

DC Superconducting Cables for present and future power needs

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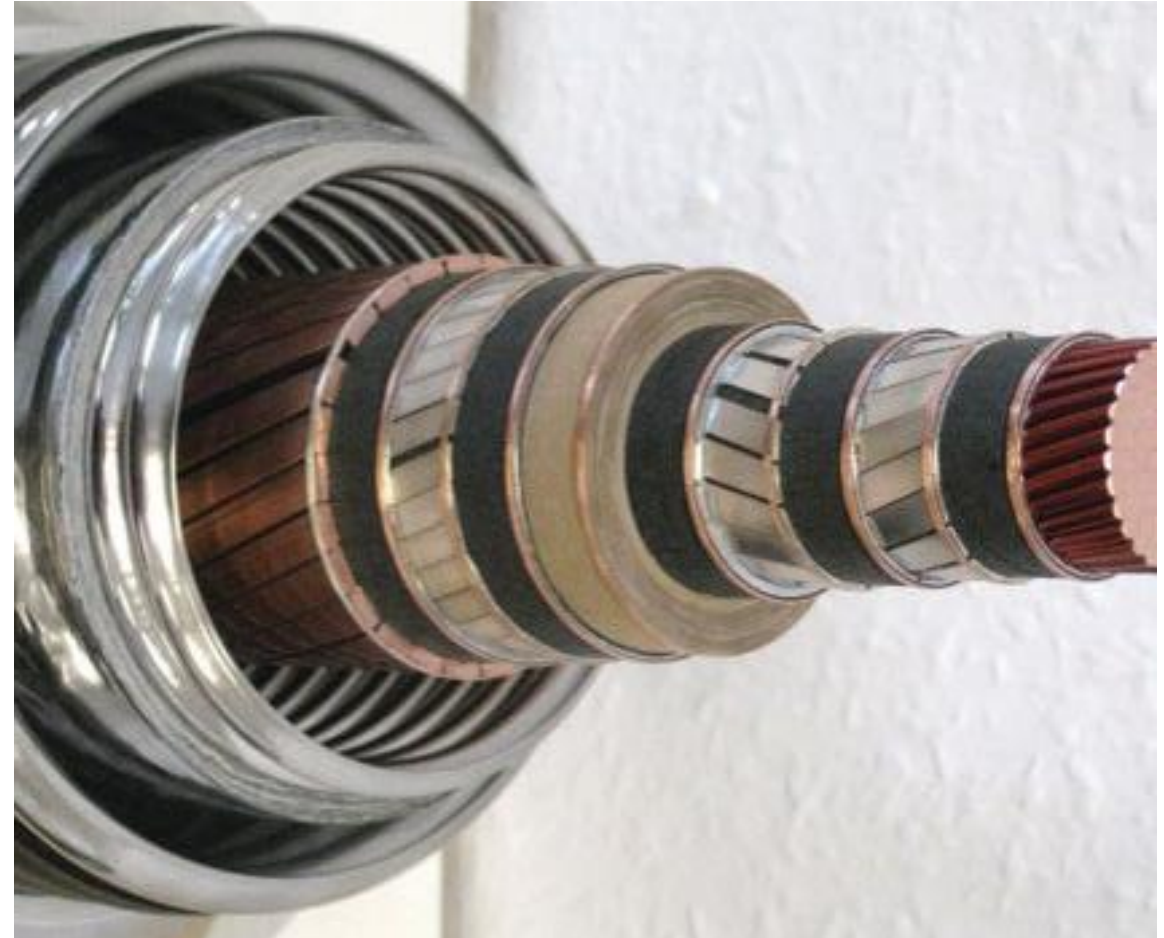
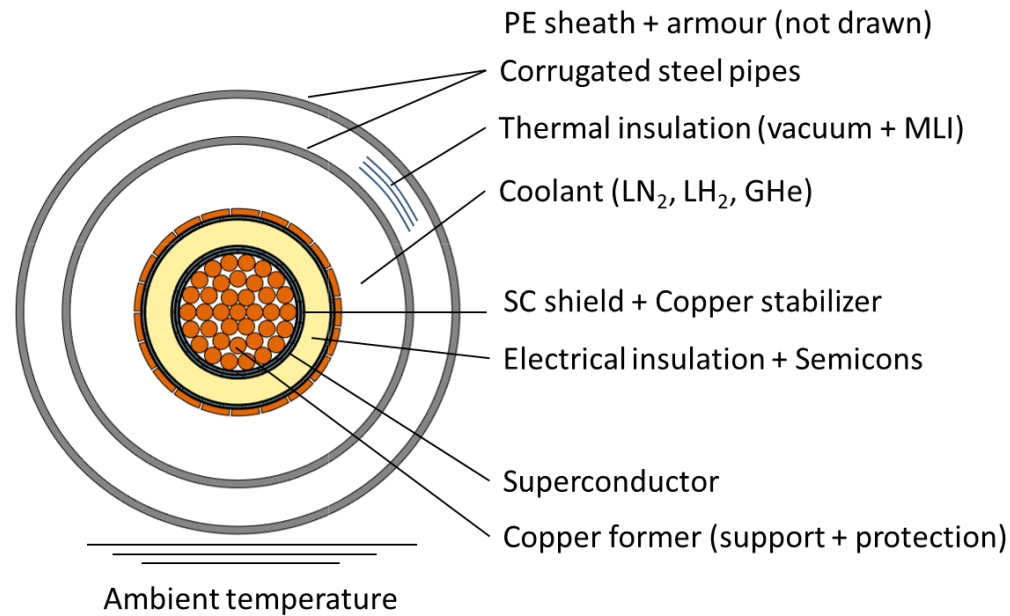
December 2, 2025, Nagasaki, Japan

Outline

HTS power cables:

- **Technology and state of the art**
 - **General characteristics and main components of SC cables systems**
 - **State of the art**
- **DC superconducting cable for today and tomorrow's power needs**
 - **How much**
 - **Which type**

Layout of a cold dielectric superconducting power cable



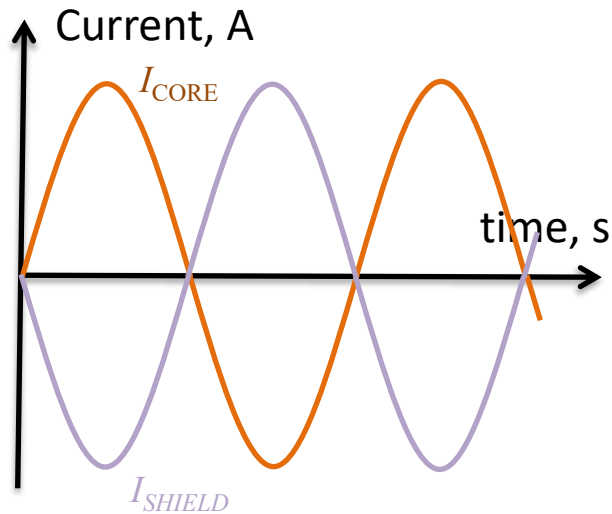
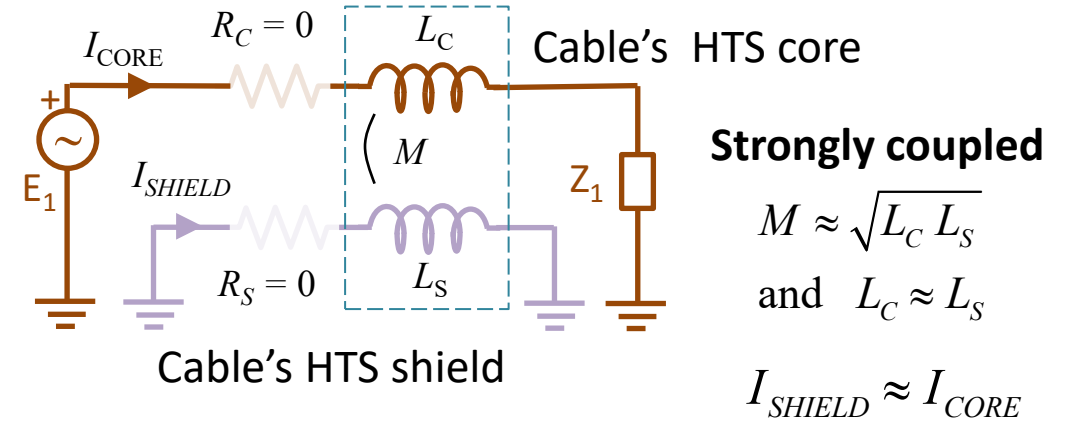
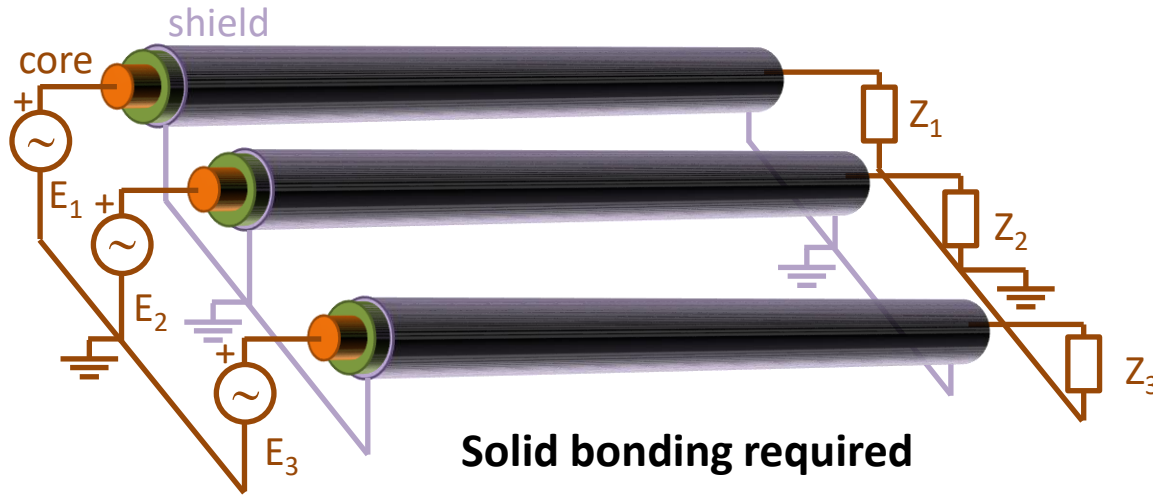
Courtesy of Nexans

A shield is required to

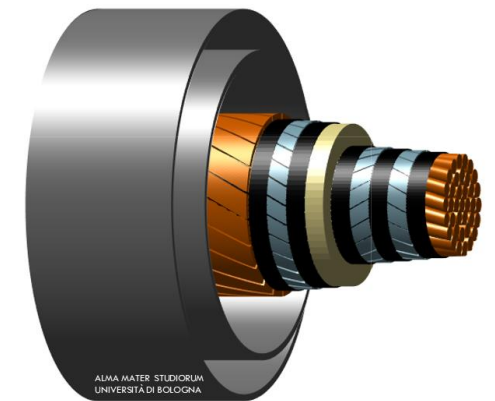
- Equalize electric field stress in the cable insulation
- Shield EM field + provide return path for neutral and fault current
- **Prevent induced currents and loss in metallic pipes**

Shield design of AC superconductor cables

AC cable system (pipes not drawn)

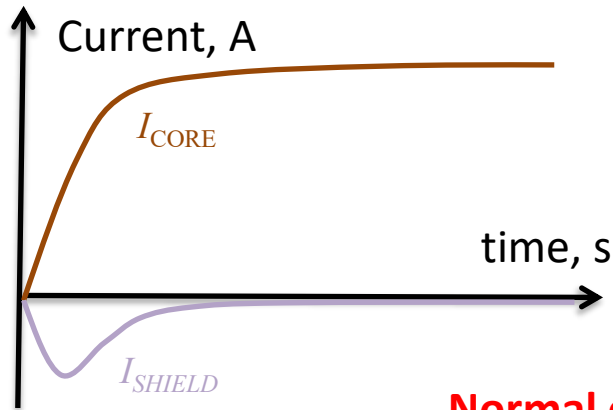
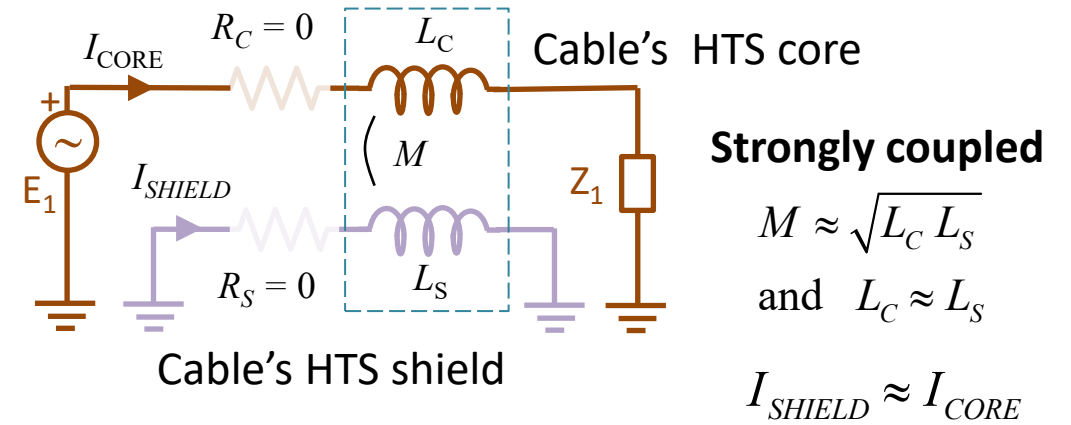


