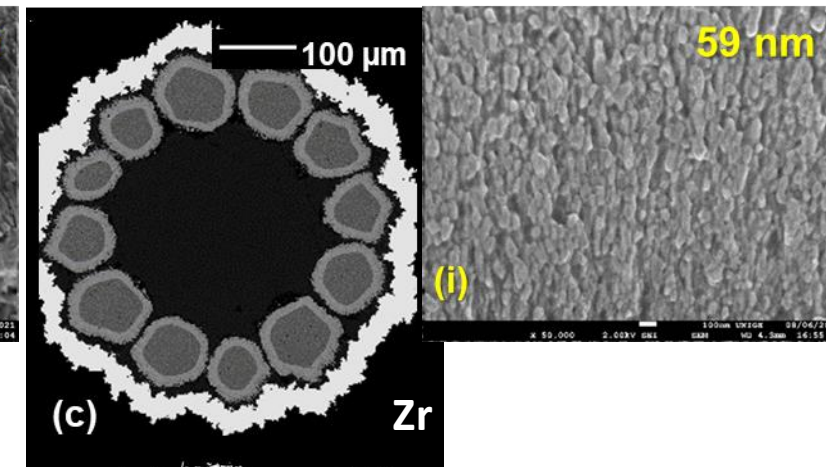
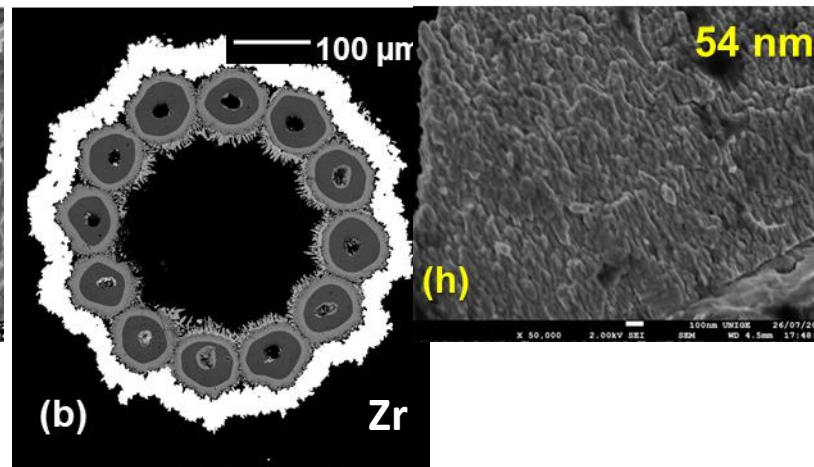
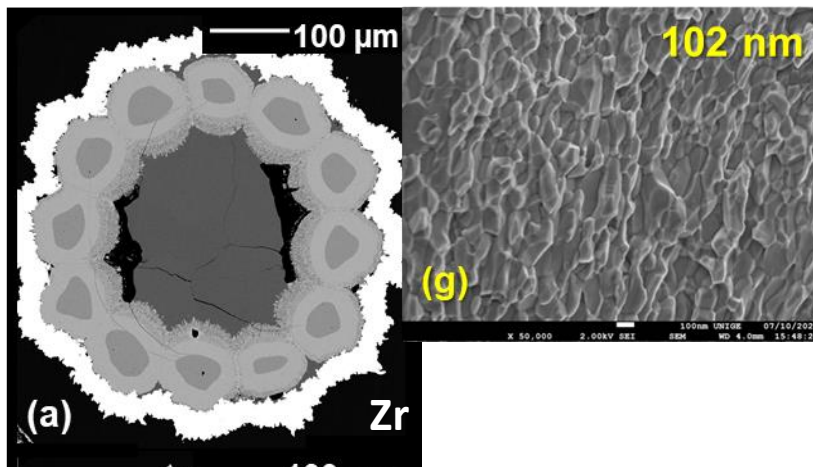
12-filament wires with an internal Sn source

