

Progress on a 100 kW fully HTS propulsion motor for zero emission aviation

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- "ZEST1 Zero Emissions for Sustainable Transport 1", funded by Innovate UK
- "Superconducting Machines for Zero Emission Aviation", selected by ERC and funded by UK Research and Innovation

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Electrification in aviation helps to achieve net-zero targets

Greenhouse gas emissions from the EU's transport*



*Excluding the United Kingdom

***The number of flights decreased in 2020 due to Covid-19 restrictions

Sources: European Environment Agency (2022), Eurostat [avia_paoc] (2022)

- The global **aviation** industry has agreed to try to achieve net-zero emissions by 2050
- One promising way for reducing emission is via electrification
- Conventional electrical motors are too heavy for aviation
- Improving conductor current density leads to lighter and more powerful electrical motors

^{**}Projections with existing measures

Improving conductor current density is desirable but with penalty

GKN Aerospace Launches H2FlyGHT: Pioneering £44M Project for 2 MW Cryogenic Hydrogen-Electric Propulsion

23 May 2024

Innovation

Airbus takes superconductivity research for hydrogenpowered aircraft a step further

* Calculation in "Analytical ac loss comparison between ReBCO, MgB2, copper and aluminum Litz wires for cryogenic electrical machines", to be published in IEEE TAS



Fig. 2: Loss per unit length of conductor when the conductors, at different temperatures, are carrying 150 Hz transport ac of different amplitudes (amplitudes converted to engineering current densities). The conductors are simultaneously being subject to 150 Hz alternating external magnetic field of amplitude 0.4 T.





250 kW GREEN and Safran

Improving conductor current density is desirable but with penalty



Fig. 2: Loss per unit length of conductor when the conductors, at different temperatures, are carrying 150 Hz transport ac of different amplitudes (amplitudes converted to engineering current densities). The conductors are simultaneously being subject to 150 Hz alternating external magnetic field of amplitude 0.4 T.

- Improving current density by providing cooling
- Cooling penalty must be considered by estimating losses

ReBCO is interesting to us:

DC rotor: zero losses with high magnetic loading AC stator: @50 K, lower losses above 5e8 Am⁻²

Exploring the potential of HTS in aviation motor

Major challenges we are facing:

- 1. Rotor: how to provide very large DC for rotational HTS coils
- 2. Stator: how to design multi-filament HTS AC coils with minimized AC losses
- 3. Different temperature requirements for rotor and stator

Main targets we want to achieve:

- Use a single type of superconductor to replace copper
- Use a simple topology
- Remove iron if possible
- >=15 kW/kg power density

100 kW motor design

Brushless axial-flux fully superconducting motor

Key novelties:

- HTS DC windings for brushless rotor
- HTS coupling AC windings for stator



- Two HTS stators
- One HTS rotor
- Double pancake coils



Achievabl	e Testing		
value	value	Unit	Description
200	100	kW	output power
1500	1500	rpm	rated speed
2	2		pole pair number
			peak current apply to one
250	160	Apk	stator
3	3		phase number
2	1.4	Т	magnetic loading
300	300	Vrms	phase voltage rms

100 kW motor design

3D FEM simulation to confirm motor performance:



100

200 (mm)







HTS rotor

HTS brushless rotor

Rotor challenge: how to provide very large DC for rotational HTS coils



Key requirements:

- 1. Higher magnetic field than PM with an air-cored design.
- 2. slow magnetic field decay rate

Solution: Closed-loop HTS coils + removeable charger

HTS brushless rotor

Previous feasibility study at 4 K*:



Brass holder



* Test was supported by LNCMI-CNRS, a member of the European Magnetic Field Laboratory (EMFL)

HTS brushless rotor: charging



HTS brushless rotor : low resistive joints

Low-resistive soldering joints :

- Temperature 200-260K
- Weight 60-180 kg
- Tested temperature-pressure variations



HTS brushless rotor : low resistive joints

• Mechanical strength of HTS joints at room temperature*



* Test was supported by Strathclyde Advanced Material Research Laboratory

aboratory lower than the yield strength of joints tested

HTS brushless rotor: decaying





Charged current	500 A		
Inductance	2640 μH		
Resistance	10 nΩ		
Temperature	50 K		
3 hour decay	1.48T -> 1.42T 4.1%		
10 hour decay	1.48T -> 1.29T 12.8%		

• Decay rate is acceptable for a 3 hour flight



HTS Stator

Challenge:

- Use narrow HTS to reduce AC loss
- Peak current is 160 A at 1.4 T

Solution: a HTS coupled winding

- Four 4mm HTS in parallel connection
- Operational temperature at 65 K to increase Ic
- Six HTS double pancake coils per stator
- Fully insulated and impregnated

Value	Unit	Description
4	mm	tape width
65	К	working temperature
250	A	self field coil Ic @ 77K
160	A	Peak current @ 1.4T





Polyimide Solder Copper Silver HTS layer Buffer layers Hastelloy C-276

*AC loss measurement of the coupled coils in presentation 1LOr1D-02



Calculated IcB is 220 A @ 77 K self-field. Measurements for six coils are consistent with simulation:





This coil experiences two types of coupling:

 Coupling via current leads between two stacks. This can be removed by inductance balance as shown below*:







- Coupling within one stack via the soldering layer. This is impossible to model in 2D for the transverse current flowing
- AC loss consists of HTS losses, coupling loss in the stack, coupling losses between two stacks (without inductance balance) and soldering losses.



Tests that were carried out so far:

- A four-pole PM rotor assembled next to the stator for testing purpose
- 800 V voltage breakdown test passed
- Open circuit voltage matches simulation









PM Stator Rotor

800V breakdown test was passed

Test in generator mode (rotating rotor, no load)

HTS stator: the relative position of the second stator



Face-face stators





30 deg shift for the second stator



- Much less third harmonics
- But only 60% of the torque



Cooling

Motor cooling



Cryogenic drive with SFCL Subcooled LN2 IEEE-CSC, ESAS and CSSJ SUPERCONDUCTIVITY NEWS FORUM (global edition), Issue No. 57, Oct 2024. Presentation given at ASC 2024, Sept 2024, Salt Lake City, Utah, USA.

Motor cooling

Thermosiphon rotational cooling

Coldhead cooling power: 50 W @ 20K





Experiment results with N2

 Time=0 min
 Surface: Temperature (K)

 \$316\$

 300

 250

 200

 150

 100

 50

 271

Thermosiphon happened here: Liquid nitrogen formed, leading to a rapid cooling for the rotor terminal.





We plan to test neon as next step Boiling point of Neon: 27.1K

Conclusion

We have designed and developed a 100 kW fully axial-flux HTS motor for aviation propulsion

- Designed power density is 15 kW/kg
- Novel brushless HTS rotor technology
- HTS coupled AC windings for stator
- Neon thermosiphon and sub-cooled LN2 for motor cooling

We are looking for visiting researchers and PhD students to work on the following topics:

- 1. HTS simulation
- 2. AC loss measurement
- 3. HTS motor design and development





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