- Induced currents in inner metallic pipe and additional heat load are prevented with the HTS shield
- Practically the same AC current (with 180° phase shift) of the core circulates in the shielding steady AC regime. **The same amount of SC as for the core is needed for the shield**



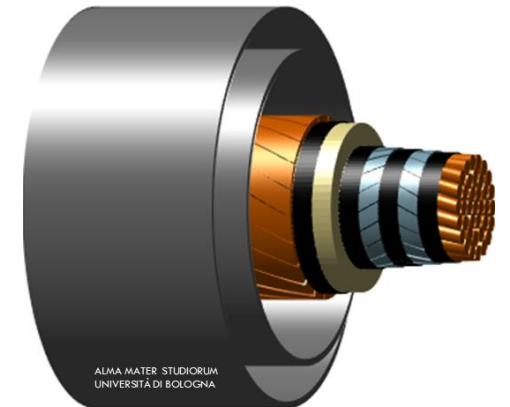
Shield design of DC superconductor cables

DC cable system (pipes not drawn)

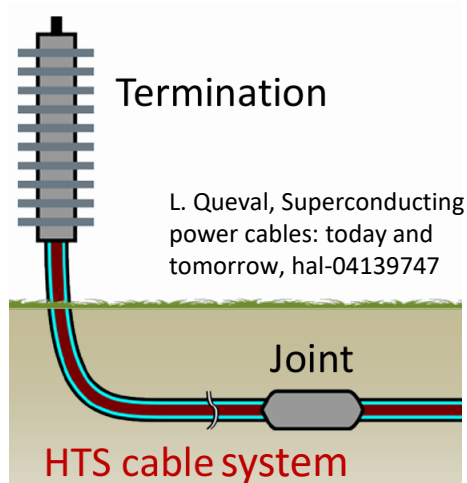


- Current is induced in the shield only during transients (energization and fault)
- No significant heating is added to the cable also in case of copper shield

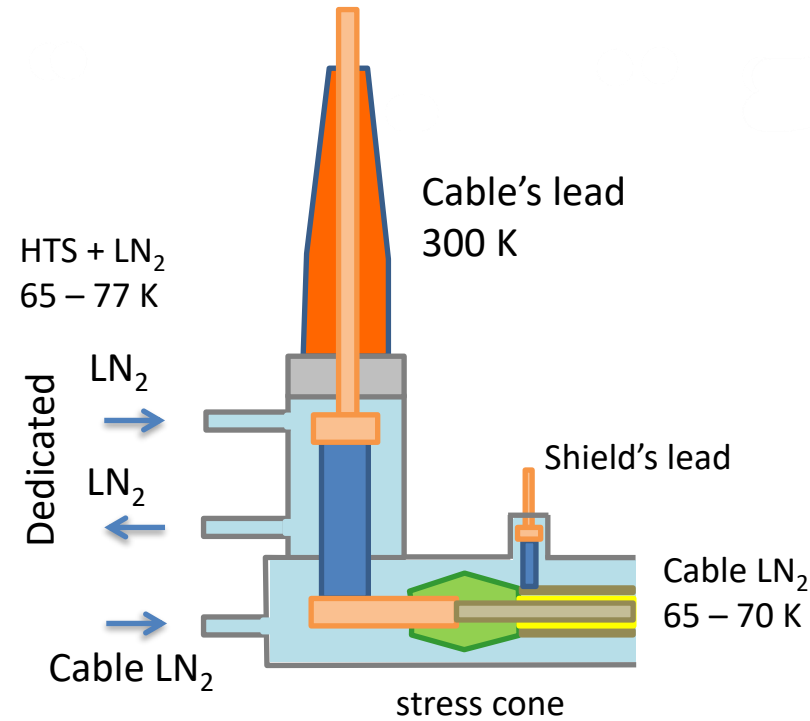
Normal conducting shield for DC superconducting cables is viable



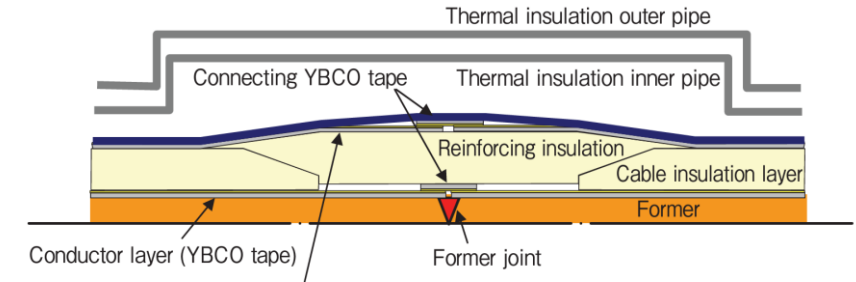
Essential “accessories” of HTS (and conventional) power cables: terminations and joints



Schematic of the termination



Schematic of the joint



S. Mukoyama et al., Development of YBCO High-Tc Superconducting Power Cables, Furukawa Review, No. 35 2009

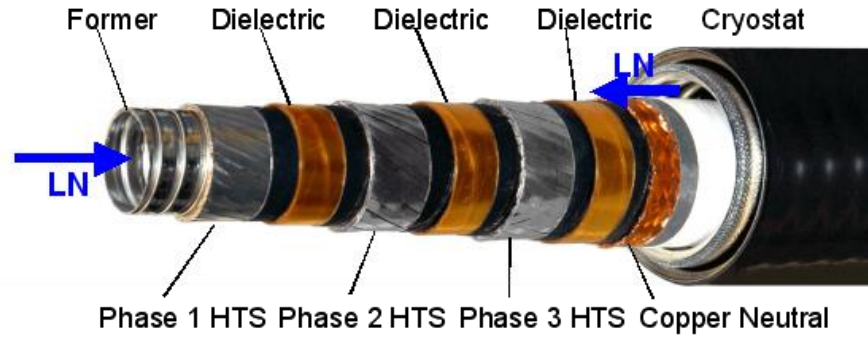
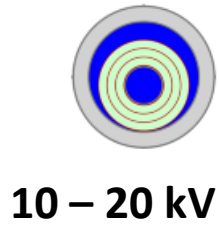
Termination of the LIPA1 HTS cable

Courtesy of Nexans

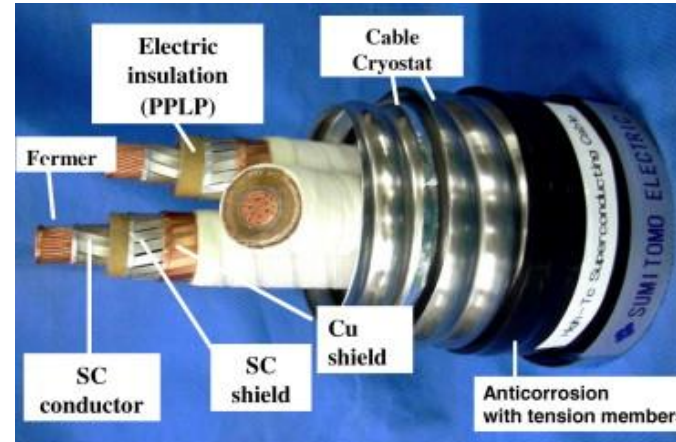
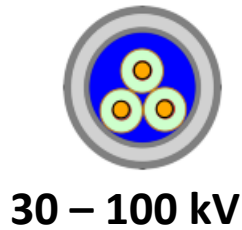


- Connection to the grid
- Management of electric stress
- Management of thermal gradient
- Management of mechanical contraction during cool down

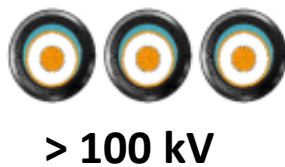
AC three phase or DC bipolar arrangements



Concentric phases/poles



Separate phases/poles with shared cryostat



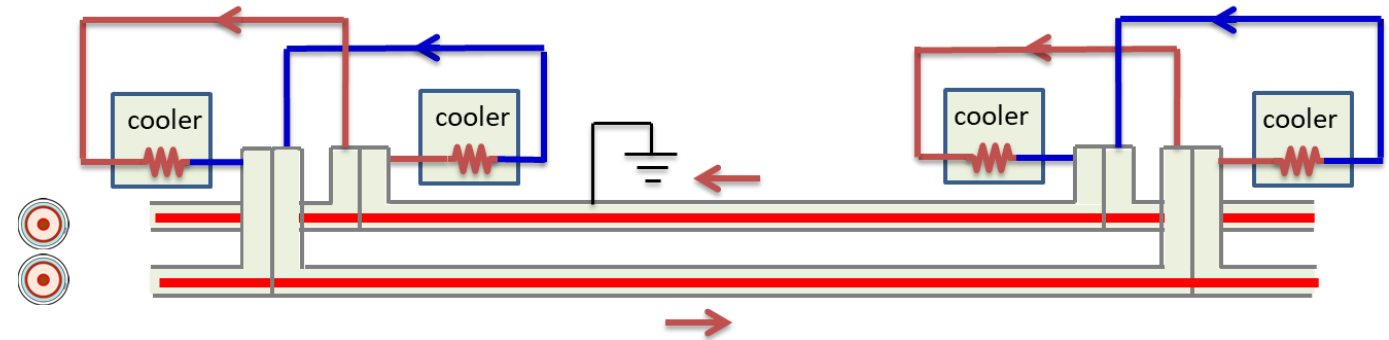
Separate phases/poles and cryostat

voltage

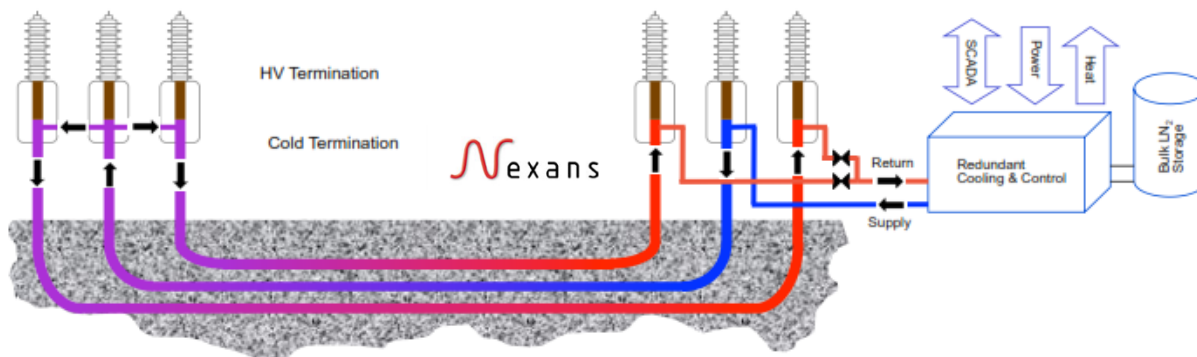
Different circulation schemes of coolant between cooling and pumping stations can be adopted depending on the layout of the cable system and in particular:

- Number of phases or poles per cryostat
- Internal or external return path of coolant

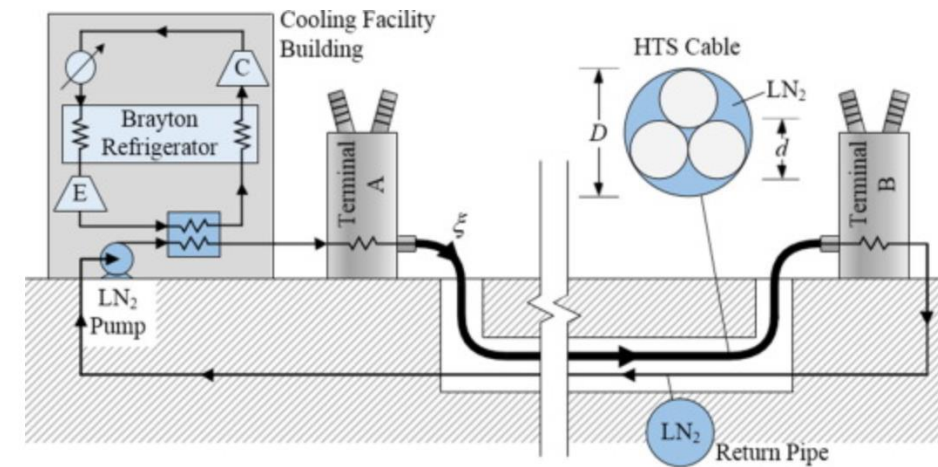
Example 1 - closed-loop circulation of coolant for a long DC cable system made of two monopoles with distinct cryostats