w/o oxygen source

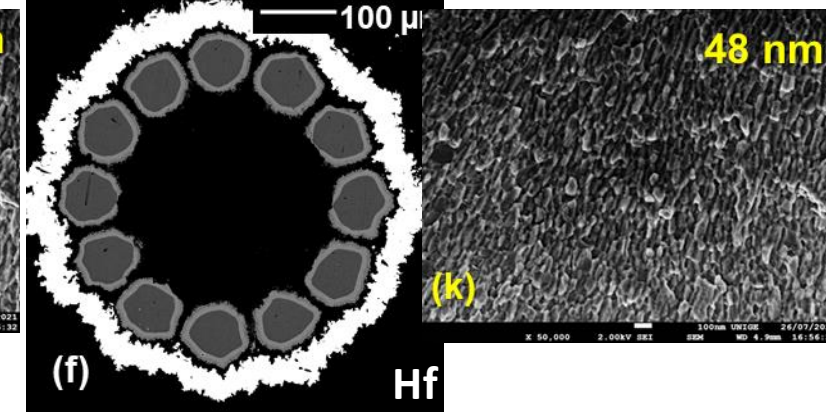
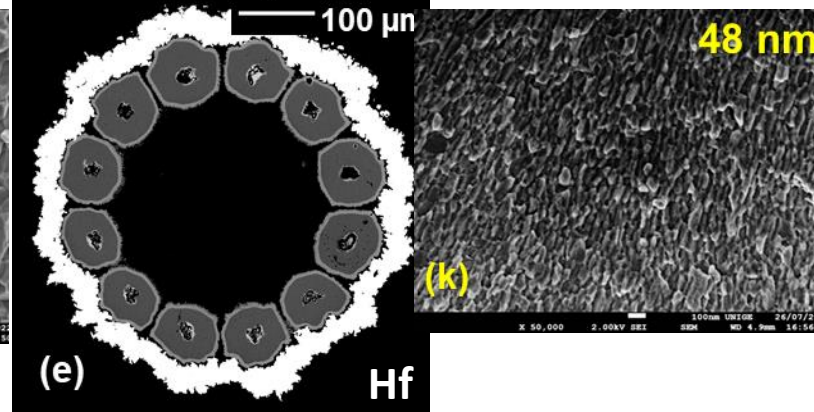
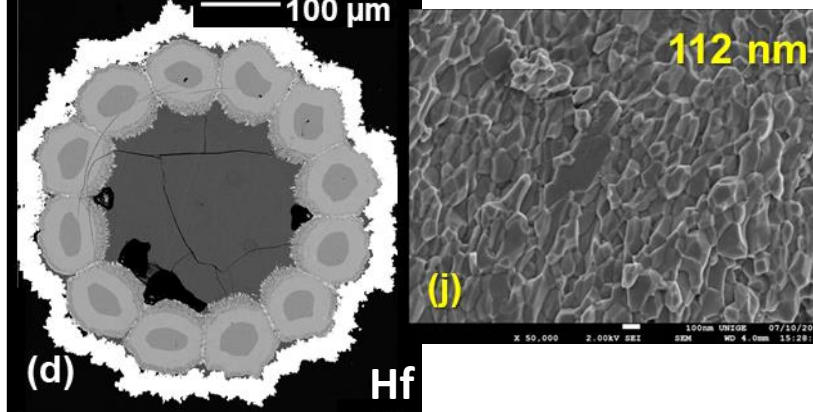
SnO₂ Core