Example 2 - closed-loop circulation of coolant for the LIPA1 three phase HV cable



Example 3 - closed-loop circulation of coolant for the Shingal three phase MV concentric cable



The HTS cable system

Thermohydraulic design:

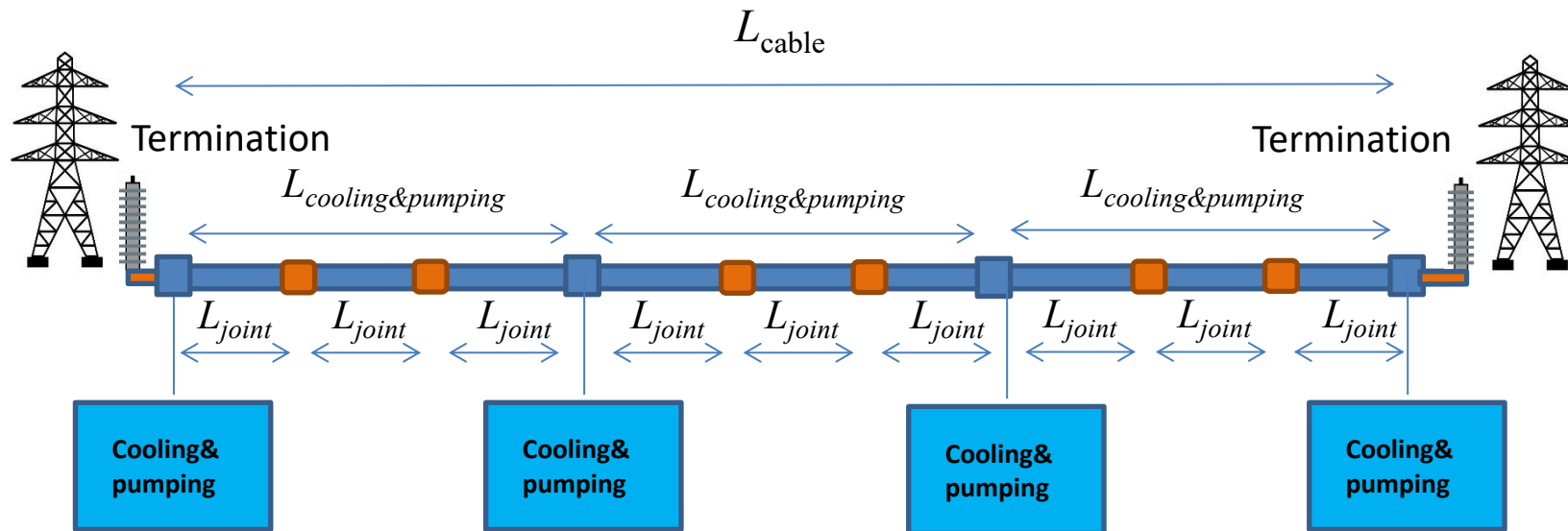
Distance $L_{cooling\&pumping}$ between cooling&pumping stations must be compatible with acceptable temperature and pressure, and may differ from overall length L_{cable} of the cable system

$$\frac{\Delta P}{\Delta x}(D_o, \dot{m}) \leq \frac{P^{in} - P_{min}^{out}}{L_{cooling\&pumping}}$$

$$\frac{\Delta T}{\Delta x}(D_o, \dot{m}) \leq \frac{T^{in} - T_{max}^{out}}{L_{cooling\&pumping}}$$

Outer diameter D_o

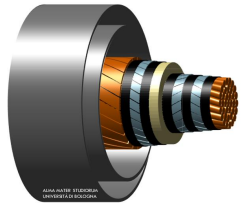
Mass flow \dot{m}



$L_{cooling\&pumping}$ may reach up to 20-40 km, depending on thermohydraulic design (D_o , \dot{m}) and constraints (see depth)

Distance L_{joint} between joints in the range 100-500 m due to manufacturing and transportation limits

Motivations for SC power cables - 1. more power and/or less voltage



higher transport current I , up to 5-10 more than conventional cable through same section

$$P = V I$$

More power at the same voltage

Less voltage at the same power

(+ operation at constant T)



| Conventional Collector Station | | SuperNode Collector Station | |
|--------------------------------|-------------------------|-----------------------------|------------------------|
| Capacity | 2 GW | Capacity | 2 GW |
| Voltage | 525 kV DC | Voltage | 80-250 kV DC |
| Volume | ~335,000 m ³ | Volume | ~74,000 m ³ |
| Weight | 20,000 tons | Weight | ~4,600 tons |
| Cost | €800m | Cost | €272m |

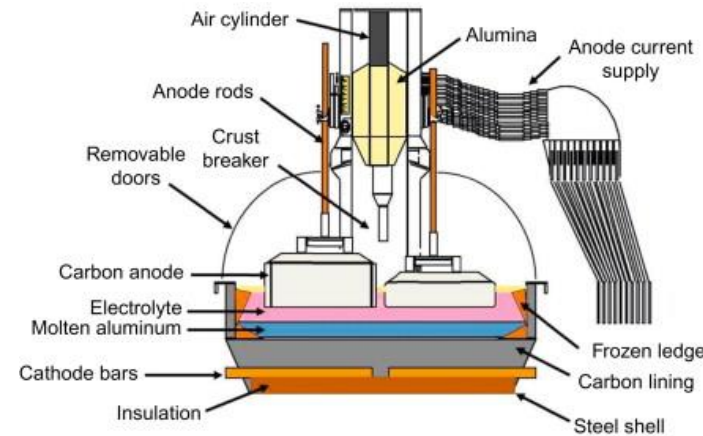
- Reducing right of way & soil occupation
- Much faster installation

- Use of existing utility civil infrastructures
- Use of other existing civil infrastructures and possibility of new integrated energy infrastructures concepts

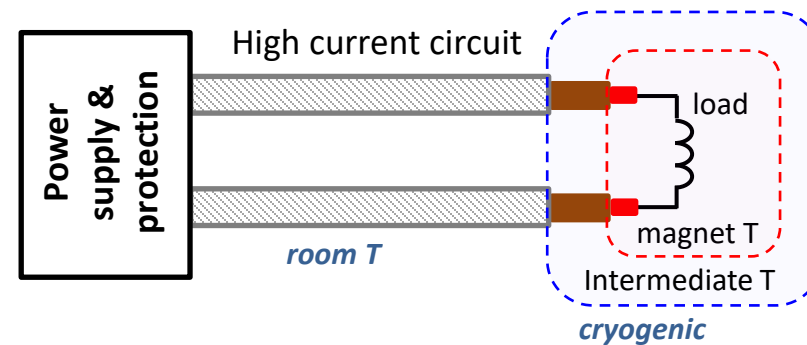
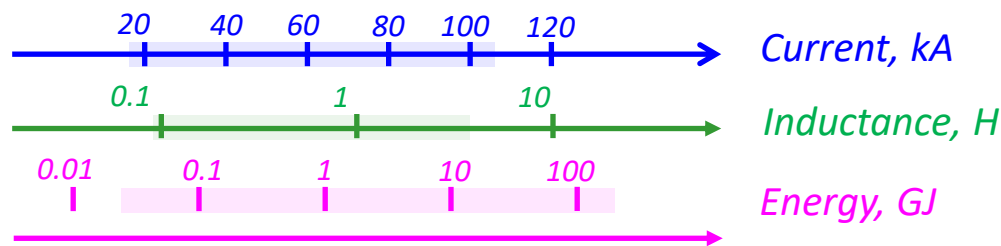
- Simplify electric equipment: conversion stages, converters' layout, platform

Motivations for SC power cables - 2. high current loads (regardless of the power)

1. Applications like chlorine, copper or zinc electrolysis as well as aluminum smelters need INTRINISC (process) direct current ranging from 10 kA up to 600 kA.



2. DC SC magnets for fusion reactors (Tokamak or Stellarator) operate with large DC currents in the range 20-105 kAs.



- Al DC Busbars
- Metallic current leads – Room T to interm. T (e.g. LN2)
- HTS Current leads – interm. T to magnet T

Motivations for SC power cables - 3. Less losses (cooling included)

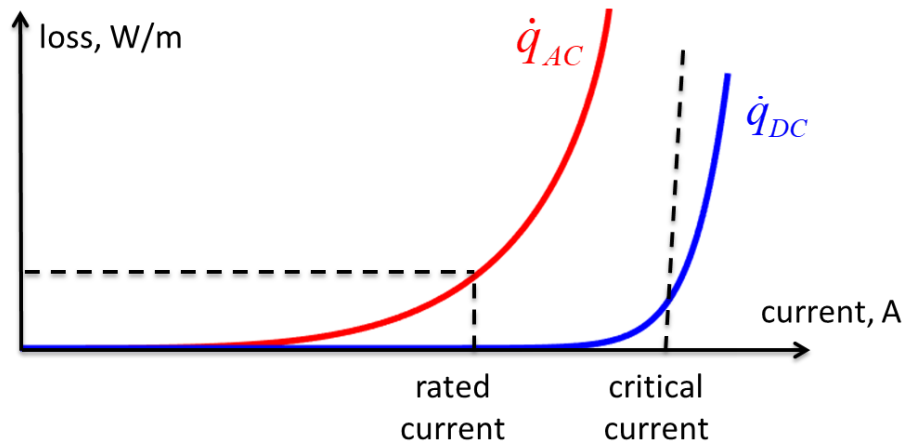
Electromagnetic losses per unit length (W/m) of current carrying superconductors:

AC transport current losses - Hysteretic diffusion of B and J

$$\dot{q}_{AC} = f \frac{\mu_0 I_c}{\pi} \left[(1-i) \ln(1-i) + (1+i) \ln(1+i) - i^2 \right] \quad i = \frac{I_{peak}}{I_c}$$

DC transport current losses - Flux creep

$$\dot{q}_{DC} = k i^n \quad (W/m) \quad i = \frac{I_{peak}}{I_c}$$



Typical losses at 65-80 K in cold dielectric power cables

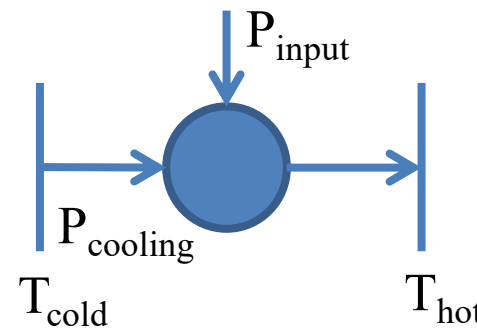
C. E. Bruzek, "Introduction to superconducting power cable systems", ESAS Summer School, Bologna 2016

| | Dependence | Parameters | Losses at 65-77 K | Losses at RT |
|--|--|---|--------------------|---------------------------|
| Radiation | Room temperature | Super-insulation spacer and diameter | 0,5 to 2 W/m | 12,5 à 50 W/m |
| HTS AC losses | Transported current Magnetic field distribution | Cable design (pitches, diameter,..) | 0,05 to 1 W/kA.m | 1,25 to 15 W/kA.m |
| Dielectric AC losses | Voltage level | Capacity of the cable and material (tg δ) | Up to 1 W/m | Up to 12,5 W/m for 220 kV |
| Eddy current AC on the cryostat | Magnetic field distribution | Cable design (pitches, diameter,..) | 0,05 to 0,1 W/kA.m | 1,25 to 2,5 W/kA.m |

Absent for DC cables

For a Cu cable typical 20 W/kAm

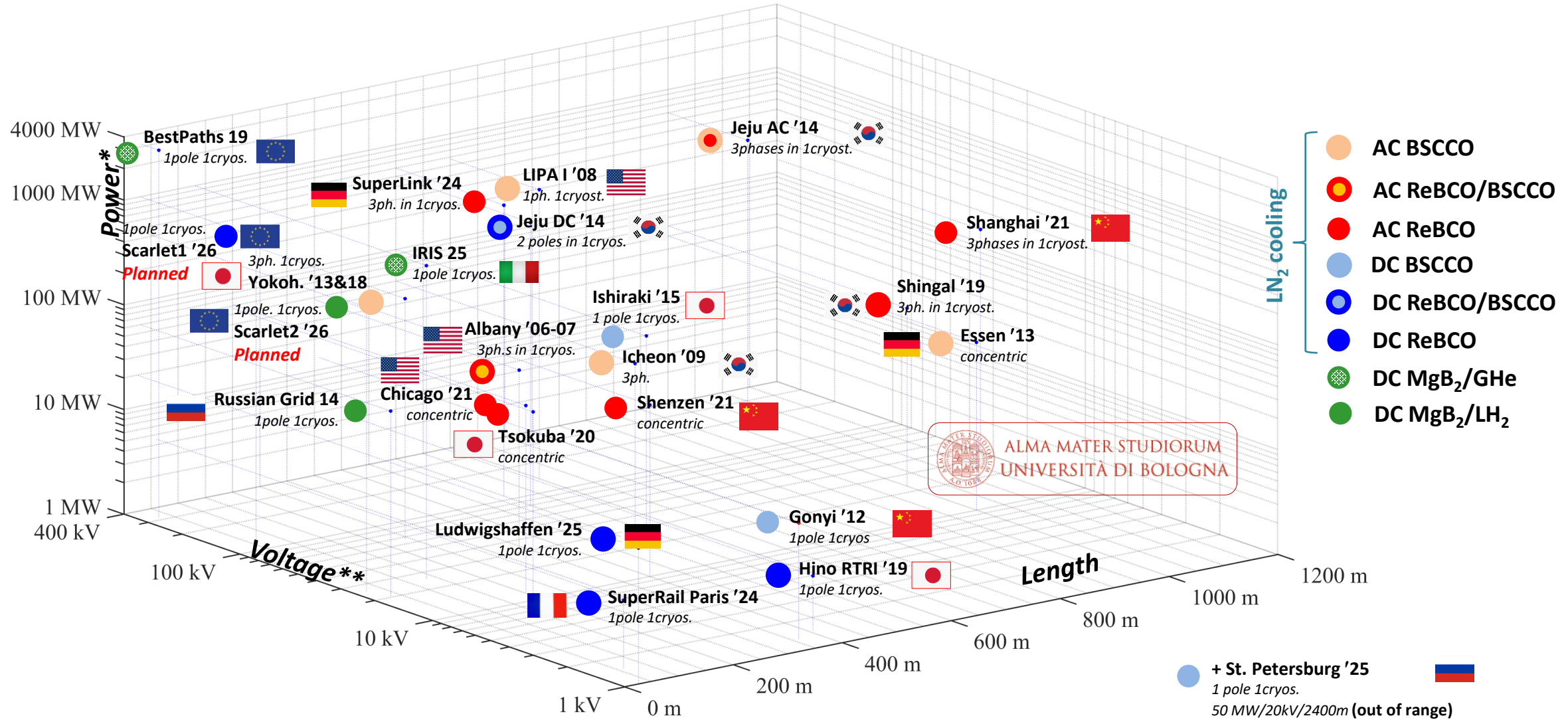
In DC cables no practical loss occurs in the superconductor



$$COP = \frac{\text{Watt of input power}}{\text{Watt of heat removed}}$$

- Cooling power a SC cable can be estimated to be approximately 25% of the losses of conventional cable system at full load
- Cooling energy over discontinuous operation (e.g. wind power transm.) may increase up to approx. 60%

State-of-the-Art of SC cable technology – main operational or demonstration projects (AC and DC)



* Apparent power (MVA) for AC cables.

Anto** Line-to-line RMS value for AC cables / Pole-to-ground value for DC cables

Chicago



AMSc
12 kV, 3 kA,
200 m
Single coaxial design
HTS material?
Energized 2021

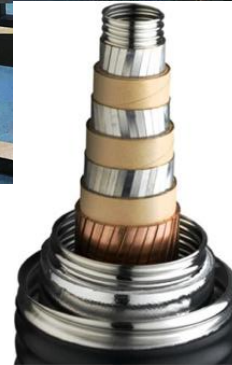


Figure:
AMSC

LIPA



Nexans
138 kV, 2.4 kA,
600 m
Single coaxial design
BSCCO 2223
Energized 2008



Figure:
Nexans

Shanghai



LS Cable
35 kV, 133 MVA, 1200 m
2G HTS
Energized 2022



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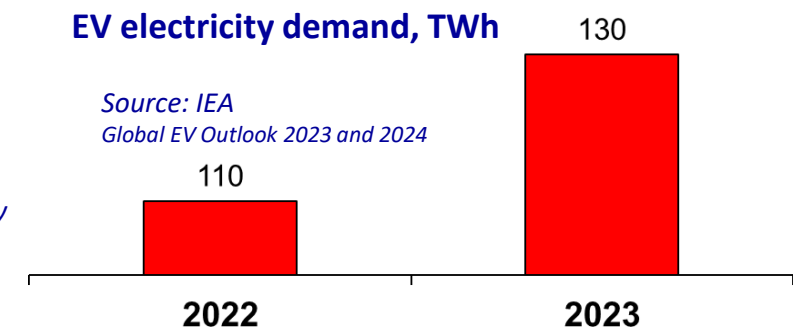
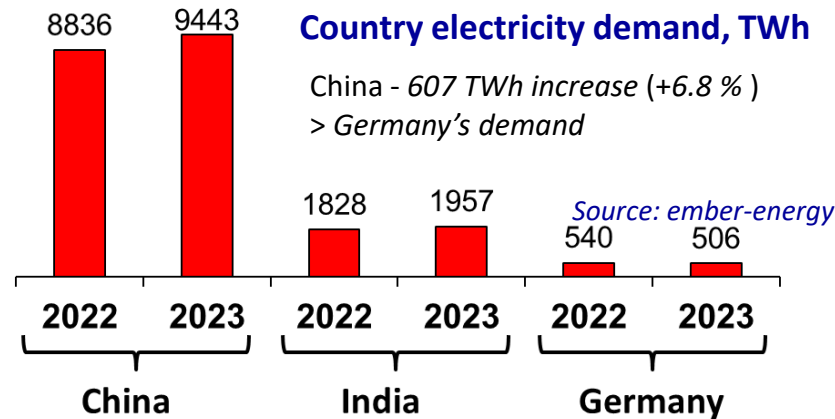
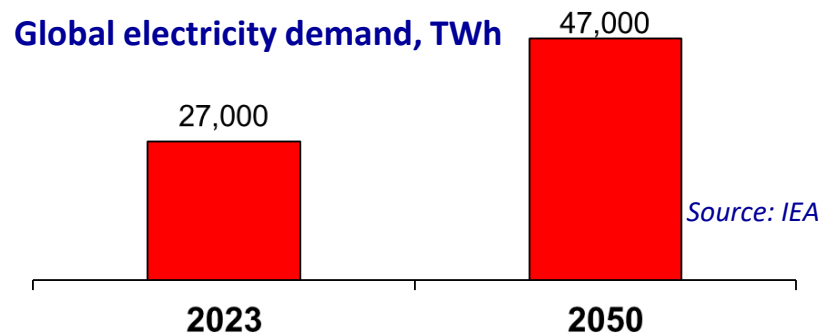
Global electricity demand – today and tomorrow

Growth in global electricity demand is set to accelerate at an average rate of 4% in the coming years due to:

1. Growth of emerging economies
2. “Electrification of everything” to meet decarbonization (i.e. electrification of terrestrial, marine and air transportation, more electric buildings, more electric heating in industry)
3. Exponential growth of new electricity needs: data centers

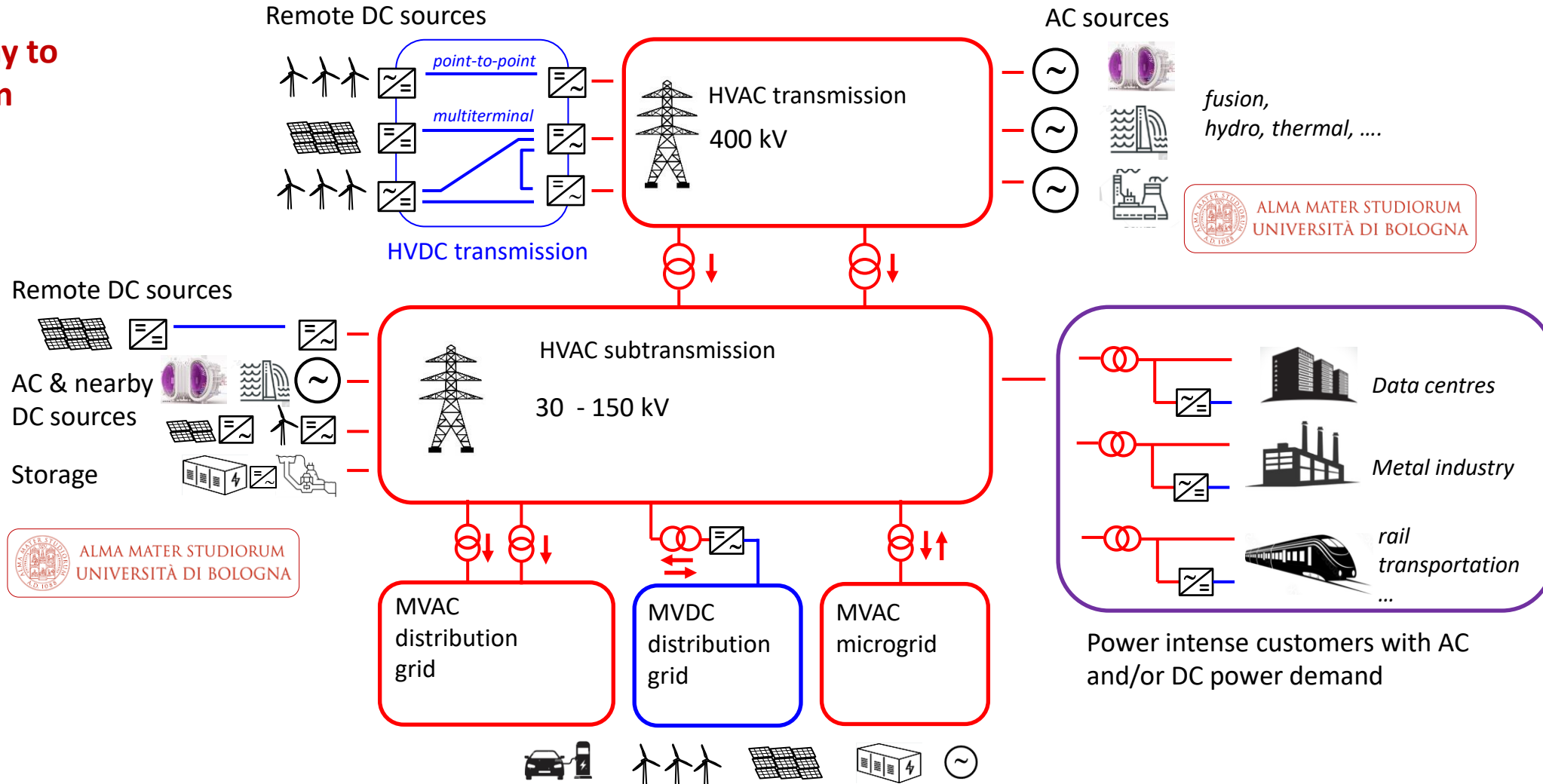


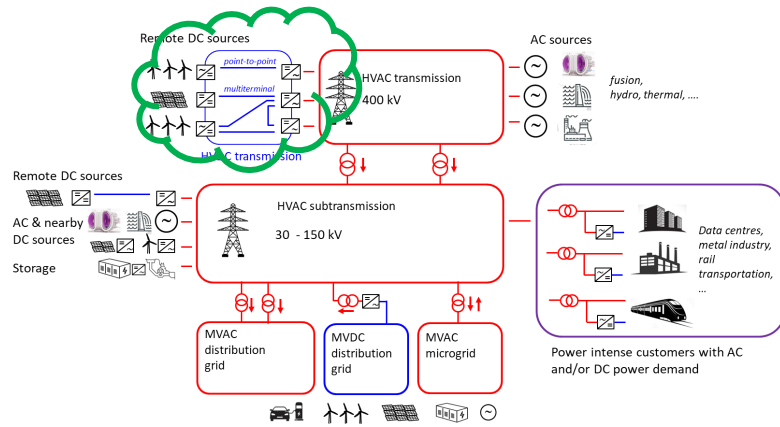
Over the next years, we will need to add as much power capacity as it took us a century to build



Addressing the challenge of growing and transforming electricity demand

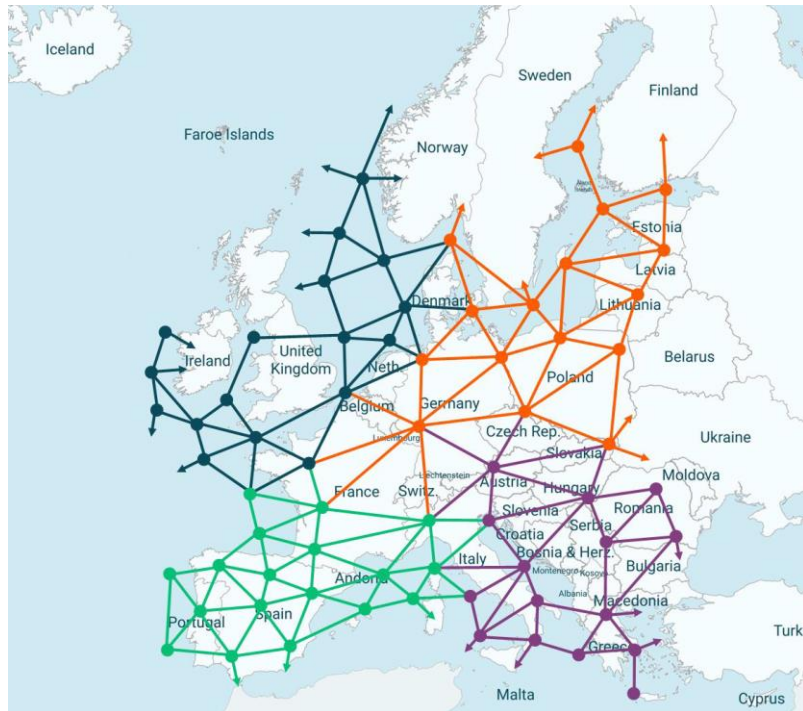
Schematic pathway to grid modernization and expansion





- **EU strategy on offshore renewable energy:** 60 GW of offshore wind and at least 1 GW of ocean energy by 2030, with a view to reach by 2050 300 GW
- **EU Solar Energy Strategy:** over 320 GW of solar photovoltaic by 2025 (more than doubling compared to 2020) and almost 600 GW by 2030
- **India's wind power potential** is estimated to be 695.50 GW at 120 meters and 1163.9 GW at 150 meters above ground level.

continental transmission grid



- **Extremely high-power density DC corridors are needed for implementing this vision which can only be achieved through HTS technology**

Superconductors will do for electricity what fiber optic cables did for telecoms by replacing the twisted pair. They will revolutionise power transfer, enabling ultra high capacity unobtrusive transmission.”