SnO₂ Annular

Nb-7.5wt%Ta-1wt%Zr



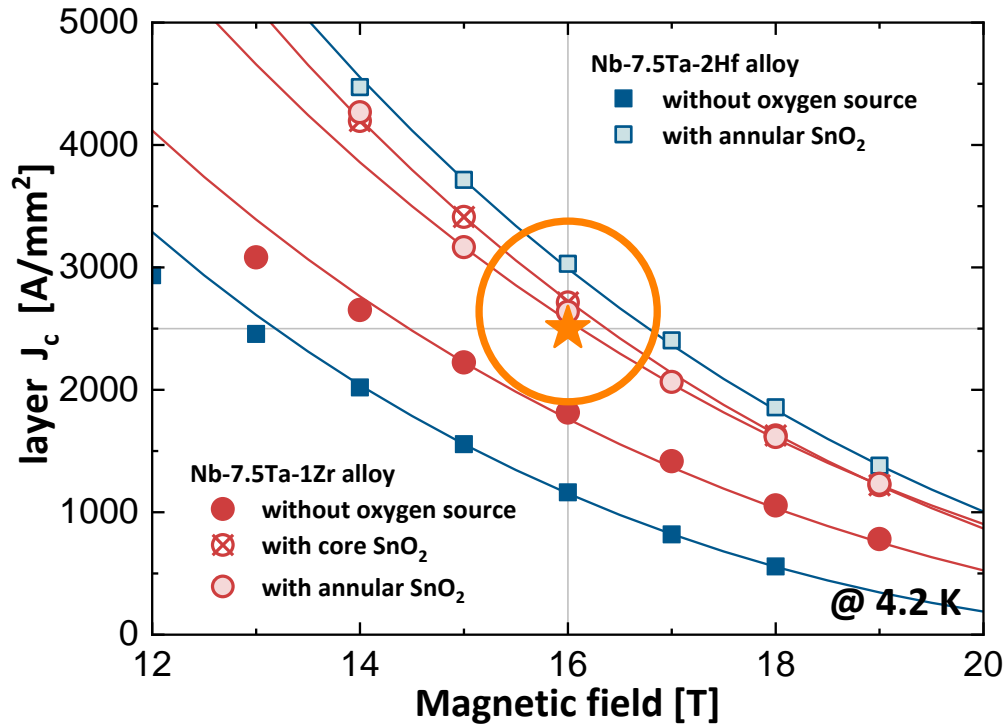
Nb-7.5wt%Ta-2wt%Hf



Internal oxidation leads to a refinement of the grain size from ~100 nm to ~50 nm regardless of the oxygen source configuration

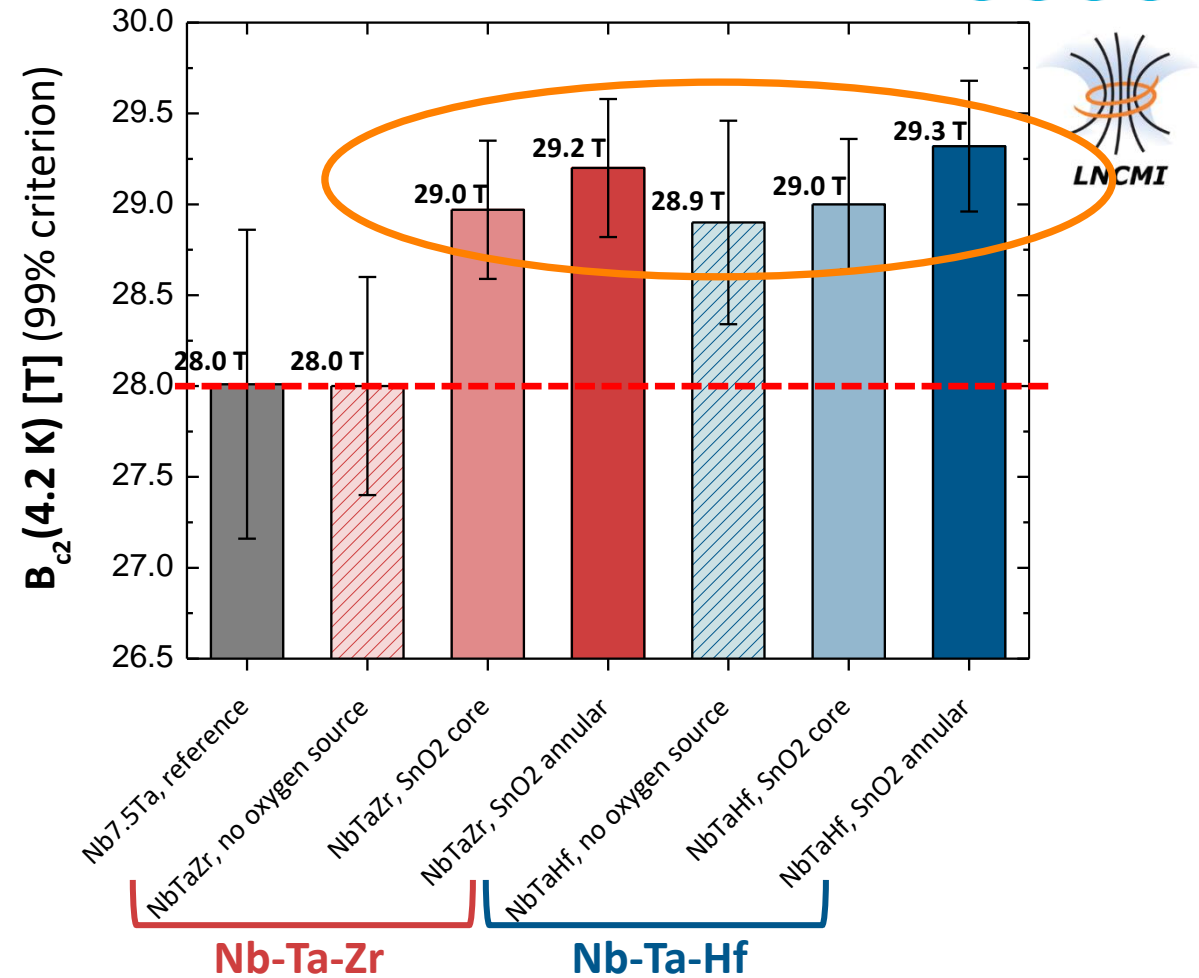
Internal Oxidation of test-bed Internal Sn subelements