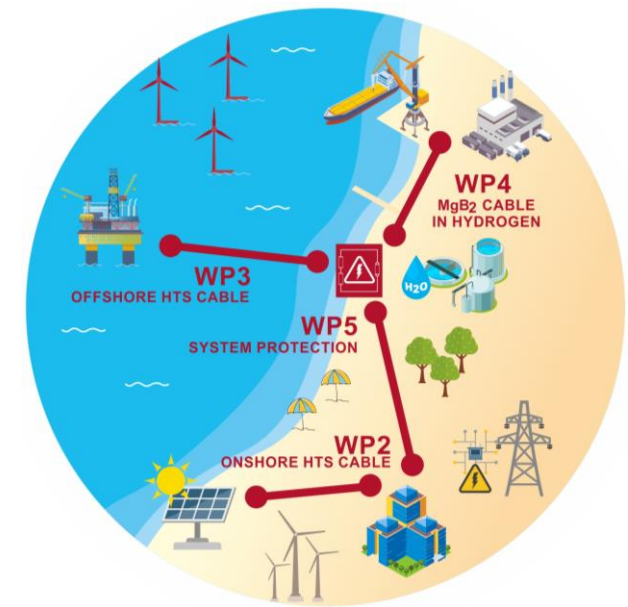
Pat Cox, SuperNode Chairman and Former President of the European Parliament

European Project SCARLET (2022-2027)

SCARLET

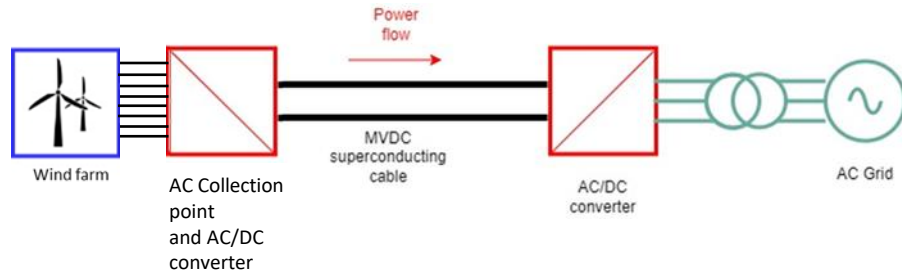
Superconducting Cables for
sustainable Energy Transition

- ❑ **Goal:** develop and industrially manufacture superconducting cable systems at the gigawatt level, bringing them to the last qualification step before commercialization
- ❑ Expertise from **15** industry and research organisations in the fields of material sciences, cryogenics, energy systems and electrical engineering
- ❑ 3 demonstration work packages
 - long-length onshore superconducting cable systems (WP2)
 - MgB₂ cables in liquid hydrogen (WP4)
 - system protection (WP5)
- ❑ 1 work package on architectures of offshore superconducting cable systems (WP3)
- ❑ 1 work package for integration studies and economic evaluation (WP1)
- ❑ lastly, work packages for communication and coordination (WP6)

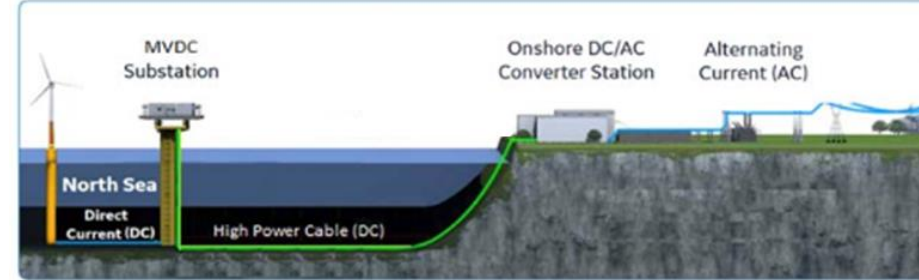
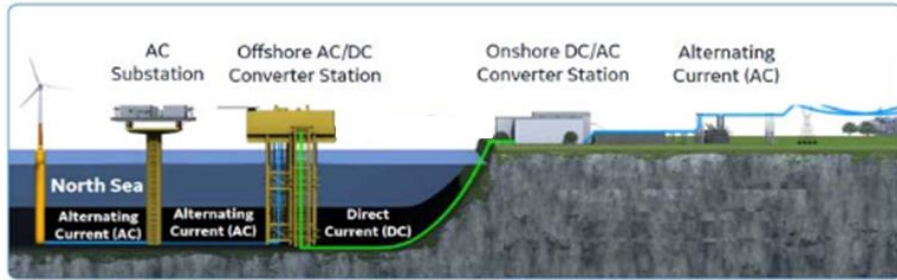
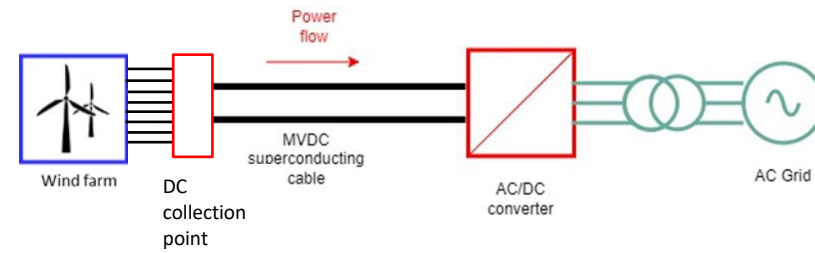


The selected case: unidirectional MVDC grid connection 1 GW offshore wind park

HVDC conventional links



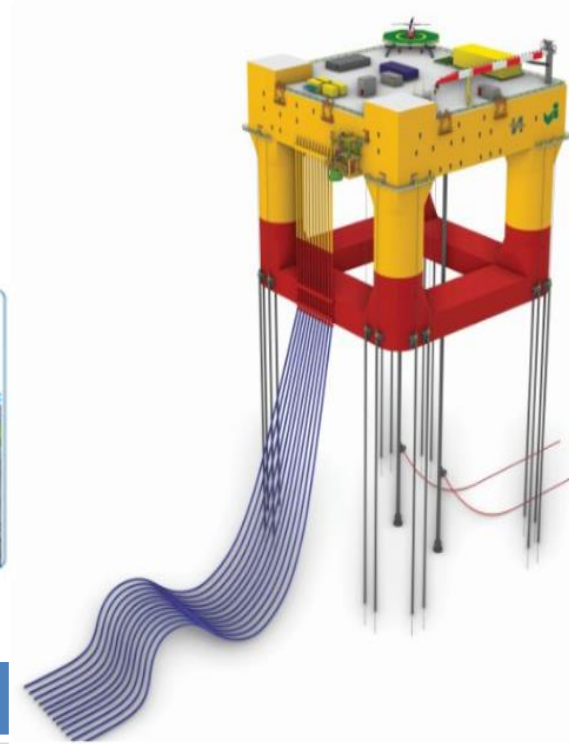
MVDC Superconducting links



No offshore substation

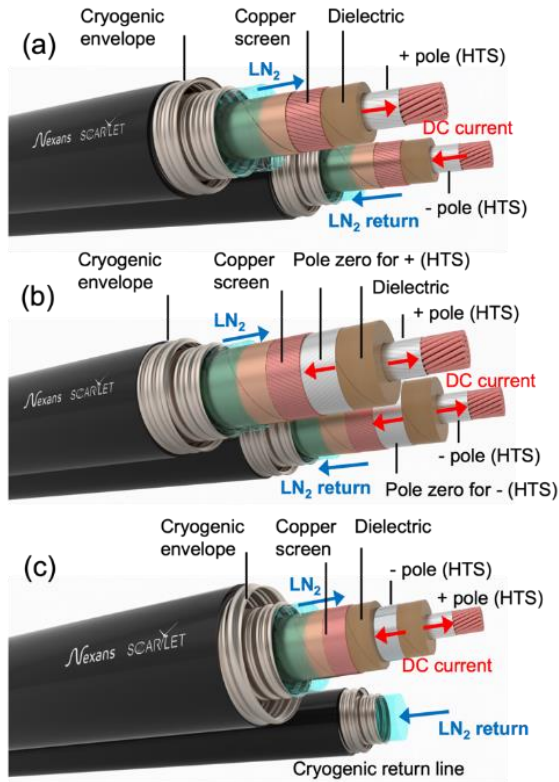
| | Cu/XLPE |
|-----------------------------|----------|
| Voltage, kVdc | ±525 |
| Current, kAdc | 0.93 |
| Temperature | 70-90 C° |
| Cooling, kW/km | 40 |
| Cooling of terminations, kW | --- |

| | HTS/LN2 | MgB2/LH2 |
|-----------------------------|---------|----------|
| Voltage, kVdc | ±50 | ±25 |
| Current, kAdc | 10 | 20 |
| Temperature | 65-75 K | 20 K |
| Cooling, kW/km | 23 | 36 |
| Cooling of terminations, kW | 30 | 30 |

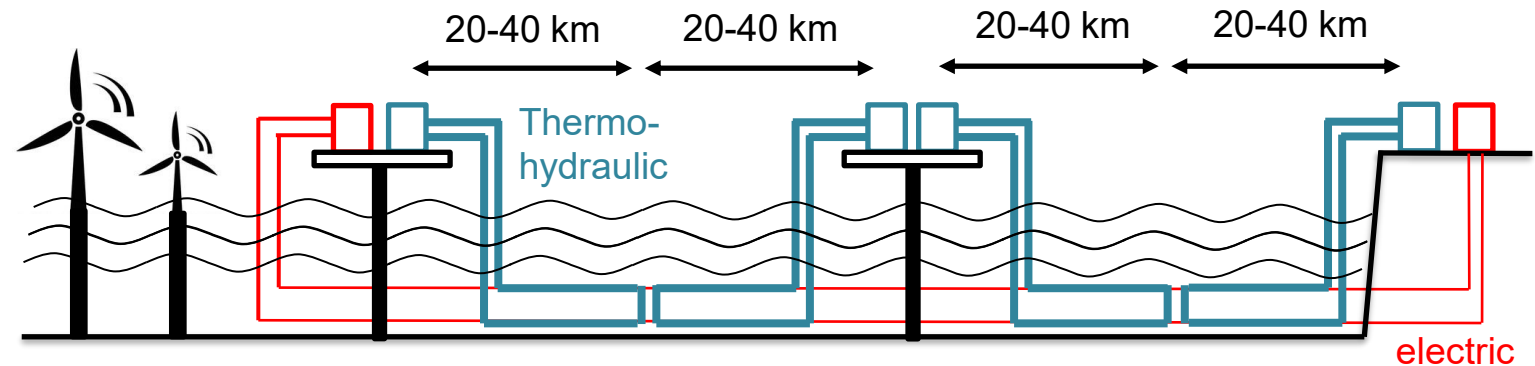


A much simplified platform hosting DC collection point is required

SCARLET - WP2&3 progress on 1 GW HTS/LN₂ cable system for off-shore wind 1/1



- LN₂-immersed cable cores, terminations&joints and cooling units developed for land based HTS cable directly applicable to submarine environments
- adapting the cryogenic envelope to withstand water pressure and dynamic mechanical stresses poses a significant challenge.



LN₂-immersed HTS cables can be cooled from a single station for lengths between 20 and nearly 40 km depending on sea depth

Three system layouts analyses based on

- Two ± 50 kV/10 kA monopoles with or without HTS shield
- Single ± 50 kV/10 kA HTS cable with concentric design and separate LN₂ return

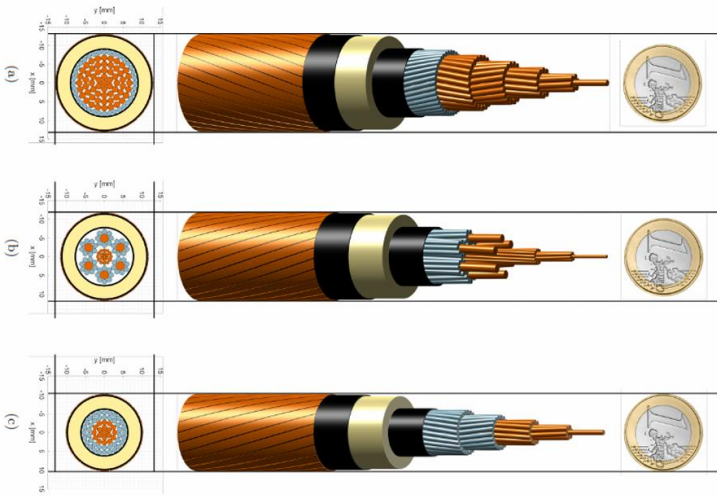
Max distance of a HTS DC cable link with no intermediate stations can reach up to 80 km



Final design to be chosen by March 2026

Source: Grid integration of high-power MVDC superconducting cables based on HTS and MgB₂, JICABLE2025

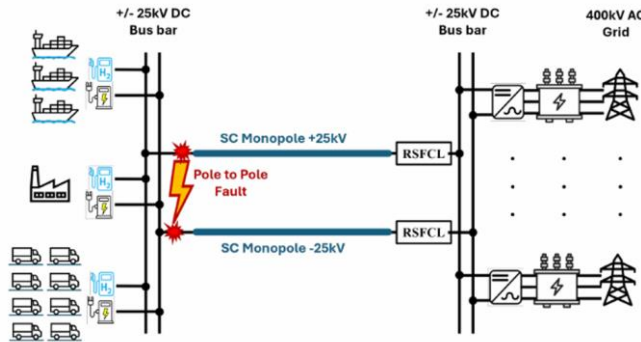
SCARLET – WP4 progress on 1 GW MgB₂/LH₂ cable system 1/2



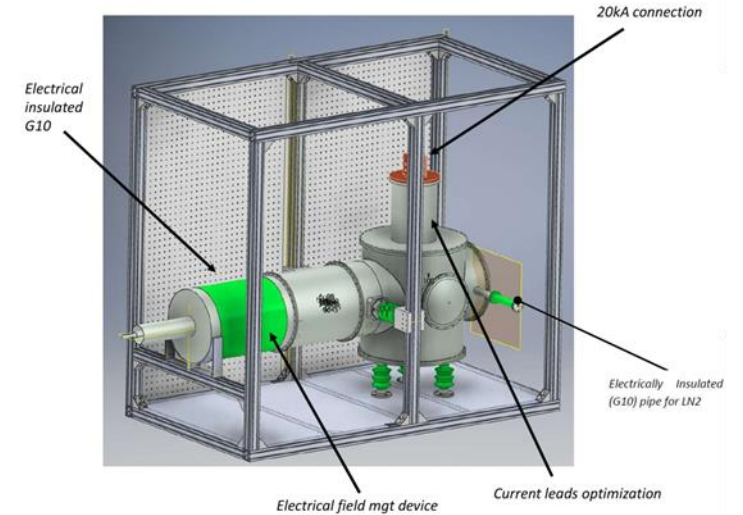
Electromagnetic design of the ±50 kV/10 kA cable completed

- Various geometrical configurations were analyzed and compared based on electrothermal transients.
- A single-layer MgB₂ cable was selected for its superior transient performance and manufacturing simplicity.

Desing of PPLP/LH2 electric insulation completed



Desing of terminations and joints completed

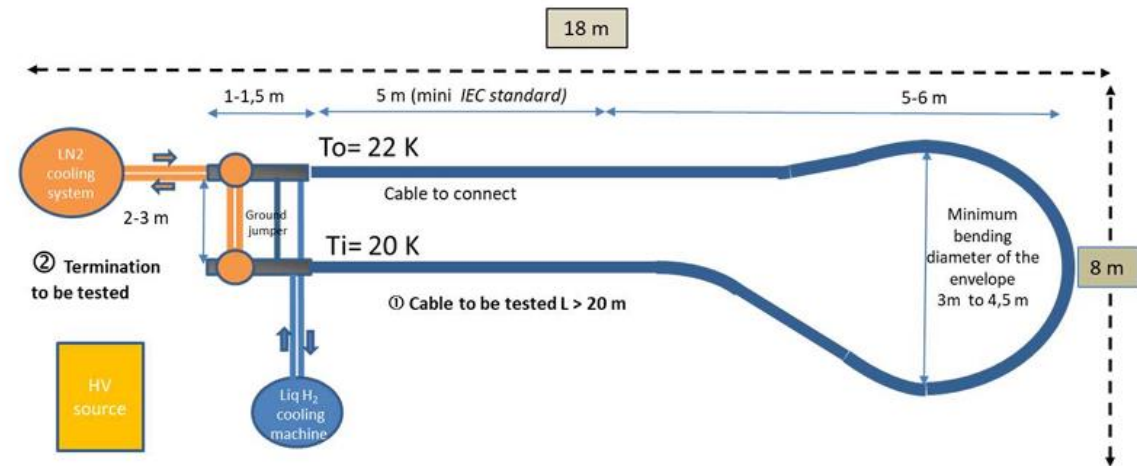


Novel setup developed to measure electrical properties of lapped insulation in LH₂



SCARLET – WP4 progress on 1 GW MgB₂/LH₂ cable system 2/2

- The manufacturing of the cable is planned for the first quarter of 2026
- Final test of the cable system at SINTEF premises scheduled by 2026



Not easy to purchase LH2 for the test (below 200kg).

The cooling system will be probably based on closed cooling loop, to recycle Hydrogen during the test with a RHCL (Rempote Helium Cooling loop) subcooling the LH2.

The decision will be taken by the end of the year based on LH consumption evaluation and delivery possibility.

Type test at Sintef followed by long duration test at Abslout System

The IRIS ± 25 kV/40 kA 1 GW MgB₂/GHe cable system 1/3



IRIS Project: Innovative Research Infrastructure on Applied Superconductivity)



in the frame of a large recovery effort called *PNRR*, the Italian branch of the Next Generation EU framework.

IRIS (Innovative Research Infrastructure on applied Superconductivity) is led by INFN (through its LASA lab in Milan) and includes also CNR-SPIN and 5 Universities).

Goal: developing applied superconductivity for HEP future collider (FCC-hh) and exploiting potential applications to society in green energy (higher sustainability) and in medical field.



- 60 M € including taxes (39 M € scientific instrumentation)
- Geographical distribution 45% North 55% South
- 36 Fixed-term positions (50% academic) 5 PhD
- Project duration: started on 1 Nov 2022, ending by 30 Apr 2026 (42 months)

| IRIS | |
|-----------------------|------------------|
| Power rating | 1 GW |
| Voltage | 25 kV |
| DC current | 40 kA |
| Operating temperature | 20 K |
| Cooling medium | He gas |
| Superconductor | MgB ₂ |
| Line length | 130 m |
| Inner pressure | 10 bar |

Istituto Nazionale di Fisica Nucleare

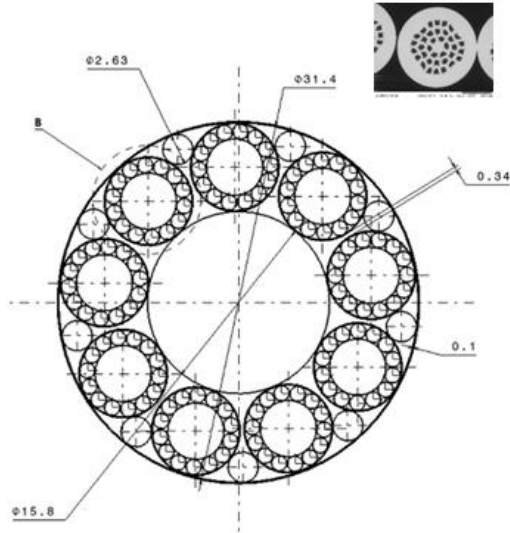
PARTNERS



The IRIS ± 25 kV/40 kA 2 GW MgB₂ cable system 2/3



CABLE DESIGN AND TEST VALIDATION



1.3mm wire



The cable has been designed in the multi-petals configuration
Able to carry 40kA with an operative margin higher than
25% at 25K and 50% at 23K

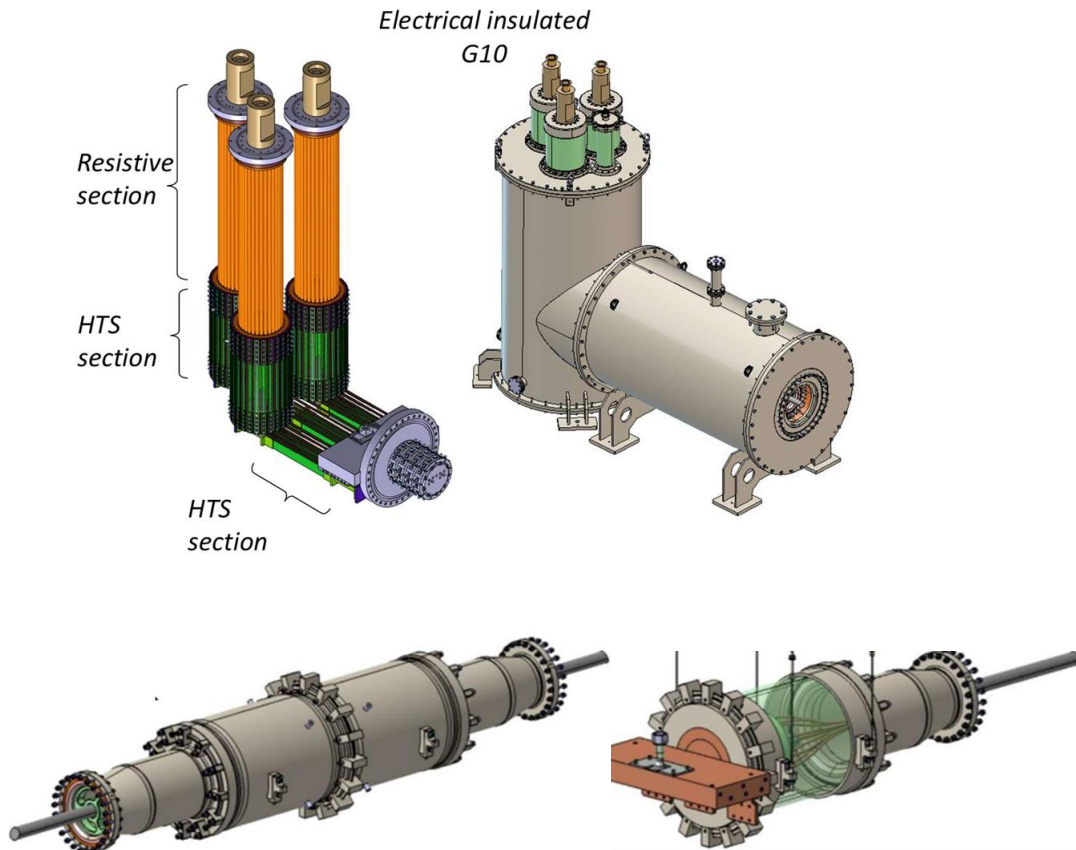
More than 100km of MgB₂ wires has been produced
to validate the cabling process and to manufacture the cable
Cabling and insulation activities has been completed



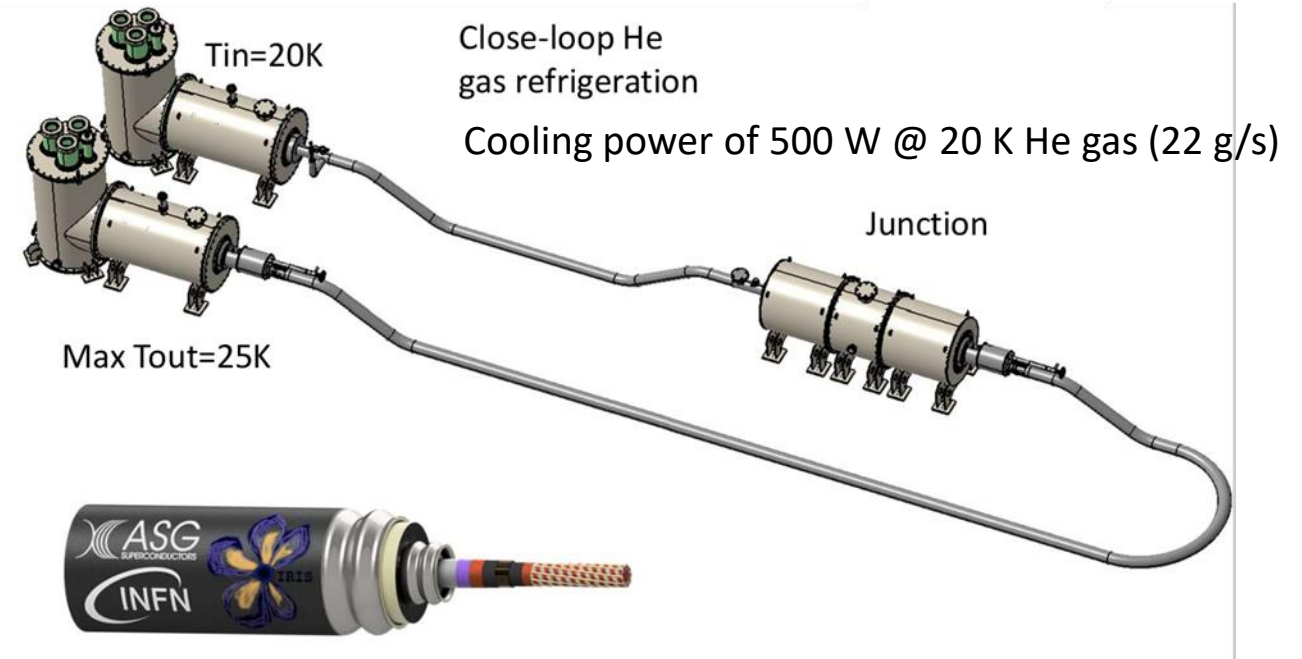
In the next weeks 20m long full cable will be
tested at ASG plant