Transport J_c and B_{c2} measurements



Layer J_c determined from transport measurements

FCC layer J_c (4.2K,16T) = 2'500 A/mm²
 considering 60% of Nb₃Sn in the non-Cu area

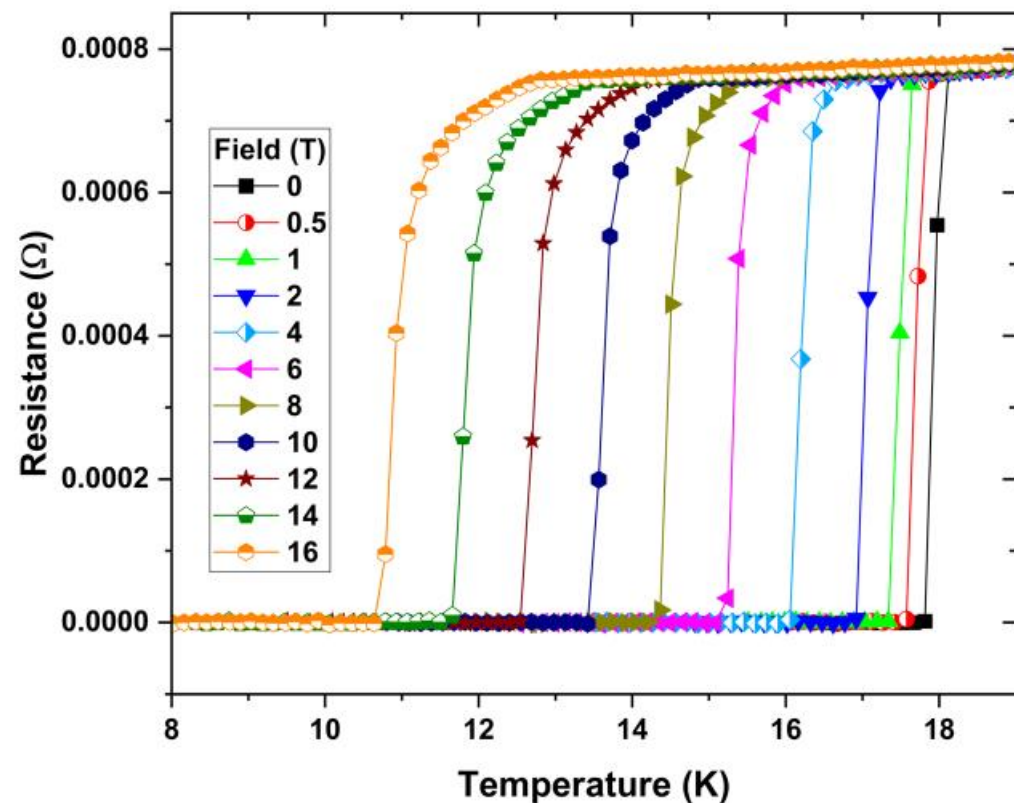


R(B) tests performed up to 33 T at LNCMI-Grenoble confirm that the record high B_{c2} values are achieved both with Hf and Zr

Exceptional High H_{c2} and H_{irr} in alloyed Nb_3Sn bulk samples

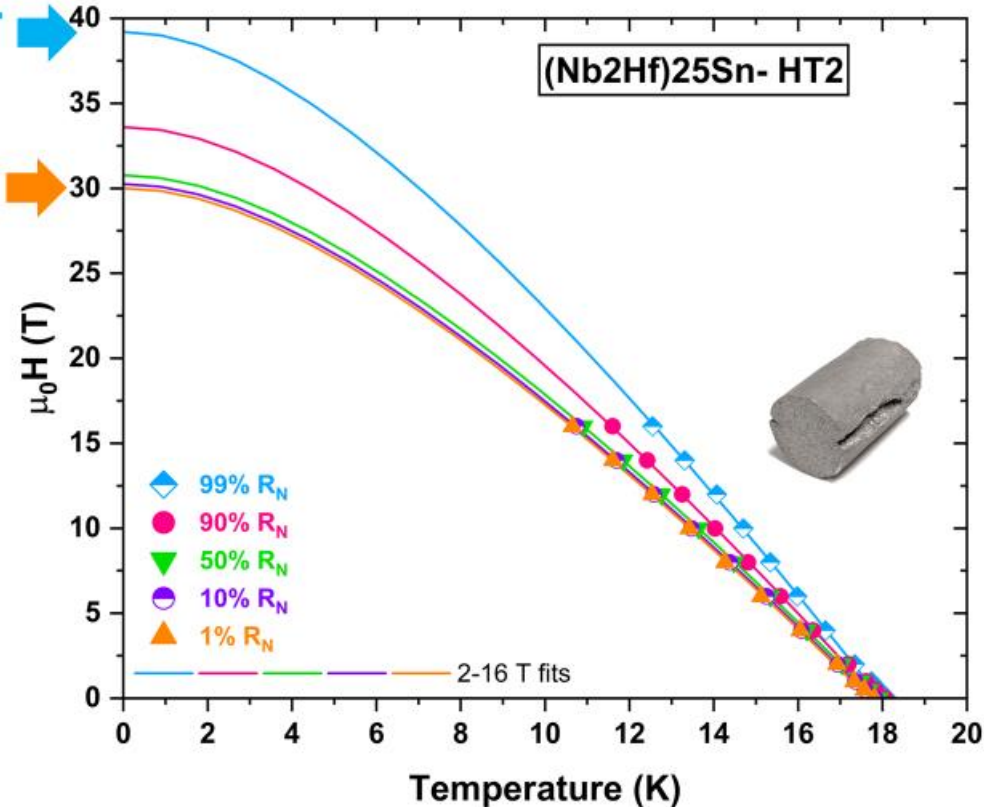
Manish Mandal, Chiara Tarantini, William L Starch, Peter J Lee, and David C Larbalestier

Florida State University



$\mu_0 H_{c2,99\%}(0) = 39.2 \text{ T}$

$\mu_0 H_{irr,1\%}(0) = 30.0 \text{ T}$



WHH extrapolations to 0 K

Conclusions and Take home Message

- LTSC have great continuing utility in commercial and technical/scientific applications
- They will be used for a number of future accelerator and fusion programs
- They have some potentially interesting new niche applications
- They have continuing potential for property improvement – as evidenced by a number of recent and exciting new results
- They can be expected to complement HTSC conductors moving forward