The IRIS ± 25 kV/40 kA 2 GW MgB₂ cable system 3/3

Terminations and joints



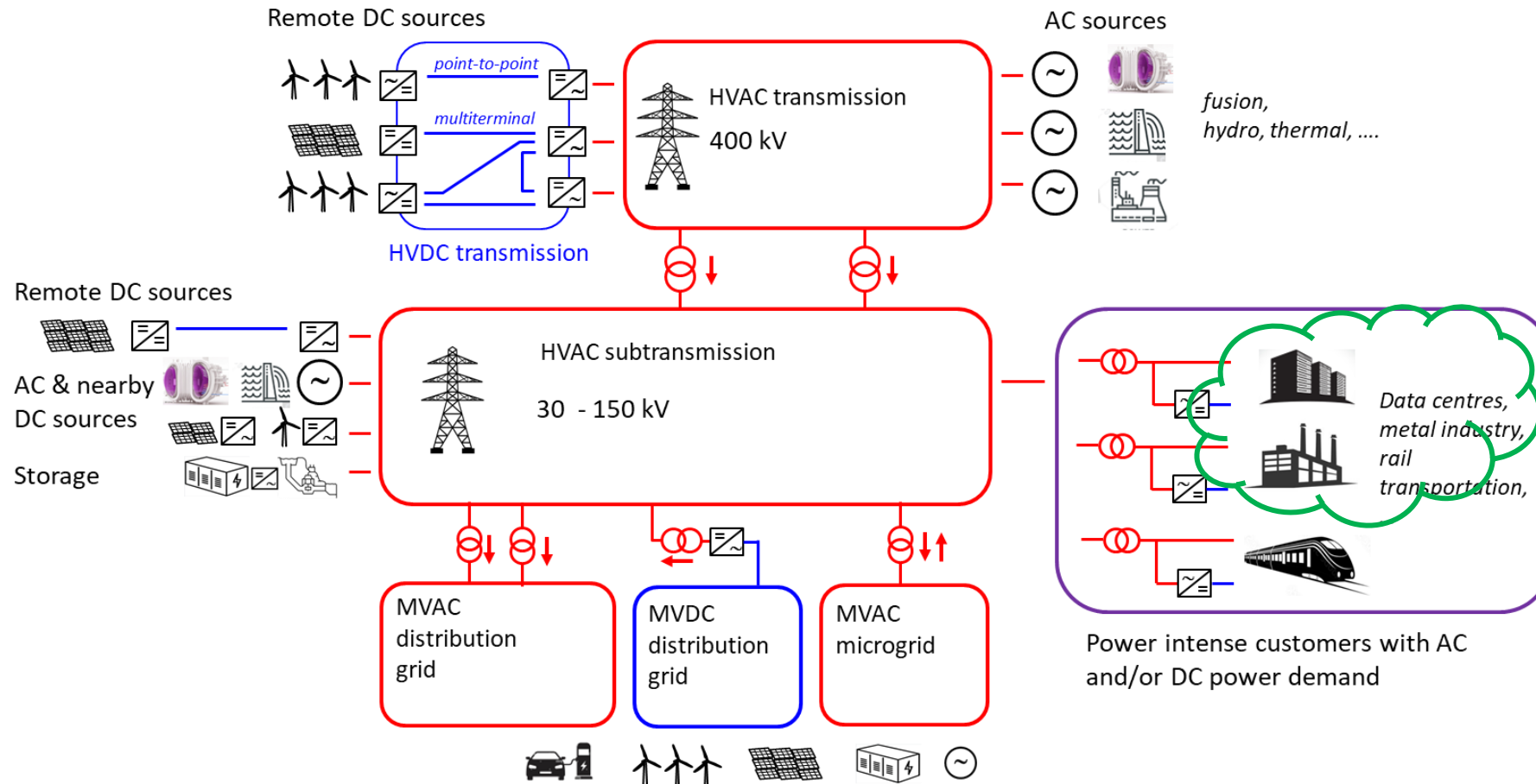
Test Line



Test to start by the end of 2025

Design completed, now in construction with most of the materials already supplied

DC SC busbars for low-voltage power-intensive customers



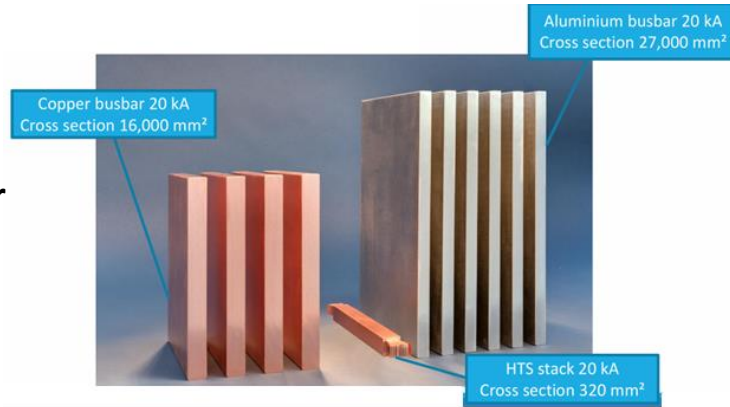
Supplying established (metal industry) and emerging (data centers) power-intensive and current-intensive DC customers

DC high-current low-voltage busbar - the VESC R&D projects 1/2



1 kV / 20 kA busbars for chlorine electrolysis successfully developed

Ludwigshaffen '25

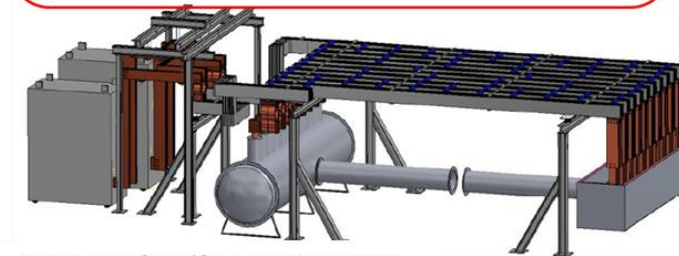


Next:
Scale up to 200 kA for aluminum electrolysis applications



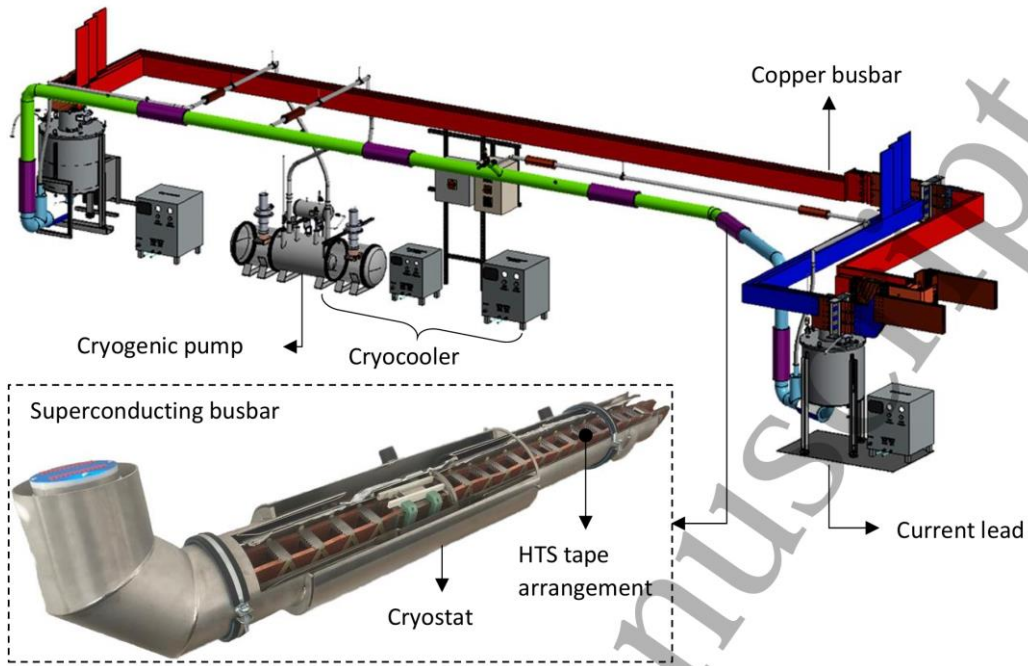
Demonstration of the short-length 200 kA HTS busbars successfully completed in 2024

- DEMO200
 - R&D-Demonstrator 200 kA, world record
 - Aluminium smelter applications
 - Test successfully performed 2024-09.



Courtesy of Wolfgang Reiser VESC

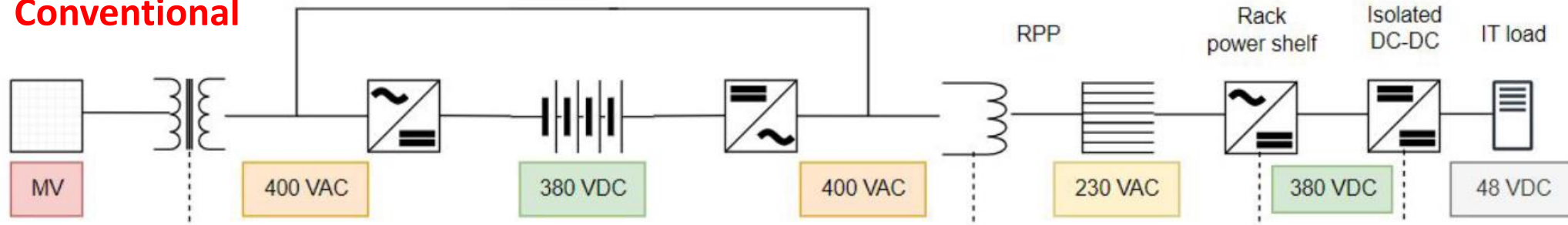
In progress:
development of a 200 kA HTS busbar, operating in parallel with existing aluminum busbars, for installation at the TRIMET industrial site



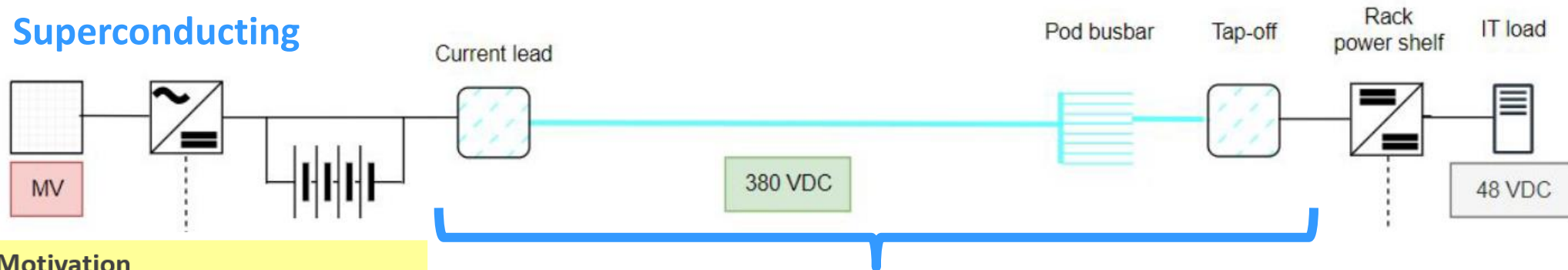
DC high-current low-voltage busbar - the VESC experience 2/2

Conventional vs. Superconducting Hyper Scale DataCenters

Conventional



Superconducting



Motivation

- Increased demand for Hyperscale DataCenters
- Increased Power per Rack
 - Up to 200 kW per Rack for AI-Applications
- Increased Efficiency Demand

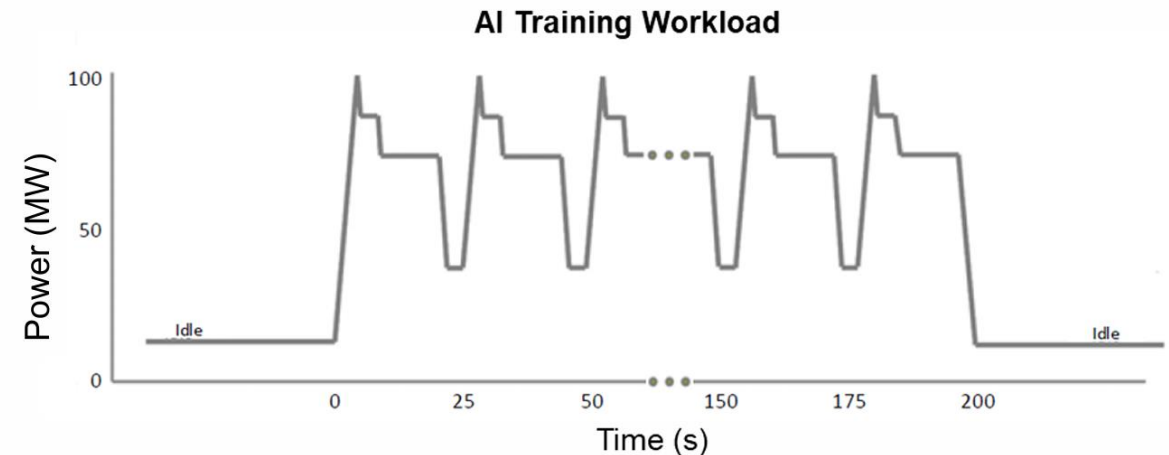
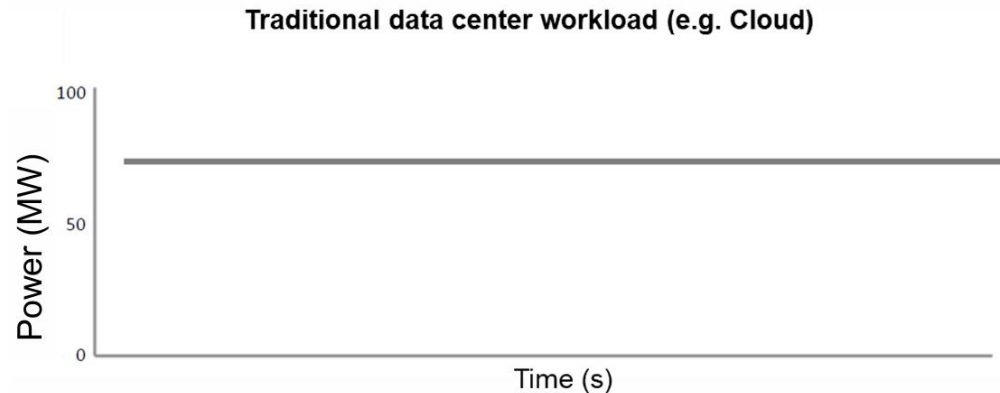
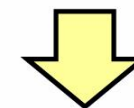
Superconducting Busbar with multiple Tap-offs
Reduction of Power Conversion Steps
DC Distribution: Up to 100 MW on Low Voltage

Courtesy of Wolfgang Reiser VESC

A warning – is rack power required by data centers ultimately DC?

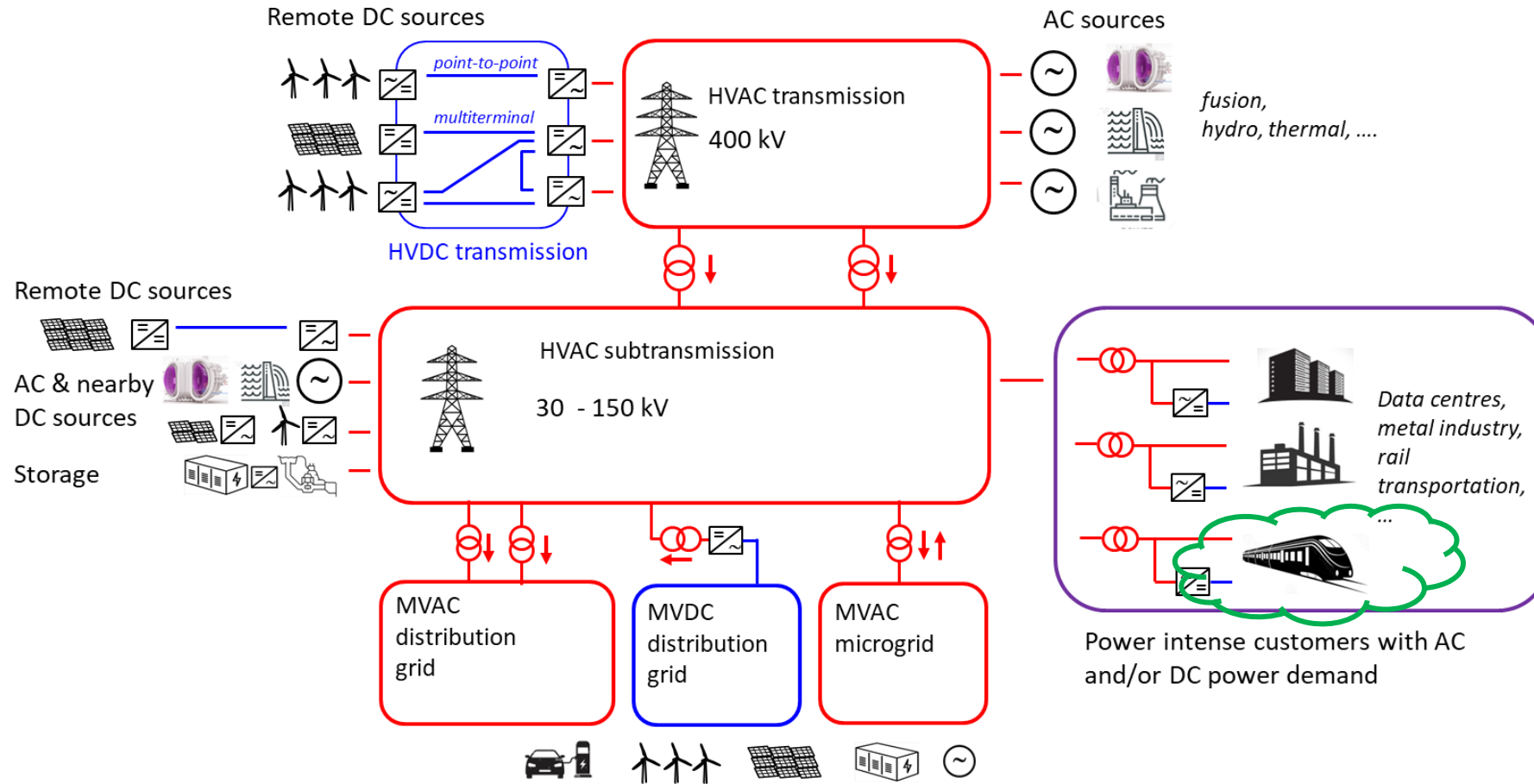
Traditional data center vs AI training Data Center

| Aspect | Traditional Data Center | AI Training Data Center |
|-----------------------|--|--|
| Purpose and Operation | Designed for steady, continuous workloads — web hosting, storage, and cloud applications. Load profile is flat and predictable . | Runs intense, batch-based workloads — AI model training and inference. Load profile is highly variable , with spikes during training and idle periods between jobs. |



Large power/current fluctuations occur in DC data center supply systems, which impact the design of the proposed SC solution

DC SC busbars for low-voltage power-intensive customers



Supplying established (metal industry) and emerging (data centers) power-intensive and current-intensive DC customers

DC HTS cables for railway power supply – The SuperRail Project 1/2

- **Motivation: the need to increase rail traffic in densely populated areas translates into the the need for upgrade of the railway power supply infrastructure**

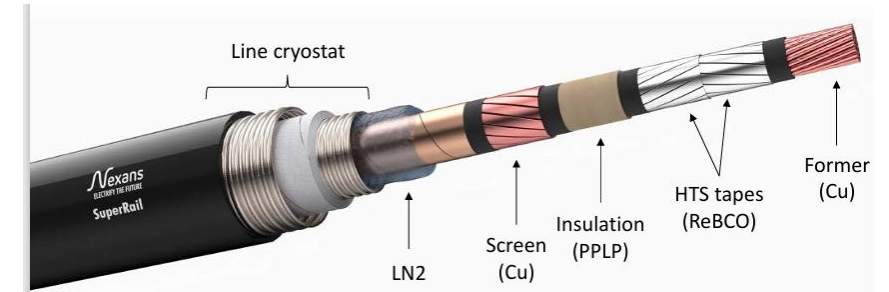
Reinforcement of Paris Montparnasse train station 28 tracks, 200 000 passengers/day on 750 trains. 50M of passengers in 2020, 90M in 2030



Existing rights of way saturated only 2× Φ100 mm conduit left = 2× 400 mm² copper cable = 2× 500 A reinforcement Instead of the required 3000 A

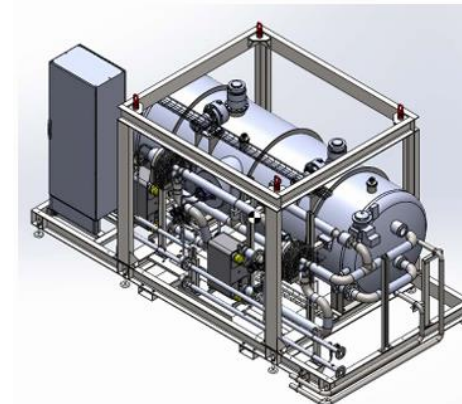
4.5 MW of nominal power (3000 A @1500 VDC) 10.5 MW of inrush power (7000 A) Fault current of 67 kA during 100 ms

Courtesy of Loïc Quéval, GeePs, CentraleSupélec,



| Electric parameters | |
|---------------------|----------------|
| Nominal voltage | 1500 V |
| Nominal current | 1500 A |
| Inrush current | 3500 A |
| Critical current | >4000 A |
| Fault current | 67 kA - 100 ms |

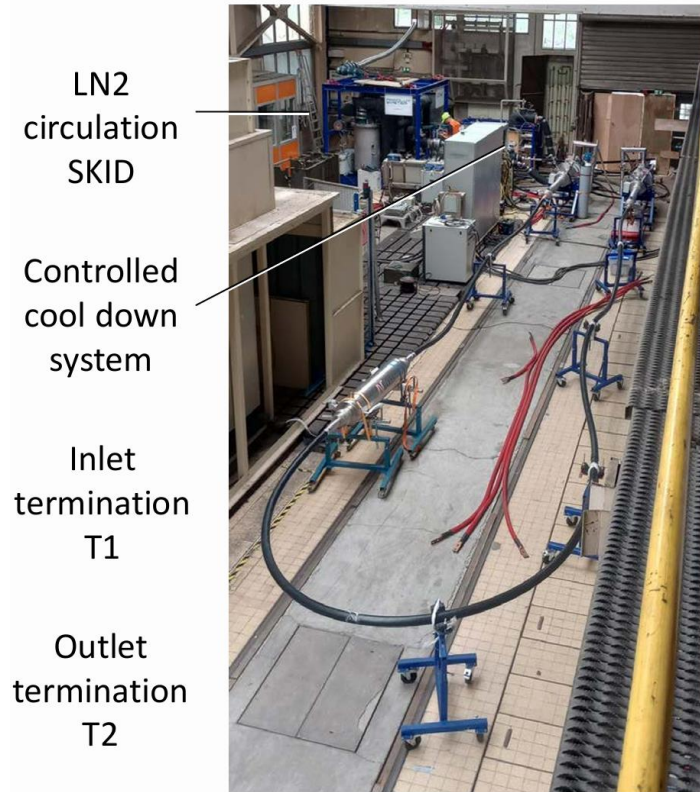
| Geometric parameters | |
|-------------------------|---------|
| Cryostat outer diameter | 74 mm |
| Minimum bending radius | 1.5 m |
| Length | 2x 60 m |



Reverse Turbo Brayton (RTB) for the final installation, with high efficiency and low maintenance
1.7 kW @67 K

DC HTS cables for railway power supply – The SuperRail Project 2/2

Summary of type test at SNCF AEF



| Test | Results |
|-------------------------------|---------|
| Thermal cycles | ✓ |
| Pressure | ✓ |
| Dielectric | ✓ |
| Lightning impulse | ✓ |
| Nominal current | ✓ |
| System losses & pressure drop | ✓ |
| Fault current & recovery time | ✓ |
| V-I characteristic | ✓ |

4.5 MW of nominal power (3000 A @1500 VDC) successfully developed and qualified

Commissioning for final installation started in 2025

Conclusion

- **HTS and MgB₂ DC power cable technology has been widely established through many demonstration projects worldwide.**
- **DC cable systems with current ratings up to 200 kA and voltage ratings in the hundreds of kV, providing a breakthrough asset for a wide spectrum of applications, are now feasible based on HTS and MgB₂ technologies.**
- **Long-running in-field demonstrators need to be deployed in order to cover the final steps toward mass market penetration**
- **Cheap and abundant superconductors are required, along with reliable and high-capacity cooling machines and accessories, and industry production capacity of the entire cable system**

Thanks for your attention

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